





### Abstract

Grain growth behaviors have been investigated in the  $UO_2$  pellets which comprise IDR- and AUC-derived uranium dioxide powders and various seed crystals. Four different seed crystals were made depending on the starting powders and the sintering conditions and then embedded in IDR- and AUC-derived uranium dioxide compacts. Compacts were sintered at 1700°C in  $H_2$  atmosphere or at 1100°C in  $CO_2$  atmosphere for 4 h. Almost all samples showed normal grain growth behaviors. However, the abnormal grain growth was observed when AUC  $UO_2$  compact containing  $H_2$ -sintered seed was sintered in  $CO_2$  atmosphere. This result may be attributed to the powder characteristics of the matrix and the O/U ratio gradient in the interface region between the matrix and seed crystal.

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2

가 . .

, 7ト UO<sub>2</sub> , . 1700°C, 4 8 μm

UO2 フト, O/U . フト . フト . O/U

2.0 2.15 . O/U 7

.

1.

# 2.

## 2-1.

$UO_2$ 1 ton/cm <sup>2</sup>				. IDR-, AUC UO <sub>2</sub> CIP(Cold Isotatic Press) 3 ton/cm <sup>2</sup>			
1900 4	, AUC	,	, 1500	IDR	・ , アト	4 가	,
			1mm	2mm			

## 2-2.

	12.02φ	1 ton/ <b>cm</b> <sup>2</sup>		
	CIP(Cold Isotatic Press)	3 ton/cm <sup>2</sup>		
1100 ,	4	,		가
1050				

. , 1700 , 4 .

1300 ,

 3.

 1

 . IDR, AUC
 UO2

 7, 1900°C, 1500°C, 1500°C, 4

 4
 .

רי 1700°C, , 1100°C, ,

.

가 AUC UO<sub>2</sub> 2가 • O/U 가 . O/U . O/U 3 1700°C 4 . 2-3 4 , 1100°C 4

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. ,

# 가

 Srolovitz [5]

 7 +
 7 +

 monte carlo
 .
 BNFL [6]
 UO2

 3
 .
 .

, 1100°C 4 . IDR UO<sub>2</sub>

. , AUC UO<sub>2</sub>

μm	2 AU	С UO <sub>2</sub>	1100°C		
. , 0/0	J	UO <sub>2</sub>			가
7	TGA 6	CO <sub>2</sub> -0.28%C O/U	O , 1200° O/U	C 25	0/U 0/U 6
	O/U		가	가,	가
		AUC UO <sub>2</sub>	• •		O/U
O/U 가 AUC Song [4] 4	C UO <sub>2</sub> . Song AUC UO <sub>2</sub>	[4] 800°C		가 가	
가			AUC UO <sub>2</sub>		O/U O/U
<b>4.</b> UO <sub>2</sub>		·	가, O/U	가	O/U 가
O/U		가			,

AUC UO<sub>2</sub>

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a) AUC sintered (1100 , CO<sub>2</sub>, 4h)
 b) IDR sintered (1100 , CO<sub>2</sub>, 4hr)
 c) AUC sintered (1700 , H<sub>2</sub>, 4h)
 d) IDR sintered (1700 , H<sub>2</sub>, 4hr)
 2.



a) AUC matrix AUC(H<sub>2</sub>, 1900) seed sintered 1700
 b) AUC matrix IDR(H<sub>2</sub>, 1900) seed sintered 1700
 c) IDR matrix AUC(H<sub>2</sub>, 1900) seed sintered 1700
 d) IDR matrix IDR(H<sub>2</sub>, 1900) seed sintered 1700
 3. H<sub>2</sub> /H<sub>2</sub>



a) AUC matrix AUC(CO<sub>2</sub>, 1500 ) seed sintered 1100
c) IDR matrix AUC(CO<sub>2</sub>, 1500 ) seed sintered 1100

b) AUC matrix IDR(CO<sub>2</sub>, 1500 ) seed sintered 1100
d) IDR matrix IDR(CO<sub>2</sub>, 1500 ) seed sintered 1100

4. CO<sub>2</sub> /CO<sub>2</sub>



a) AUC matrix AUC(CO<sub>2</sub>, 1500 ) seed sintered 1700
b) AUC matrix IDR(CO<sub>2</sub>, 1500 ) seed sintered 1700

5. H<sub>2</sub> /CO<sub>2</sub>



**a,b**) AUC matrix AUC(H<sub>2</sub>, 1900 ) seed sintered 1100 **e**) IDR matrix AUC(H<sub>2</sub>, 1900 ) seed sintered 1100

c,d) AUC matrix IDR(H<sub>2</sub>, 1900 ) seed sintered 1100
f) IDR matrix IDR(H<sub>2</sub>, 1900 ) seed sintered 1100

6.  $CO_2$  /H<sub>2</sub>



