

## Lattice Boltzmann simulations of the rising bubble flows

Seungyeob Ryu, Cheon Tae Park, Juhyeon Yoon, Keung Koo Kim  
Korea Atomic Energy Research Institute, Deokjin-dong 150, Yusung-Gu, Daejeon

### 1. Introduction

Recently, the lattice Boltzmann method (LBM) has gained much attention for its ability to simulate fluid flows, and for its potential advantages over a conventional CFD method. The key advantages of LBM are, (1) suitability for parallel computations, (2) absence of the need to solve the time-consuming Poisson equation for a pressure, and (3) an ease with the way multiphase flows, complex geometries and interfacial dynamics may be treated[1].

The motion of the bubbles in a liquid has been the focus of both academic and practical interest. The central problem is the relationship between the rise velocity, bubble shape due to the interface deformation and flow field. The buoyancy effect due to density difference in the two phase flows is characterized with Eotvos and Morton numbers[2].

In this study, a single bubble rising under a buoyancy is simulated with the method proposed by Zheng et al.[3]. The simulation results are compared with those of a previous numerical method such as VOF. The results by LBM are also presented for the coalescence of the bubbles. The main objective of the present work is to establish the lattice Boltzmann method as a viable tool for the simulation of multiphase or multi-component flows.

### 2. Methods and Results

#### 2.1 Methodology

Here, we consider a flow with two phases which have different densities. The low density and high density are noted as  $\rho_L$  and  $\rho_H$  respectively. The flow can be described by the Navier-Stokes equations and an interface evolution equation as [3]

$$\frac{\partial \phi}{\partial t} + \nabla \cdot (\phi \bar{u}) = \theta_M \nabla^2 \mu_\phi \quad (1)$$

$$\frac{\partial n}{\partial t} + \nabla \cdot (n \bar{u}) = 0 \quad (2)$$

$$\frac{\partial n \bar{u}}{\partial t} + \nabla \cdot (n \bar{u} \bar{u}) = -\nabla \cdot P + \mu \nabla^2 \bar{u} + \bar{F}_b \quad (3)$$

where  $\theta_M$  is called mobility,  $\mu_\phi$  is the chemical potential,  $P$  is the pressure tensor,  $\bar{F}_b (= \phi \bar{g}, \text{ if } \phi < 0)$  is the body force, and  $n, \phi$  are defined as

$$n = \frac{\rho_A + \rho_B}{2}, \phi = \frac{\rho_A - \rho_B}{2}$$

where  $\rho_A$  and  $\rho_B$  are the density of fluid A and fluid B respectively.

Under the lattice Boltzmann framework, Eq. (1) can be solved by iterating the evolution equation for a set of distribution functions. These distribution functions evolve with a modified lattice Boltzmann equation and BGK approximation,

$$g_i(x + e_i \delta t, t + \delta t) = g_i(x, t) + \Omega_i + (1 - q) \delta g_i$$

with

$$\Omega_i = \frac{g_i^0(x, t) - g_i(x, t)}{\tau_\phi}$$

$$\delta g_i = g_i(x + e_i \delta t, t) - g_i(x, t) \quad (4)$$

where  $g_i$  is the distribution function,  $\Omega_i$  is the collision term,  $\tau_\phi$  is the dimensionless single relaxation time,  $e_i$  is the lattice velocity, and  $q$  is a constant coefficient.

In Eq. (3), the term  $\nabla \cdot P$  is related to the surface tension force. This force can be rewritten as a potential term,

$$\bar{F}_s = -\nabla \cdot P = -\phi \nabla \mu_\phi - \nabla p_0$$

where  $p_0 = n c_s^2$ ,  $c_s$  is the speed of sound.

The potential form for the surface tension force is adopted to keep the energy conservation. Mathematically, the potential form and stress form are identical. However, numerically, the discretization error is different[3]. Thus, it is useful to eliminate spurious currents.

The lattice Boltzmann implementation of Eqs. (2) and (3) can be described as

$$f_i(x + e_i \delta t, t + \delta t) = f_i(x, t) + \Omega_i \quad (5)$$

with

$$\Omega_i = \frac{f_i^0(x, t) - f_i(x, t)}{\tau_n} +$$

$$\left(1 - \frac{1}{2\tau_n}\right) \frac{w_i}{c_s^2} [(\bar{c}_i - \bar{u}) + \frac{(\bar{c}_i \cdot \bar{u})}{c_s^2} \bar{c}_i] (-\phi \nabla \mu_\phi + \bar{F}_b) \delta t$$

The equilibrium distributions satisfy the conservation laws as

$$\phi = \sum_i g_i, n = \sum_i f_i$$

$$\bar{u} = \left[ \sum_i f_i \bar{c}_i + \frac{1}{2} (-\phi \nabla \mu_\phi + \bar{F}_b) \right] / n$$

The details are Ref. [3].

The chemical potential is chosen as

$$\mu_\phi = A(4\phi^3 - 4\phi^{*2}\phi) - \kappa\nabla^2\phi$$

Following the same procedure as [3], we can obtain the profile along the normal direction of the interface

$$\phi = \phi^* \tanh(2\zeta/w)$$

Where  $\zeta$  is the coordinate which is perpendicular to the interface, and  $w$  is the thickness of the interface layer,

$$w = \frac{\sqrt{2\kappa/A}}{\phi^*}$$

For a flat interface, the surface tension coefficient can be evaluated by Rowlinson and Widom[4].

$$\sigma = \int \kappa \left( \frac{\partial\phi}{\partial\zeta} \right)^2 d\zeta$$

We can obtain the surface tension coefficient as

$$\sigma = \frac{4\sqrt{2\kappa A}}{3} \phi^{*3}$$

Where  $\phi^* = \frac{\rho_H - \rho_L}{2}$ .

## 2.2 Results

The two dimensional single bubble rising under a buoyancy is simulated. The density ratio and the surface tension are the same as Takada et al.[2]. The bubble is surrounded with stationary walls. Initially, it is located at a lower region of the computational domain (80x300). The dimensionless parameters are defined as

$$Eo = \frac{g(\rho_H - \rho_L)D^2}{\sigma}, \quad M = \frac{g(\rho_H - \rho_L)\mu_H^4}{\rho_H^2\sigma^3}$$

The bubble will rise at a nearly constant velocity due to the balance between the buoyancy and the drag force. The comparison of simulation results are shown in Fig. 1. The present results are in good agreement with those of the VOF method and Takada's LBM[3]. As shown in Fig. 1, the Eotvos number( $Eo$ ) increases gradually from 5 to 40. The increase of  $Eo$  is equivalent to the decrease of the surface tension. These will enhance the deformation of a bubble. These results are clearly presented in Fig. 1.

## 3. Conclusion

The lattice Boltzmann method for two phase flows has been applied to the simulations of bubbles under a buoyancy. The results for the rise velocity, and the bubble shapes with Eotvos and Morton numbers were found to be in good agreement with the VOF method and other LBM method. The coalescence of the bubbles is also presented. Also, it can be implemented easily for a three dimensional case.

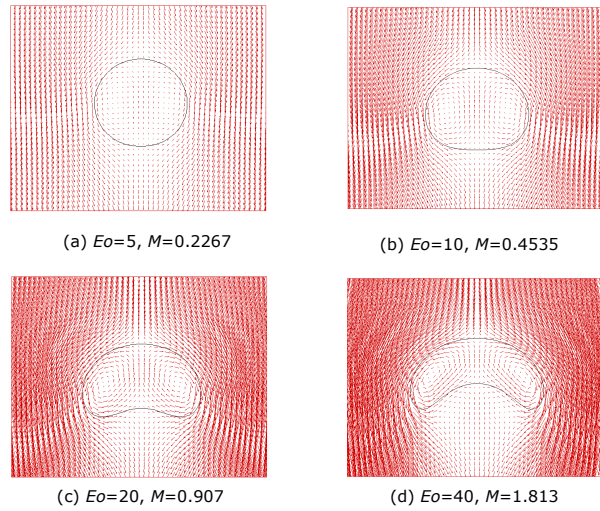


Fig. 1. The flow velocities and interfacial profiles of rising bubbles simulated with present LBM method. ( $w=3$ ,  $D=20$ ,  $\Gamma=1$ , density ratio=2.45,  $\sigma = 0.00521$ ).

## REFERENCES

- [1] Dieter A. Wolf-Gladrow, Lattice Gas Cellular Automata and Lattice Boltzmann method, Springer: Berlin, 2000.
- [2] N. Takada, M. Misawa, A. Tomiyama, and S. Hosokawa, Simulation of bubble motion under gravity by lattice Boltzmann Method, J. Nucl. Sci. Technol., Vol. 38, pp. 330-341, 2001.
- [3] H. W. Zheng, C. Shu, and Y. T. Chew, A lattice Boltzmann model for multiphase flows with large density ratio, J. Comput. Phys., Vol. 218, pp. 353-371, 2006.
- [4] J. S. Rowlinson, and B. Widom, Molecular Theory of Capillarity, Clarendon, Oxford, 1989.