

## Effect of temperature and pressure on the overall heat transfer coefficient in VHTR-based SI process heat exchangers

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### 1. Introduction

The sulfur-iodine (SI) cycle and Westinghouse sulfur hybrid cycle, combined with a very high temperature gas-cooled reactor (VHTR), are well-known as feasible technologies for hydrogen production [1]. The SI process consists of a Bunsen reactor; H<sub>2</sub>SO<sub>4</sub>, SO<sub>3</sub>, and HI decomposers; and a HI pre-heater. The overall heat transfer coefficient of the process heat exchanger (PHE) used in the SI process is a very important factor when sizing the PHE.

In this paper, a sensitivity analysis on the overall heat transfer coefficient has been carried out as a function of operation temperature and pressure.

### 2. Process Heat Exchangers and Used Equations

As shown in Fig. 1, the process gas in the tube side of shell-and-tube type equipment is heated by high-temperature helium in the shell side.

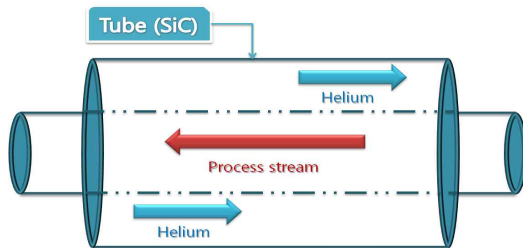


Fig. 1. PHE counter current flow model.

The target components in the VHTR-based SI process are a H<sub>2</sub>SO<sub>4</sub> decomposer, SO<sub>3</sub> decomposer, and HI pre-heater.

Table I: Equipment Parameter

Device		H <sub>2</sub> O	H <sub>2</sub> SO <sub>4</sub>	SO <sub>3</sub>	SO <sub>2</sub>	O <sub>2</sub>
SO <sub>3</sub> Decomposer	Inlet mole flow rate (mol/s)	489.78	6.68	444.62	0	0
	Inlet temperature (K)	Process stream = 1023, He = 1183				
	Outlet mole flow rate (mol/s)	503.35	2.16	163.57	285.62	142.81
	Outlet temperature (K)	Process stream = 1123, He = 1085				
H <sub>2</sub> SO <sub>4</sub> Decomposer	Inlet mole flow rate (mol/s)	228.06	277.41	173.90	0	0
	Inlet temperature (K)	Process stream = 740, He = 1085				
	Outlet mole flow rate (mol/s)	498.78	6.68	444.62	0	0
	Outlet temperature (K)	Process stream = 1023, He = 959.7				

Device		H <sub>2</sub> O	I <sub>2</sub>	HI	H <sub>2</sub>
HI Pre-heater	Inlet mole flow rate (mol/s)	1294.06	234.91	978	0
	Inlet temperature (K)	Process stream = 547.4, He = 842.3			
	Outlet mole flow rate (mol/s)	1294.06	234.91	978	0
	Outlet temperature (K)	Process stream = 723, He = 743			

The overall heat transfer coefficient can be expressed as follows [2].

$$\frac{1}{U} = \frac{1}{h_o} + \frac{1}{h_i(D_i/D_o)} + \frac{1}{h_w} + \frac{1}{h_s} \quad (1)$$

$$h_i = 0.125 \frac{\lambda_i}{D_i} \left( \frac{D_p G_i}{\mu_i} \right)^{0.75} \quad 0.35 < \frac{D_p}{D_i} < 0.60 \quad (2)$$

$$h_i = 0.813 \frac{\lambda_i}{D_i} \exp(-6D_p/D_i) \left( \frac{D_p G_i}{\mu_i} \right)^{0.9} \quad \frac{D_p}{D_i} < 0.35 \quad (3)$$

$$h_o = \frac{0.273c_p G_o}{(c_p \mu_o / \lambda_o)^{2/3} (D_o G_o / \mu_o)^{0.365}} \quad (4)$$

$$h_w = \frac{2\lambda_t}{(D_o - D_i)} \quad (5)$$

U : overall heat transfer coefficient [W/(m<sup>2</sup>·K)]

h<sub>o</sub> : outside heat transfer coefficient [W/(m<sup>2</sup>·K)]

h<sub>i</sub> : inside heat transfer coefficient [W/(m<sup>2</sup>·K)]

D<sub>i</sub> : internal diameter of tube [m]

D<sub>o</sub> : external diameter of tube [m]

D<sub>p</sub> : diameter of packing material [m]

C : conversion factor (British units to MKS units)

h<sub>w</sub> : heat transfer across tube wall [W/(m<sup>2</sup>·K)]

h<sub>s</sub> : fouling heat transfer coefficient [W/(m<sup>2</sup>·K)]

G<sub>o</sub> : external superficial mass flow rate per unit area [kg/(s·m<sup>2</sup>)]

G<sub>i</sub> : internal superficial mass flow rate per unit area [kg/(s·m<sup>2</sup>)]

λ<sub>i</sub> : inside thermal conductivity [W/(m·K)]

λ<sub>o</sub> : outside thermal conductivity [W/(m·K)]

λ<sub>t</sub> : thermal conductivity of tube [W/(m·K)]

μ<sub>i</sub> : internal viscosity of fluid [Pa·s]

μ<sub>o</sub> : external viscosity of fluid [Pa·s]

c<sub>p</sub> : heat capacity of fluid [kJ/(kg·K)]

### 3. Results and Discussion

Figs. 2, 3, and 4 show the temperature sensitivities of the overall heat transfer coefficient in the H<sub>2</sub>SO<sub>4</sub> and SO<sub>3</sub> decomposers and HI pre-heater.

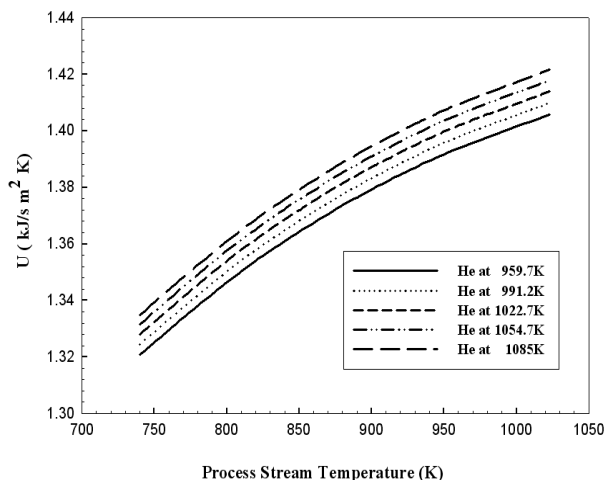


Fig. 2. Overall heat transfer coefficient as a function of helium temperature in a  $H_2SO_4$  decomposer.

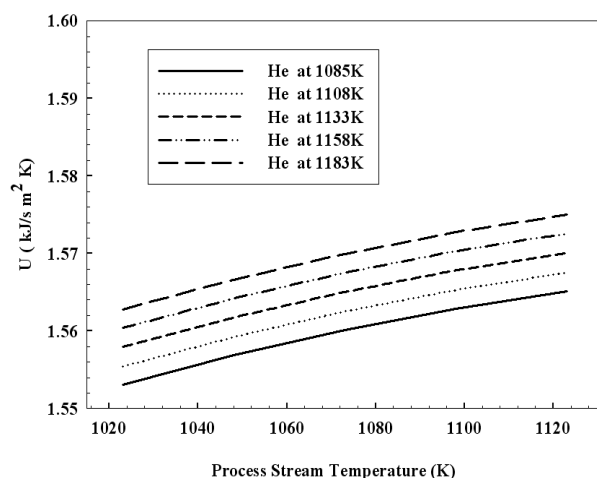


Fig. 3. Overall heat transfer coefficient as a function of helium temperature in a  $SO_3$  decomposer.

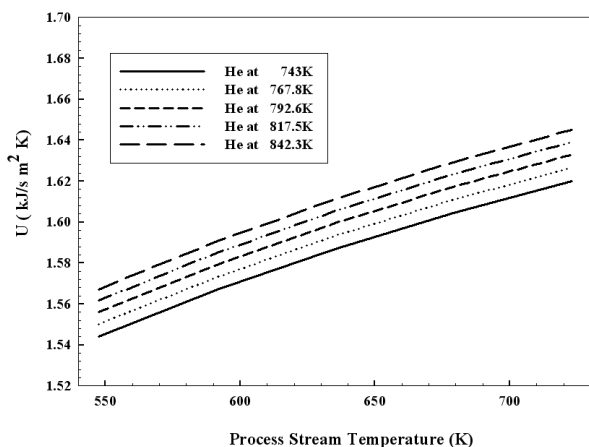


Fig. 4. Overall heat transfer coefficient as a function of helium temperature in a HI pre-heater.

Figs. 5 and 6 show the pressure sensitivities of the overall heat transfer coefficient and internal heat transfer coefficient in the  $SO_3$  decomposer, respectively; The  $H_2SO_4$  decomposer and HI pre-heater have the same trend as the  $SO_3$  decomposer.

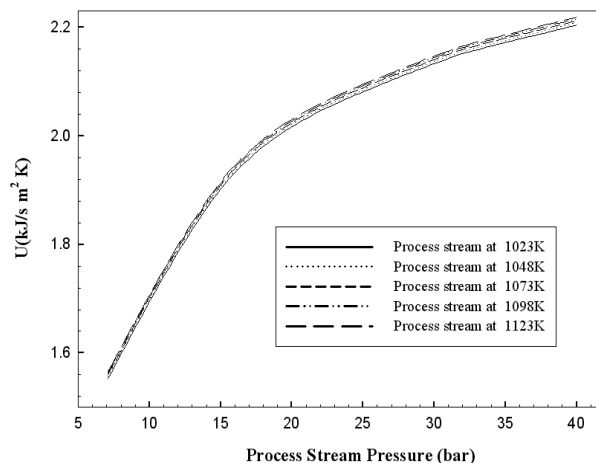


Fig. 5. Overall heat transfer coefficient as a function of process stream pressure in a  $SO_3$  decomposer.

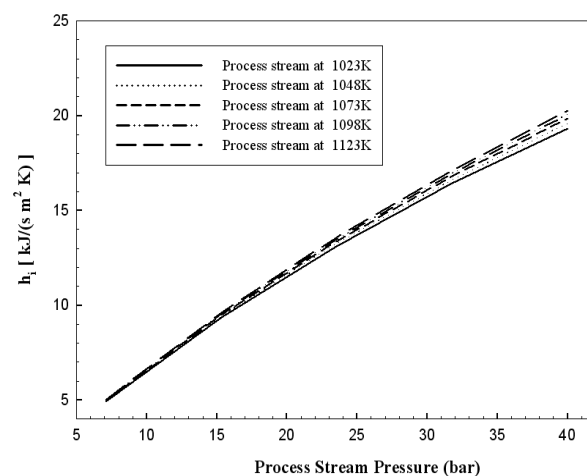


Fig. 6. Internal heat transfer coefficient as a function of process stream pressure in a  $SO_3$  decomposer.

#### 4. Summary

The effects of operation temperature and pressure on the overall heat transfer coefficient have been analyzed. The overall heat transfer coefficient is increased with an increase in the operation temperature and pressure in the process heat exchangers installed inside the  $H_2SO_4$  and  $SO_3$  decomposers and the HI pre-heater.

#### Acknowledgments

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- [2] Jakob M. Elements Heat Transfer, 3rd edition, vol. 2, Wiley, New York, 1957.