# Control of Resintering Behavior of UO<sub>2</sub> Fuel Pellets by Modifying the Microstructure

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#### 1. Introduction

Pores in UO<sub>2</sub> fuel pellets and fission gas bubbles which were generated during the fuel irradiation were converted to vacancies by the interaction with fission fragment.[1] These vacancies shifted to the grain boundary and then diffused out to open-pores. As a result of the vacancy diffusion, UO<sub>2</sub> fuel pellets were redensified and the dimension of pellets was decreased. This resintering behavior of UO<sub>2</sub> fuel pellets during the irradiation affect the fuel performance of nuclear fuel rods[2]. It is important to control the pore structure of the UO<sub>2</sub> pellets in order to enhance their dimensional stability during the irradiation. [3]

Zinc stearate is frequently used for a lubricant in  $UO_2$  pellet fabrication process. Small amount of Zinc stearate is mixed with  $UO_2$  powder and made to pellets. It is volatilized in the initial stage of sintering and forms a irregular-shape-pore.[4] It is known that  $TiO_2$  is able to accelerate facilitation of grain growth and form a round-shape-pore.

This paper deals with the resintering behavior of  $UO_2$  fuel pellets which contain additives of Zinc stearate and  $TiO_2$ .

#### 2. Experimental and Results

ADU UO<sub>2</sub> powder was mixed with various contents of high purity titania powders for 1 h and then 0.5 wt% zinc stearate was mixed with these powder mixture for 0.5 h in a tumbling mixer. The powder mixture was compacted into a green pellet with a pressure of 300 MPa. Green pellets of UO<sub>2</sub> and UO<sub>2</sub> containing 0.1, 0.2 wt% TiO<sub>2</sub> and 0.5, 1.0 wt% zinc stearate were prepared. These green pellets were sintered at 1730 °C for 4 h in H<sub>2</sub> flowing gas. The resintered pellets were prepared by resintering the sintered pellets at 1700 °C for 24 h in flowing H<sub>2</sub> gas.

The density of the sintered and re-sintered pellets was measured by using an immersion method. Ceramographic samples of re-sintered pellets were prepared by a mounting, grinding, polishing and etching the pellets. The pellet was cut in the axial direction. And then a grinding and polishing process was performed. To observe the grain structure, a thermal etching for the polished samples was carried out at 1250  $^{\circ}$ C for 2h in a CO<sub>2</sub> flowing atmosphere. The microstructure of the samples was observed by an optical microscopy. The grain size of the sample was measured by using the linear intercept method.



Figure 1. The pore structure of ADU UO<sub>2</sub> pellets( $\times$ 200) (a) 0.5 wt% Zinc stearate (b) 0.5 wt% Zinc stearate + 0.1 wt% TiO<sub>2</sub>

Figure 1 shows the pore structure change of Zinc stearate doped  $UO_2$  pellets according to the addition of TiO<sub>2</sub>. The shape of pores in Fig. 1(a) is irregular. Many tiny pore exist in Fig.1(a). However, when the TiO<sub>2</sub> was doped in this pellets, shape of pores become round and the number of micro-pores was remarkably decreased.



Figure 2. The grain structure of ADU UO<sub>2</sub> pellets( $\times$ 200) (a) 0.5 wt% Zinc stearate (b) 0.5 wt% Zinc stearate + 0.1 wt% TiO<sub>2</sub>

The grain structures of resintered  $UO_2$  pellet are shown in Figure 2. The grain size of Zinc stearate doped  $UO_2$  pellet is about 11.5 µm. The grain size of Zinc stearate and TiO<sub>2</sub>-doped  $UO_2$  pellet increased up to about 46.5 µm. This grain size is four times larger than the zinc stearate doped  $UO_2$  pellet. Most of pores were located at the grain boundary in Fig.2(b).

Fig.3 shows the densities of sintered and resintered pellets. Fig. 3(a) shows the resintered density changes of un-doped UO<sub>2</sub> pellets. In spite of the density difference of UO<sub>2</sub> pellets before resintering, the final resintered pellet density was similar to each other. Fig. 3(b) shows the density change of sintered and resintered pellets in zinc stearate doped UO<sub>2</sub> system. In contrast to Fig.3(a), density increased in the resintered pellet is independent to the initial sintered pellet density. Fig. 3(c) shows the sintered and resintered pellet density of zinc stearate and TiO<sub>2</sub> doped UO<sub>2</sub> pellets. The resintered pellet density is the largest in the low density pellets as like in

fig. 3(a). However, resintered pellet density increment is considerably mitigated in these pellets.

## 3. Conclusion

Pores of an irregular shape were formed in Zinc stearate doped  $UO_2$  pellets. Pores of a round shape were formed in TiO<sub>2</sub> doped  $UO_2$  pellet.

Re-sintered density increment was mitigated in the pellets which have irregular shape pore structure. It was found that re-sintered density increment could be controlled by controlling the pore structure of  $UO_2$  pellets. The pore structure of sintered pellet can be controlled by combining the addition of zinc stearate and TiO<sub>2</sub>.

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Figure 3. The density change after re-sintering  $UO_2$  pellets; (a) Pure  $UO_2$  (b) Zinc stearate doped  $UO_2$  (c) 0.5wt% Zinc stearate + TiO<sub>2</sub> doped  $UO_2$