## Fabrication of sintered duplex burnable absorber pellets

2004

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## Abstract

Crack formation has been investigated in a duplex burnable absorber pellet, which is composed of two different materials;  $UO_2-10wt\%Gd_2O_3$  in core and  $UO_2-2wt\%Er_2O_3$  in shell. Cracks propagated from the core-shell interface to the both region in the undoped pellet. The crack formation could be attributed to the backstress, which results from the differential densification between the core and the shell. Small amounts of MnO considerably affect the densification rate of  $UO_2-10wt\%Gd_2O_3$ . The densification rate of  $UO_2-10wt\%Gd_2O_3$  was accelerated with the content of MnO. The sintered core-shell interface was joined without cracks by adding 0.1wt% MnO to the core material.

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 $UO_2$ 가 (gadolinium) .  $UO_2$ 가 (erbium) 가  $UO_2$ . 가 Gd 가 Er •  $(U,Gd)O_2$  $(U,Er)O_2$ , (U,Gd)O<sub>2</sub> . UO<sub>2</sub>  $(U,Er)O_2$  $Gd_2O_3$  $UO_2$ - $Gd_2O_3$  $UO_2$ - $Er_2O_3$  $Er_2O_3$ . 가 1600°C-1800°C 2-4 Gd Er UO<sub>2</sub> 가 [1]  $(U,Gd)O_2$  $(U,Er)O_2$ . 가 . , 가 (duplex pellet) . 가 .[2]  $UO_2$ -2wt% $Er_2O_3$  $UO_2$  $UO_2$ - $10wt\%Gd_2O_3$  $UO_2$ 1200–1500°C  $Gd_2O_3$ 가  $UO_2$  $Gd_2O_3$ .  $Gd_2O_3$ .[3-5] 가 . 가 2.  $UO_2$  $Er_2O_3$ 2wt% tubular  $UO_2$ 1 . 가 1 tubular (MnO)  $Gd_2O_3$ 10wt% 10 . MnO가 가  $Gd_2O_3$ MnO  $Gd_2O_3$ 12 .

1  $UO_2-2wt\% Er_2O_3$  $UO_2-10wt\%Gd_2O_3$ 가  $3 \text{ ton/cm}^2$ . . 1700°C, H<sub>2</sub>-3%CO<sub>2</sub> 4 Dilatometer 8 mm 2.85 g 10 mm . 1650°C 5 K/min 가 dilatometer push-rod . 가 가 LVDT , 가 cycle . 3. 2  $2wt\% Er_2O_3$  7  $UO_2$ UO<sub>2</sub>-10wt% Gd<sub>2</sub>O<sub>3</sub> 3 . 가 0.1 wt% MnO MnO 가 . . 가 MnO 4 UO<sub>2</sub>-10wt%Gd<sub>2</sub>O<sub>3</sub>, .  $UO_2$ -2wt% $Er_2O_3$ .  $UO_2\text{-}10wt\%Gd_2O_3$ 1510°C  $UO_{2}-$ 

2wt%Er<sub>2</sub>O<sub>3</sub> 1220°C 7t . /

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		가								가
MnO 가		$UO_2-10wt\% Gd_2O_3$				$UO_2-2wt\% Er_2O_3$				
				151(			Mn	0	가	
$UO_2$ -10Wt%Gd <sub>2</sub> O <sub>3</sub>				1510	50					
MnC	)가	가	UO <sub>2</sub> -10	)wt%Gd <sub>2</sub> O <sub>3</sub>			가		가	
				가	0.	1 wt%	MnO	가		
				가 1280	)°C					
U			$UO_2-2wt\% Er_2O_3$			220°C				
			MnO	0.1 wt%		가				

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4.  $UO_2-10wt\%Gd_2O_3$ , UO<sub>2</sub>-2wt%Er<sub>2</sub>O<sub>3</sub> 가 dilatometer  $UO_2$ -2wt% $Er_2O_3$  $UO_2$  $UO_2\text{-}10wt\%Gd_2O_3$  $UO_2$  $Gd_2O_3$ 1200-1500°C 가 . 가  $UO_2-10wt\%Gd_2O_3$ MnO 가 dilatometer . MnO 가 가 가 가  $UO_2-Gd_2O_3$ 0.1 wt% MnO

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**3.** R. Manzel and W. O. Dörr, "Manufacturing and Irradiation Experience with UO<sub>2</sub>/Gd<sub>2</sub>O<sub>3</sub> Fuel," *Am. Ceram. Soc. Bull.*, **59** 601-603 (1980).

- **4.** S. M. Ho and K. C. Radford, "Structural Chemistry of Solid Solutions in the UO<sub>2</sub>-Gd<sub>2</sub>O<sub>3</sub> system," *Nucl. Tech.*, **73** 350-360 (1986).
- **5.** R. Yuda and K. Une, "Effect of Sintering Atmosphere on the Densification of UO<sub>2</sub>-Gd<sub>2</sub>O<sub>3</sub> compacts," *J. Nucl. Mater.*, **178** 195-203 (1991).





 $2. \ UO_2 - 10wt\% Gd_2O_3/UO_2 - 2wt\% Er_2O_3$ 



3. 0.1wt% MnO 7 UO<sub>2</sub>-10wt%Gd<sub>2</sub>O<sub>3</sub>/UO<sub>2</sub>-2wt%Er<sub>2</sub>O<sub>3</sub>



4. MnO 기