

Shielding Performance Evaluation of the Alternative Design for a Concrete Plug of Calandria Vault in the Wolsong Units 3 and 4

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Introduction

Calandria Vault Water Makeup (CVWM)

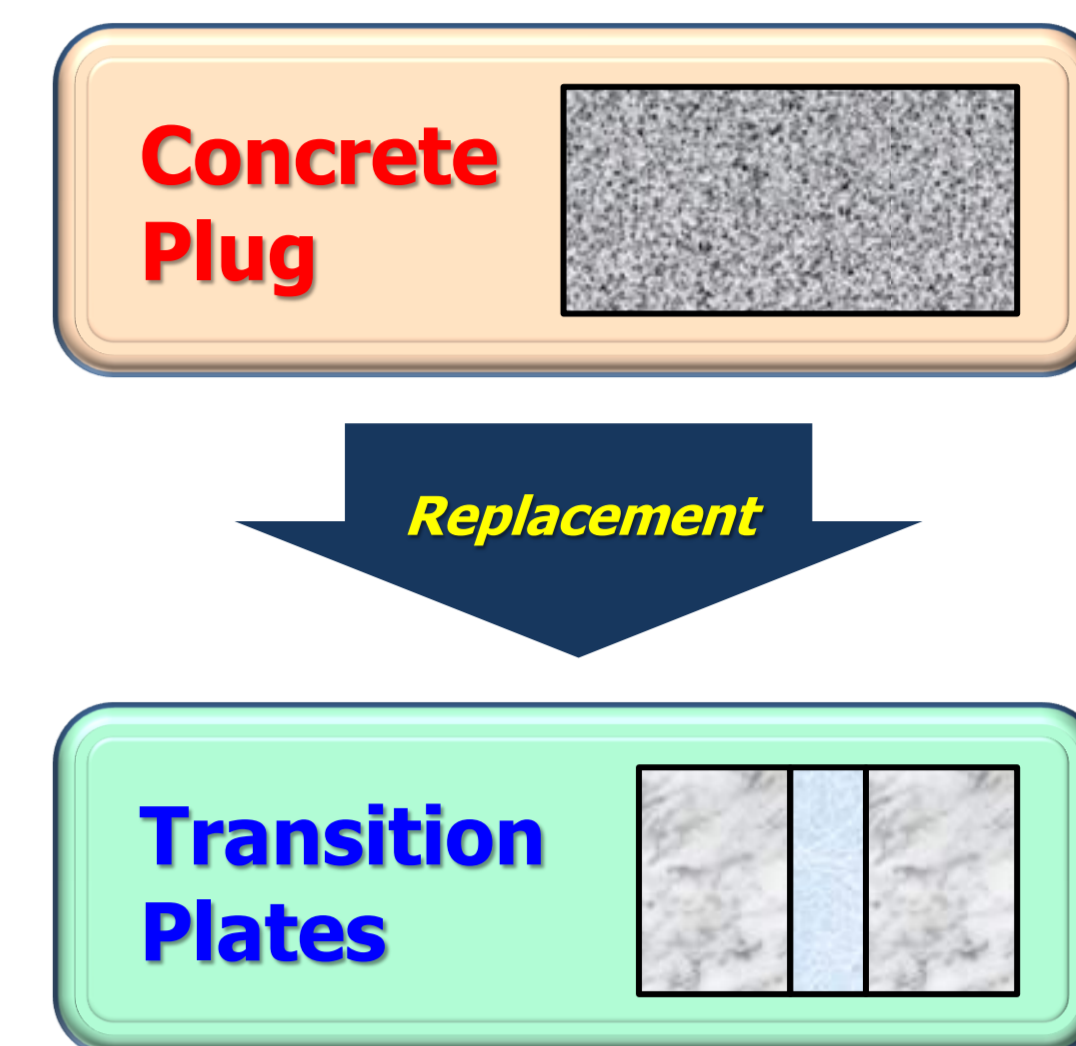
- The flow-path for supplying emergency cooling water to the calandria vault
- Utilized in case that loss of cooling function for the reactor is lasted over a long period of time due to beyond DBAs

Alternative design for the calandria vault is currently under review.

- Replacement of a concrete plug by the transition plate (made of two steel plates)
- Should be designed to provide at least an equivalent shielding effectiveness compared with a concrete plug

The shielding analysis for each design

- Carried out for confirming feasibility of the replacement
- Comparing the shielding performance between a concrete plug and the alternative design (i.e. transition plates)



Methods

Computer Code: MicroShield v9.05 (Point Kernel Method)

Input Data and Assumptions

- Dimensions: Inputted referring to drawings for each design
 - Some values are reasonably determined by the engineering judgment.
- Material and Density

Region	Material	Density [g/cc]	
Source	Air	0.00122	
Concrete Plug	Concrete	2.35	
Transition Plate	T-1	Iron	6.67
	T-2	Iron	5.49
	T-3 & T-4	Iron	7.86
Air Gap	Air	0.00122	
Cover Plate	Iron	7.86	

Source Terms

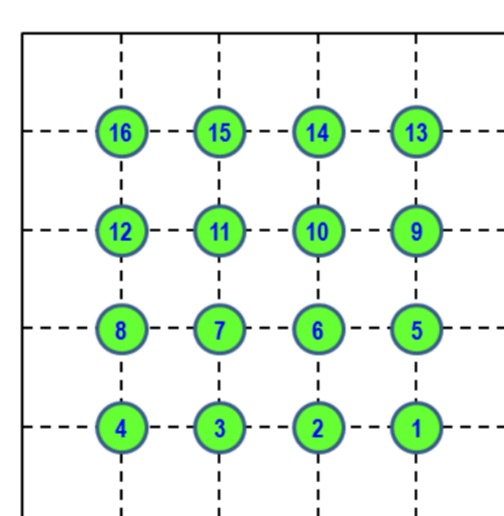
- Assumed that 1 Ci of ¹⁶N is uniformly distributed in the source region filled with air
- Gamma-rays are sorted into energy groups using standard indices.

Nuclide Library: ICRP-107

Flux-to-Dose Conversion Factors: ICRP-74 (Based on ICRP-60)

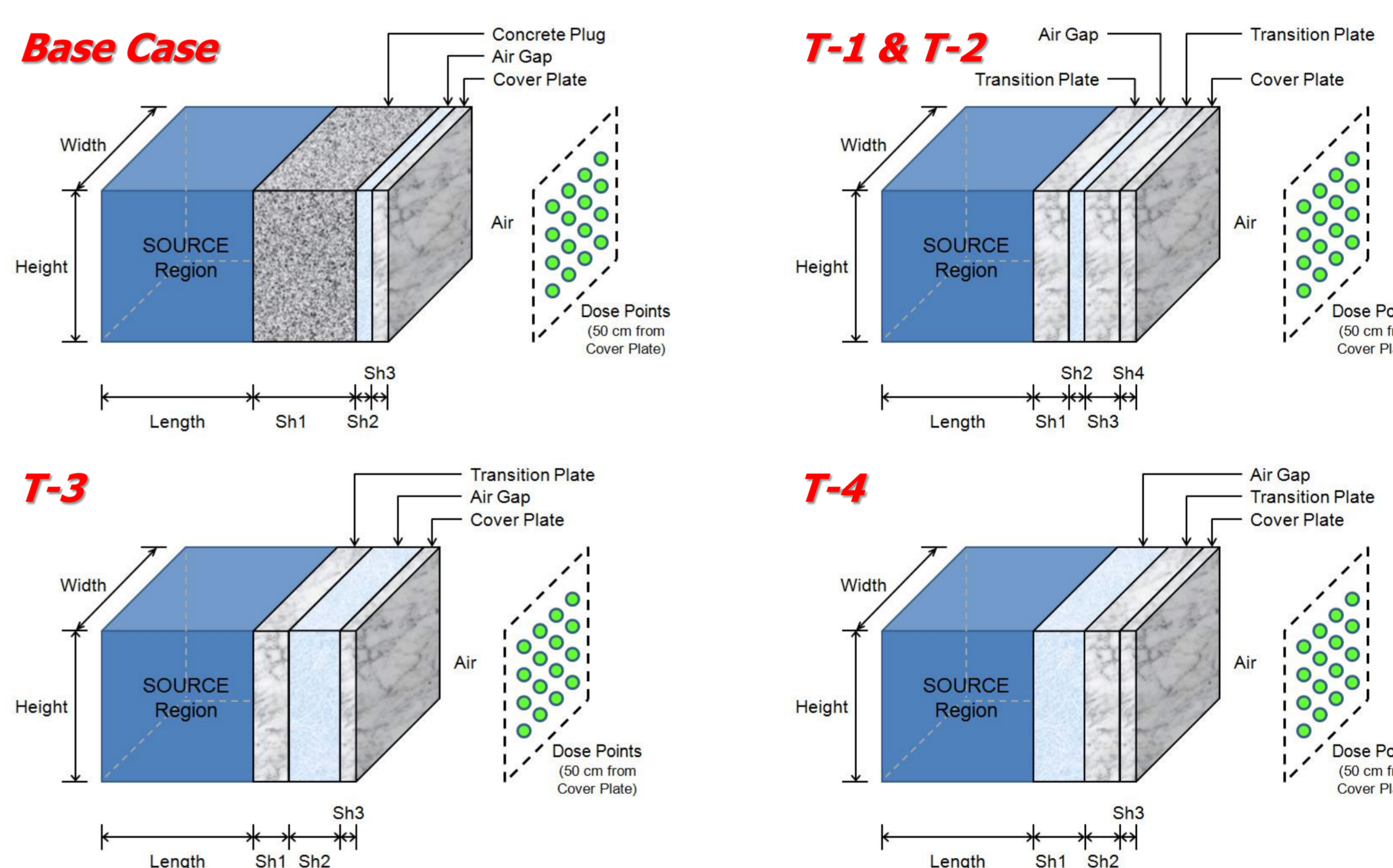
Dose Points

- A total of 16 intersections of imaginary lines which divide width and height into 5 equal parts, respectively.
- 50 cm above the cover plate



Cases Evaluated

Case	Description
Base	A concrete plug is installed.
T-1	A concrete plug is replaced by the transition plate made of 2 plates of steel, which are separated from each other by an air gap. It is assumed that steel and 8 cylindrical openings are homogeneously mixed in the transition plate. A density of the plate is adjusted considering the total volume of openings.
T-2	Very similar to case "T-1". The homogenized density for half space of the plate is applied as that for the whole plate referring to configuration of the transition plate.
T-3 T-4	Since there may be the radiation streaming through openings, a single plate (i.e. the lower or upper part) is only considered in each case. A plate excluded from the calculation is assumed to be an air gap.

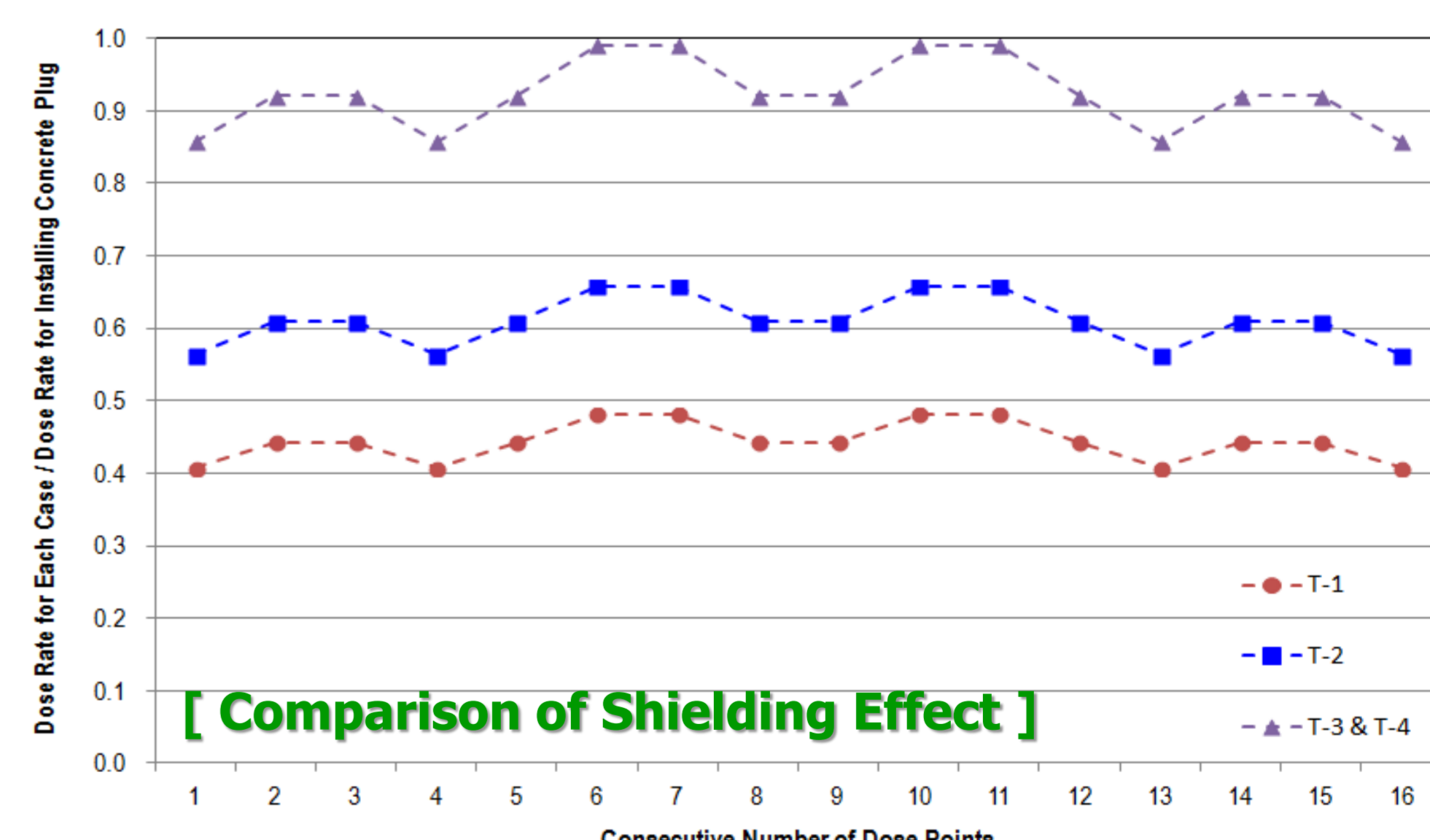


Results and Discussion

For each case,

- the effective dose rate by dose point are evaluated, and
- the value obtained with a concrete plug is considered as the reference value (i.e. 100%) for each point.
- The fraction of dose rate can be calculated through dividing the value for the transition plate by that for a concrete plug.

The alternative design provides a better shielding than a concrete plug, even if only a single plate is considered in the calculation.



Conclusions

Ratio of Dose Rate for Each Case to that for Base Case

Cases	Minimum	Maximum
T-1	0.408	0.482
T-2	0.563	0.659
T-3	0.857	0.989
T-4	0.857	0.989

Based on these results,

- The feasibility of replacement of a concrete plug by two (2) steel plates is confirmed.
- In the aspect of the gamma-ray shielding, it is judged that the transition plate is designed to provide an equivalent or up to about 50% better performance in comparison with the original design using a concrete plug.
- These results will be updated by the additional information, if necessary, and could be applied to the installation design for CVWM.

Acknowledgments

This study was supported by an engineering service contract (with Hyundai Engineering Co., Ltd.) titled "Installation design of the Calandria Vault Water Makeup (CVWM) for Wolsong Units 3 and 4 (Nuclear Mechanical Design)", and grant funded by KHNP.