

## U<sub>3</sub>O<sub>8</sub> 가 UO<sub>2</sub>

### Grain Growth in U<sub>3</sub>O<sub>8</sub>-seeded UO<sub>2</sub>

150

UO<sub>2</sub> U<sub>3</sub>O<sub>8</sub> 5 wt% 가  
 . UO<sub>2</sub> 5 wt% U<sub>3</sub>O<sub>8</sub> 가  
 1300 °C 1700 °C 가 0 4  
 . 1300 °C 가 가 가  
 가 가 가 가 1700 °C  
 가 . , 1600 °C  
 1700 °C 가 UO<sub>2</sub> 2

#### Abstract

Densification and grain growth have been investigated in 5 wt% U<sub>3</sub>O<sub>8</sub> seeded UO<sub>2</sub> and compared with those of the common UO<sub>2</sub> pellet. UO<sub>2</sub> compacts and 5 wt% U<sub>3</sub>O<sub>8</sub> seeded UO<sub>2</sub> compacts were sintered at 1300-1700 °C for 0h to 4 h. Density and grain size of the sintered pellets were measured by the water immersion method and the image analyzer. The seeded pellet has a slightly lower density during the intermediate stage. However, the differences between two pellets decrease up to less than 0.5 %TD with increasing the sintering temperature. The grain sizes of two kinds of pellets are similar until 1600 °C but that of the seeded pellet rapidly increases with increasing the sintering temperature.

# 1.

Interaction) 가 . PCI (Pellet Clad  
 가 UO<sub>2</sub>  
 . [1] 가  
 . Turnbull [2] 가  
 , 20 µm 1700 °C 40  
 . [3] Cr<sub>2</sub>O<sub>3</sub>, Nb<sub>2</sub>O<sub>5</sub>, TiO<sub>2</sub>, SiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub> 가  
 가 . [4-10] U<sub>3</sub>O<sub>8</sub>  
 가 UO<sub>2</sub> 가 . [11]  
 가 가  
 UO<sub>2</sub> U<sub>3</sub>O<sub>8</sub> 가 가 UO<sub>2</sub>  
 U<sub>3</sub>O<sub>8</sub>  
 가  
 UO<sub>2</sub> U<sub>3</sub>O<sub>8</sub> 가  
 U<sub>3</sub>O<sub>8</sub>  
 가

# 2.

. . . . .  
 ton/cm<sup>2</sup> . . . . .  
 . . . . .  
 °C . . . . .  
 1700 °C . . . . .  
 1700 °C . . . . .

ADU-UO <sub>2</sub>	UO <sub>2</sub>	400 °C	4	U <sub>3</sub> O <sub>8</sub>
U <sub>3</sub> O <sub>8</sub>	1300 °C	4		1.5
5 wt%가	ADU-UO <sub>2</sub>		ADU-UO <sub>2</sub>	5 wt%
가	UO <sub>2</sub>	3 ton/cm <sup>2</sup>		1300
°C	1700 °C			
1700 °C			1700 °C	1      4

2  
 analyzer 1  $\mu\text{m}$ -alumina 300 80HNO<sub>3</sub>-20H<sub>2</sub>O<sub>2</sub> 30 Image

3.

Fig. 1(a) UO<sub>2</sub> 400 °C 4 U<sub>3</sub>O<sub>8</sub> SEM U<sub>3</sub>O<sub>8</sub>  
 1300 °C 4 1.5 ton/cm<sup>2</sup> 가 U<sub>3</sub>O<sub>8</sub>  
 6.3  $\mu\text{m}$  chip 가  
 UO<sub>2</sub> 가 Fig. 2  
 1300 °C 가  
 67 %TD 가 UO<sub>2</sub>  
 가 1400 °C 5 %TD  
 1700 °C, 4 0.5 %TD  
 98 %TD  
 Fig. 3 UO<sub>2</sub> 1600 °C  
 sub-micron 가 1700 °C가 가 1.5  $\mu\text{m}$   
 4 7  $\mu\text{m}$  U<sub>3</sub>O<sub>8</sub> 가 , Fig. 4  
 1600 °C sub-micron 가  
 가 stacking fault twin U<sub>3</sub>O<sub>8</sub>  
 1700 °C가 가 4.6  $\mu\text{m}$  4 14  $\mu\text{m}$   
 Fig. 5 1600 °C  
 UO<sub>2</sub> 가 sub-micron 가 가  
 가 10  
 , Fig. 3 4 가 , 1600  
 °C 가  
 1700 °C가 UO<sub>2</sub> 1700 °C, 0  
 1.6  $\mu\text{m}$  가 UO<sub>2</sub> 4.5  $\mu\text{m}$

. ,  $\text{UO}_2$  1700 °C, 4 가  
 14  $\mu\text{m}$   $\text{UO}_2$  가  
 7  $\mu\text{m}$  .  
 가 가  
 . , 가  $\text{UO}_2$  가 ,  
 가 가  $\text{U}_3\text{O}_8$   
 가 , 가  $\text{U}_3\text{O}_8$  .  
 가  $\text{UO}_2$  ,  
 $\text{UO}$  가  $\text{U}_3\text{O}_8$  가 .  
 가 , 가 가 .  
 가  
 가  
 Fig. 6 가 1650 °C, 0 .  
 가

. 1700 °C가  
 가  
 가  
 가  
 가 Twin  
 가  
 .[12]  $\text{U}_3\text{O}_8$  가  $\text{UO}_2$   
 가

#### 4.

$\text{UO}_2$   $\text{U}_3\text{O}_8$  5 wt% 가  
 $\text{UO}_2$  5 wt%  $\text{U}_3\text{O}_8$  가  
 1300 °C 1700 °C 가 0 4 1300  
 °C 가 가 가 가  
 가 가 1700 °C 가  $\text{U}_3\text{O}_8$  5  
 wt% 가 1600 °C  
 1700 °C 가  $\text{UO}_2$  2  
 4 2 .

1. A. H. Booth, AECL 496 (1957).
2. J. A. Turnbull, J. Nucl. Mater., 50 (1974) 62-68.
3. K.W. Song et al, J. Kor. Nucl. Soc. 26 (1994) 484.
4. I. Amato, R. L. Colombo, A. P. Balzari, J. Nucl. Mater., 18 (1966) 252.
5. J. B. Ainscough, F. Rigby, S. C. Osborn, J. Nucl. Mater. 52 (1974) 191.
6. H.J. Matzke, J. Nucl. Mater. 30 (1969) 26.
7. H. Assmann, W. Dorr, G. Gradel, G. Maier, M. Peehs, J. Nucl. Mater. 98 (1981) 216.
8. J.B. Ainscough, L.F.A. Raven, P.T. Sawbridge, "Fission Gas Retentive UO<sub>2</sub> Fuels," in Fabrication of Water Reactor Fuel Elements, P.53, IAEA-SM-233/16 (1979).
9. K.C. Radford, J.M. Pope, J. Nucl. Mater., 116 (1983) 305.
10. K. W. Lay, J. Am. Ceram. Soc., 51[7], (1968) 373-376.
11. K.W. Song et al, J. Nucl. Sci. & Tech., Supplement 3 (2002) 838-841.
12. Y.S. Yoo et al., J. Eur. Ceram. Soc., 17 (1997) 805-811.

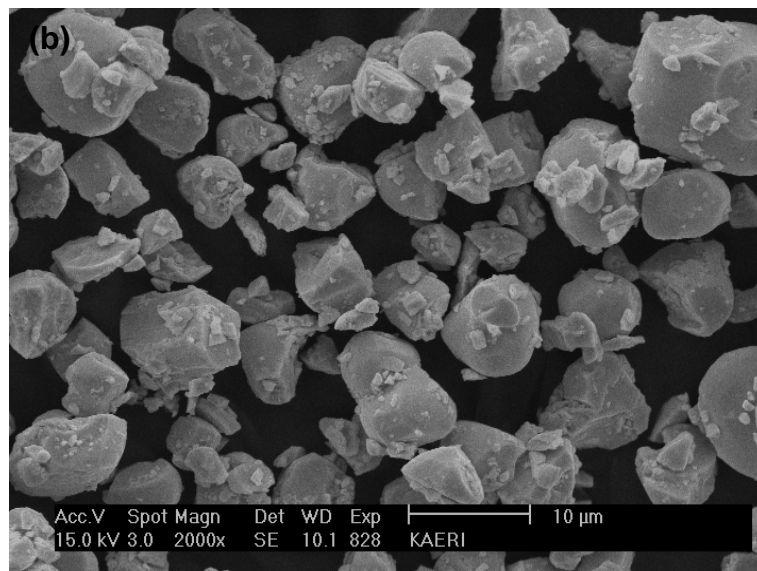
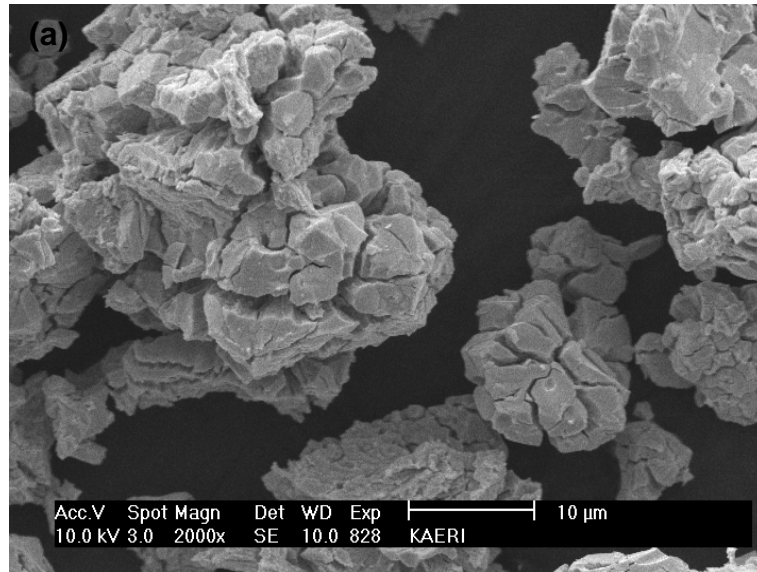


Fig. 1. SEM images of (a) raw  $U_3O_8$  powder and (b)  $U_3O_8$  seed.

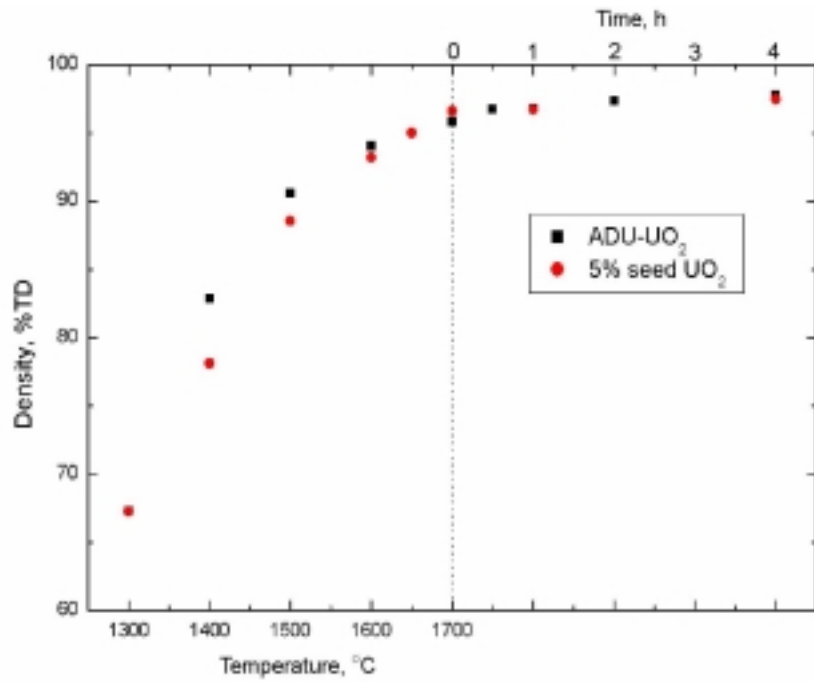


Fig. 2. Variations in relative density for ADU-UO<sub>2</sub> and 5 wt% seeded UO<sub>2</sub>.

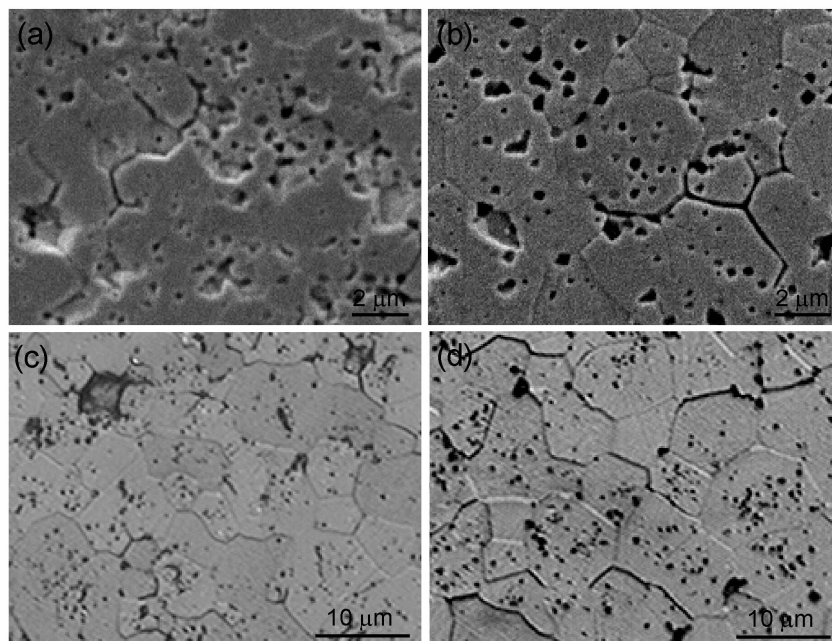


Fig. 3. Microstructures of ADU-UO<sub>2</sub> samples sintered at (a) 1600 °C for 0 h, (b) 1700 °C for 0 h, (c) 1700 °C for 1 h and (d) 1700 °C for 4 h.

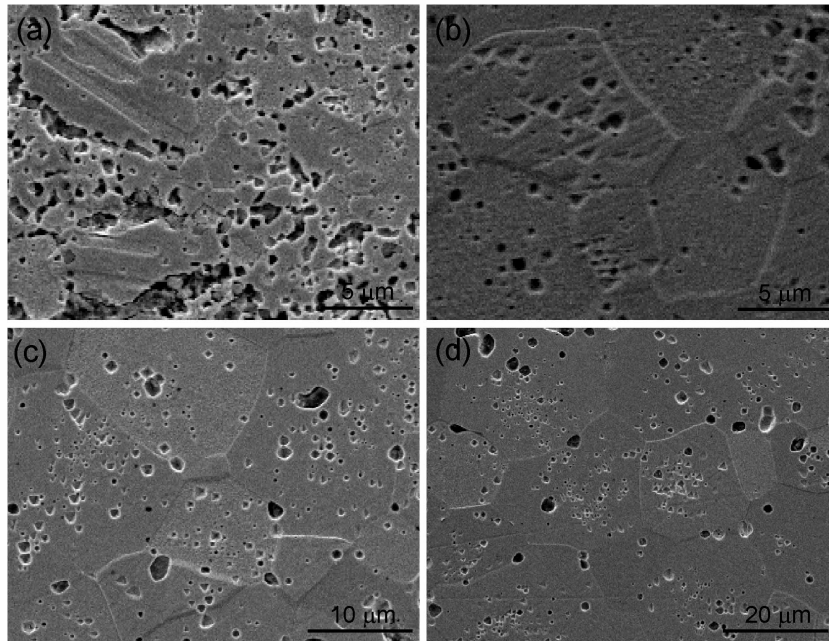


Fig. 4. Microstructures of 5 wt% seeded  $\text{UO}_2$  samples sintered at (a) 1600 °C for 0 h, (b) 1700 °C for 0 h, (c) 1700 °C for 1 h and (d) 1700 °C for 4 h.

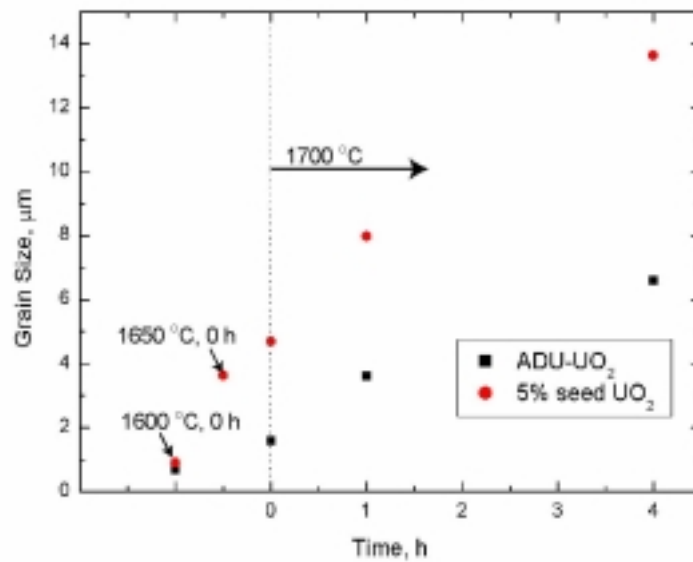


Fig. 5. Variations in average grain size for ADU- $\text{UO}_2$  and 5 wt% seeded  $\text{UO}_2$ .



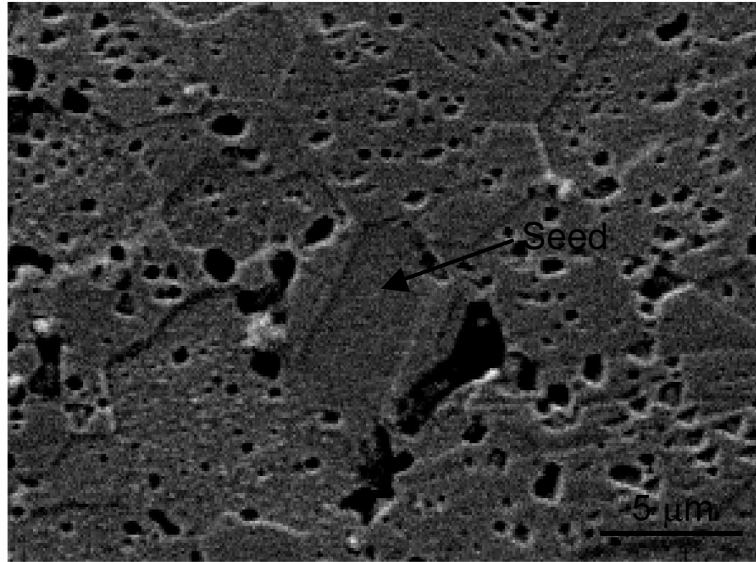


Fig. 6. Microstructures of 5 wt% seeded UO<sub>2</sub> sintered at 1650 °C for 0 h.