# Effect of a Gas Atmosphere on the Grain Growth of UO2

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### 1. Introduction

The grain and pore structures of a ceramic pellet as a nuclear fuel is one of the most important properties, which is related to the fission gas release and the pellet/clad interaction (PCI) during a irradiation in a reactor [1]. UO<sub>2</sub> or MOX pellets having large grains can be obtained by a control of the sintering parameters and/or by the application of an oxidative sintering process. The pellet properties can also be modified by using sintering additives such as TiO<sub>2</sub>, Cr<sub>2</sub>O<sub>3</sub> and Nb<sub>2</sub>O<sub>5</sub>, and this method has been attempted by various researchers [2,3,4]. Recently, Joung et al. [5] reported that the isothermal sintering of UO<sub>2</sub> compacts in air was possible at a high temperature above 1803K. They confirmed that the sintered UO<sub>2</sub> pellet consisted of a single grain. The oxygen in the air contributes to the grain growth for this sintering process, but we need to understand the oxidation behavior and phase change of the pellet in air at a high temperature.

In this work, the sintering behavior of  $UO_2$  was studied by using both a TGA and an alumina tube furnace to confirm the effect of air on the grain growth of the pellet in the first step of an air sintering. The densification and grain growth of the pellet for the sintering in H<sub>2</sub>-air-H<sub>2</sub> were compared with those for the sintering in CO<sub>2</sub>-air-CO<sub>2</sub>-H<sub>2</sub>. This study demonstrates a sintering process and its sintering conditions for the  $UO_2$  pellets which consist of large grains or a single grain.

#### 2. Experimental

UO<sub>2</sub> powder was produced by the Integrated Dry Route in BNFL co, and it had an O/U ratio of 2.15, an average particle size of 2.2  $\mu$ m, and a specific surface area of  $2.36m^2/g$ . The milling of UO<sub>2</sub> powder was accomplished by using a planetary mill (FRITSCH pulverisette 6). This prepared powder was pressed with a compaction pressure of 300MPa with a die-wall lubrication method and the compacts have green density of 5.8g/cm<sup>3</sup> for UO<sub>2</sub>. Thermogravitic (Cahn, TG171) experiments to observe the O/M ratio changes during the oxidation were carried out in the H<sub>2</sub>-air and CO<sub>2</sub>-air at 1550 °C. The TG was heated up in a  $H_2$  or  $CO_2$ atmosphere and the gas was changed into air at the reaction temperature. The air sintering in a tube furnace was conducted by the following four stages. Firstly, the  $UO_2$  compact was heated up to the sintering temperatures (1530-1700  $^{\circ}$ C) in CO<sub>2</sub>. Secondly, it was soaked for a range of 0~60 min. at the set temperature in air. Thirdly, it was reduced down to  $1200^{\circ}$  C in CO<sub>2</sub>. Fourthly, it was soaked in H<sub>2</sub> at the same temperature for 2h and then cooled down to a room temperature with flowing H<sub>2</sub> to adjust the O/U ratio of UO<sub>2</sub> pellets to 2.00. For the sintering in H<sub>2</sub>-air-H<sub>2</sub>, UO<sub>2</sub> compact was heated up to the sintering temperatures of  $1530^{\circ}$ C, 1600 °C or 1700 °C in H<sub>2</sub> then soaked for 1h in the air. At the soaked temperature, the pellet was reduced in H<sub>2</sub> for 1h. To avoid a reaction between H<sub>2</sub> and air, N<sub>2</sub> gas was purged into the furnace for 1 min. The sintered density of the pellets was measured by the liquid immersion method. In order to observe the microstructures of the UO2 pellets, thermal etching was carried out at 1450  $^{\circ}$ C for 1 hour in CO<sub>2</sub>. The average grain size was determined using the linear intercept method.

#### 3. Results

Thermo gravimetric (TG) curves of  $UO_2$  samples at 1550 °C are shown in Fig. 1. Before flowing air for the  $CO_2$ -air reaction, the O/U ratio of the  $UO_2$  sample was 2.18 and for the H<sub>2</sub>-air reaction it was 2.00. The saturation levels (phase boundary) and oxidation gradients were similar for both the  $CO_2$ -air and H<sub>2</sub>-air reactions.



Fig. 1 TG curves of  $UO_2$  samples reacted in the  $H_2$ -air and  $CO_2$ -air atmosphere.

The density and grain size of the UO<sub>2</sub> pellets sintered by the H<sub>2</sub>-air-H<sub>2</sub> process are compared with those for the CO<sub>2</sub>-H<sub>2</sub> sintering process in Table. 1. Sintered density at 1530 °C in H<sub>2</sub>-air-H<sub>2</sub> is a little lower than that of the other pellets. The grain size was continuously increased with the sintering temperature, but an abnormal grain growth did not appear in the H<sub>2</sub>air-H<sub>2</sub> process. For the CO<sub>2</sub>-air-CO<sub>2</sub>-H<sub>2</sub> sintering process, abnormal grain growth was observed in the pellet when a sintering time in air was longer than 5min.

| Gas Step conditions                                  | Sintering     |                | Sintered           | Grain        |
|--|---------------|----------------|--------------------|--------------|
|  | Temp.<br>(°C) | Time<br>(min.) | density<br>(%T.D.) | size<br>(um) |
| H <sub>2</sub> -Air-H <sub>2</sub>                   | 1530          | 10             | 97.1               | 5            |
|  | 1600          | 60             | 99.1               | 72           |
|  | 1700          | 60             | 99.0               | 123          |
| CO <sub>2</sub> -Air-CO <sub>2</sub> -H <sub>2</sub> | 1530          | 10             | 98.2               | 1500         |

Table 1. Properties of the  $UO_2$  pellets sintered in  $H_2$ -Air- $H_2$  and  $CO_2$ -air- $CO_2$ - $H_2$ .

The microstructure of the pellet sintered for 6 min in air at 1530  $^{\circ}$ C with CO<sub>2</sub>-air-CO<sub>2</sub>-H<sub>2</sub> process is shown in Fig. 2. It shows a duplex grain structure, which consists of some large grains surrounded by many fine grains.



Fig. 2 Microstructures of  $\mathrm{UO}_2$  pellet sintered for 6min. with  $\mathrm{CO}_2\text{-air-}\mathrm{CO}_2\text{-}\mathrm{H}_2$  process.

The microstructures of the UO<sub>2</sub> pellets sintered for 60min. in air at (a) 1530 °C, (b) 1600 °C and (c) 1700 °C in the H<sub>2</sub>-air-H<sub>2</sub> process and for 10min. in air at (a) 1530 °C in the CO<sub>2</sub>-air-CO<sub>2</sub>-H<sub>2</sub> process air air shown in Fig. 3. The grain size was very fine when the pellet was sintered at 1530 °C in H<sub>2</sub>-air-H<sub>2</sub>, but an order of millimeters for the CO<sub>2</sub>-air-CO<sub>2</sub>-H<sub>2</sub> process at the same sintering temperature.



Fig. 3 Microstructures of UO<sub>2</sub> pellets sintered at (a) 1530 $^{\circ}$ C, (b) 1600 $^{\circ}$ C and (c) 1700 $^{\circ}$ C in H<sub>2</sub>-air-H<sub>2</sub> and at (a) 1530 $^{\circ}$ C in CO<sub>2</sub>-air-CO<sub>2</sub>-H<sub>2</sub>.

From this result, the difference of the grain growth in  $H_2$ -air- $H_2$  and in  $CO_2$ -air- $CO_2$ - $H_2$  seems to have originated from the O/U ratio just before flowing the air at the sintering temperature. The grain growth in the  $CO_2$ -air- $CO_2$ - $H_2$  process was accelerated by the abnormal growth caused by the hyperstoichiometric O/U ratio of the pellet at the initial sintering step.

## 4. Conclusion

The sintering behavior of  $UO_2$  samples was studied using a thermergravity analyzer and a tube furnace at sintering temperatures from 1530 °C to 1700 °C in air. The following conclusions were obtained from this study:

1. The saturation levels and oxidation gradients of the samples oxidized in  $CO_2$ -air and in  $H_2$ -air are similar.

2. The sintered density in  $H_2$ -air- $H_2$  and in CO<sub>2</sub>-air-CO<sub>2</sub>- $H_2$  is over 97%. An abnormal grain growth was observed in the CO<sub>2</sub>-air-CO<sub>2</sub>- $H_2$  process.

3. The difference in the grain growth between the  $H_2$ air- $H_2$  and  $CO_2$ -air- $CO_2$ - $H_2$  process originated from the hyperstoichiometric O/U ratio of a sample just before a sintering in air for the latter process.

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