

Fabrication and Properties of Metal Matrix Composites as a Neutron Absorber Material of the Spent Nuclear Fuel Dry Storage System

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1. Introduction

Dry storage systems have many advantages such as transportability, expandability of capacity, reduced management, and passive safety. To successfully manage the criticality and decay heat of spent fuel, neutron absorption and heat dissipation are important aspects. B₄C/Al metal matrix composites (MMC) are used as basket materials that contain SNF assembly [1]. Conventional B₄C/Al MMC is fabricated by Powder Metallurgy (P/M) [1-3]. In this study, a new technique is introduced to fabricate B₄C/Al MMC using compact melting & pressing. In addition, the feasibility of the new material, Gd₂O₃/Al MMC as a dry storage basket material, was investigated. Gd₂O₃ was selected because of its large neutron absorption cross section that can efficiently manage the criticality with a small amount of reinforcement.

2. Review of conventional basket materials

2.1. Cadmium

Cadmium is a good shielding material because it has large thermal neutron absorption cross section and good mechanical properties [4]. A comparison between the thermal absorption cross section of Cadmium and other neutron absorbers is listed in Table 1. Nevertheless, Cadmium, which is poisonous and dangerous for the health of workers during the fabrication, must be sealed to avoid leakage in use.

Table 1. Thermal absorption cross-section of isotopes

Isotopes	Thermal absorption cross-section, δ [barn]
B-10	200
Cd-113	30000
Gd-157	254000

2.2. Boron-containing plastics

Polyethylene and polypropylene are commonly used for the matrix of boron-containing plastics because they have good processability. However, boron-containing plastics have poor mechanical properties such as low toughness [5].

2.3. Bohler material (Boron-alloyed stainless steels)

Boron steel can hardly meet the demand of the practical applications due to the limitation of boron content [6].

2.4. Boral, Boralyn (B₄C/Al MMC)

B₄C can capture Helium that is produced by neutron absorption of boron nuclide because of its particular crystal structure [3] [7]. Therefore, B₄C is proper to be a neutron absorbing materials in the basket. In addition, heat dissipation is an important factor to choose the basket material. Aluminum has a high thermal conductivity therefore, B₄C/Al MMC is widely used as a basket material. When the mass fraction of B₄C is changed from 5% to 20% in B₄C/Al composites, its toughness decreases and its hardness increases [3]. Also, due to its lower neutron absorption cross-section when compared to Cd, a 5 mm B₄C/Al neutron absorber with high B₄C content ($\geq 30\%$) achieves neutron shielding properties similar to a 0.5 mm Cd plate by neutron transmission testing results [3]. It is very inefficient in terms of storage capacity in a limited area.

3. Design and experimental preparation

3.1. Fabrication of B₄C/Al MMC with compact melting & pressing

Porosity is usually increased when fabricating MMC with a high volume fraction. Therefore, to reduce the porosity of MMC, a new technique, compact melting & pressing, was used to make a low porosity MMC even with small size reinforcement and a high volume fraction.

3.2. Design of Gd₂O₃/Al MMC

In this study, 5, 10, 15, 20, 30, and 40 vol. % Gd₂O₃ particle-reinforced aluminum MMCs were investigated. 7075Al powder was used as matrix, Gd₂O₃ particle size is around 10 μ m. It was also fabricated by compact melting & pressing. Theoretical density of each sample is shown in Table 2 and the density can be calculated using equation (1).

$$\rho_c = \frac{1}{\frac{x\%}{\rho_p} + \frac{1-x\%}{\rho_m}} \quad (1)$$

where $x\%$ is the mass fraction of Gd₂O₃, ρ_c is the theoretical density of Gd₂O₃ composite, ρ_p and ρ_m are the densities of Gd₂O₃ and Al, respectively.

The absorption and attenuation relationship for Gd₂O₃/Al composite can be expressed in the following equation (equation (2)) [8].

$$I = I_0 e^{-Nh\sigma_a} \quad (2)$$

Table 2. Composition and density of MMC

Specimen	Gd [vol.%]	Al [vol.%]	Density [g/cm ³]
S01	5	95	3.02
S02	10	90	3.24
S03	15	85	3.45
S04	20	80	3.67
S05	30	70	4.09
S06	40	60	4.51
S07	50	50	4.94

where I_0 and I are the intensities of the incoming and outgoing neutrons, respectively, N is the atomic nuclear number per cubic centimeters, h is the thickness of the absorber, and σ_a is the neutron absorbing cross section. σ_a can be calculated by the volume percentage of each component and the thermal neutron absorbing cross sections of Gd and Al, which are 254,000 barns and 0.23 barn as shown in the following equations [3] [9] [10].

$$h = \frac{-\ln I/I_0}{N\sigma_a} \quad (3)$$

$$N = 2 \times \frac{x\rho_c}{M_{Gd_2O_3}} \times N_A \times A_{157Gd} \quad (4)$$

Where $M_{Gd_2O_3}$ is the molar mass of Gd_2O_3 , N_A is Avogadro's number, and A_{157Gd} is the natural abundance of 157-Gd, which is 15.65% [10].

Neutron transmittance of the 0.5 mm Cd plate $I/I_0 = 0.004\%$, and 3.5 mm 20wt.% B_4C/Al MMC has the same effectiveness [3]. Using equations (2) (3), and (4), it is calculated that 0.0002 mm 5wt.% Gd_2O_3/Al MMC has equivalent neutron absorbing property to a 0.5 mm Cd plate or 3.5 mm 20wt.% B_4C/Al MMC.

4. Results

4.1. Microstructure of MMC

Figure 1 shows the microstructure of Gd_2O_3/Al MMC and B_4C/Al MMC with a volume fraction of 30vol.% and 40vol.%, respectively. Porosity was low despite of high volume fraction of reinforcement.

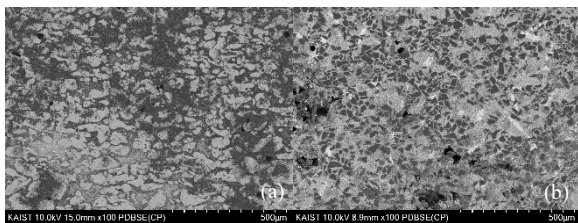


Figure 1 (a) Gd_2O_3/Al MMC (30vol.%) and (b) B_4C/Al MMC (40vol.%)

4.2. Hardness test

The Rockwell hardness test was performed with a B scale and the three-point bending tests were performed

using a universal testing machine (UTM, Instron 5583, Instron Corporation, USA). It was shown that the hardness decreases as volume fraction of Al increases. The hardness values of Gd_2O_3 and Aluminum 7075-T6 are 116.5 and 87, respectively [11] [12].

4.3. Strength and toughness

The tensile strength of Aluminum 7075 alloy is 220 MPa. By adding reinforcement, strength increases. If the reinforcement composition is too high, 40vol% for example, Gd_2O_3 particles contact with each other and high porosity is formed reduces the strength of the MMC. Impact energy of the Gd_2O_3/Al composite is determined by the Charpy impact test.

5. Conclusions

Gd_2O_3 reinforced Aluminum can achieve the same neutron absorbing material behavior with better mechanical properties than the conventional B_4C/Al MMC material. The application of Gd_2O_3/Al MMC in spent nuclear fuel dry storage system may lower the decay heat and the required minimum wet storage period before dry storage can be reduced.

ACKNOWLEDGMENT

This work was supported by the National Research Foundation of Korea (NRF, No. 2014M3C1A9060721) grant funded by the Korea government

REFERENCES

- [1] Jun Kusui, Katsuyuki Hayashi, Kazuo Iwasa, Masakazu Iwase, PATRAM 2004, Paper # 100, 2004
- [2] R.A. Van Konynenburg, P.G. Curtis, T.S.E. Summers, "Scoping Corrosion Tests on Candidate Waste Package Basket Materials for the Yucca Mountain Project", UCRL-ID-130386, Lawrence Livermore National Laboratory Yucca Mountain Project, Livermore, 1998
- [3] P. Zhang, Y. Li, and W. Wang, Journal of Nuclear Materials 437, pp. 350-358, 2013
- [4] R.G. Abrefah, R.B.M. Sogbadji, E. Ampomah-Amoako, Nuclear Engineering and Design 241, pp. 3017-3019, 2011
- [5] Courtney Harrison, Sean Weaver, and Craig Bertelsen, Journal of Applied Polymer Science Vol. 109, pp. 2529-2538 2008
- [6] Joseph R. Davis, Metals Handbook, Vol.2 - Properties and Selection: Nonferrous Alloys and Special-Purpose Materials, ASM International 10th Ed, 1990
- [7] M. Zawiskya, M. Basturka, R. Derntla, Applied Radiation and Isotopes 61, pp.517-523, 2004
- [8] Mark J. Rivard, Robert G. Zamenhof, Applied Radiation and Isotopes 61, pp. 753-757, 2004
- [9] Shu-wei Wang, Ying Liu Ying, Jun Li Jun, Functional Materials 39, pp. 558-561, 2008
- [10] M. Basturk, J. Arzmann, and W. Jerlich, Journal of Nuclear Materials 41, pp. 189-200, 2005
- [11] Tile, Furring, and LS O'Bannon, Dictionary of Ceramic Science and Engineering© Plenum Press, pp.115, 1984
- [12] Marta Bavio, Mauricio Fernández, Erica Zubillaga, Roberto Servant and Eduardo Gautier, Microchemical Journal 128, pp. 320-324, 2016