

Adjoint Sensitivity Analysis and Design Optimization of S-CO₂ Recompression Brayton Cycle for SFR Application

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1. Introduction

Supercritical CO₂ cycle (S-CO₂ Cycle) is a closed Brayton cycle which uses supercritical CO₂ as working fluid. CO₂ shows abrupt change in thermo-physical properties near the critical point. The S-CO₂ power cycle utilizes the reduced compression work near the critical point to increase the efficiency.

A S-CO₂ cycle has advantages of having high efficiency and small component size compared to other gas cycles. Considering these aspects, attempts have been made to apply S-CO₂ cycles for the secondary side of nuclear systems, such as sodium-cooled fast reactor (SFR).

Obtaining the cycle with the highest efficiency for a given layout at the steady or off-design states is the most important steps in the first step of design. In recent years, some attempts have been made to apply artificial neural network and genetic algorithm for parametric optimization of a S-CO₂ cycle. [1] These attempts are usually successful, but they have some limitations as they are based on probability theory. Optimization techniques based on a probabilistic method are not easy to converge to the desired precision. It may also need too much computational resources and time to solve problems having more variables, such as a problem with off-design control strategy, because the probability theory-based methodology generally has an exponential complexity in terms of the number of variables.

In this paper, the authors propose a method to quickly analyze the 1st order sensitivity (Jacobian vector) and the 2nd order sensitivity (Hessian matrix) of the objective function using the adjoint method [2] and to optimize S-CO₂ cycle using the calculated sensitivities. The proposed methodology can be applied to all kinds of cycles. The authors present an example of the cycle optimization for the recompression Brayton cycle at the SFR condition. The optimization was performed using the Levenbert-Marquardt algorithm [3] using Jacobian and Hessian obtained via the adjoint method.

2. Methods and results

2.1 S-CO₂ Recompression Brayton cycle for SFR

A S-CO₂ Recompression Brayton cycle is a highly efficient cycle that is composed of not too many components. This cycle layout has low temperature difference between the inlet and outlet temperature of heat receiving section. Since, CO₂ does not react with

sodium violently, this cycle is one of the promising candidates for the secondary side of SFR.

The cycle layout of S-CO₂ recompression Brayton cycle is shown in Figure 1.

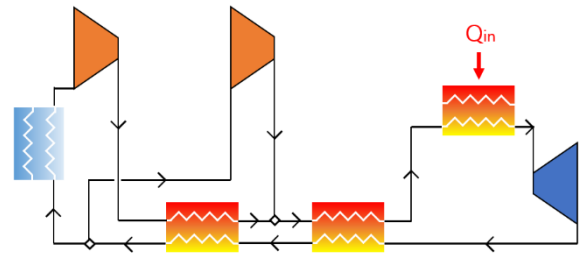


Figure 1. S-CO₂ Recompression Brayton Cycle

Cycle design parameters for SFR are shown in Table 1.

Table 1. Cycle design parameters

| Layout | Recompression Brayton | |
|-----------------------------|-----------------------|-----|
| System Maximum Pressure | 20 | MPa |
| Turbine Inlet Temperature | 505 | °C |
| Cooler Outlet Temperature | 31.3 | °C |
| Turbine Efficiency | 90 | % |
| Compressor Efficiency | 80 | % |
| Recuperator Effectiveness | 95 | % |
| HTR hot side pressure drop | 60 | kPa |
| HTR cold side pressure drop | 30 | kPa |
| LTR hot side pressure drop | 40 | kPa |
| LTR cold side pressure drop | 20 | kPa |
| Precooler pressure drop | 20 | kPa |
| Heater pressure drop | 50 | kPa |
| Turbine pressure ratio | Optimized | |
| Split ratio | Optimized | |

2.2 Adjoint Method

The easiest way to obtain the sensitivity of a parameter of an objective function at single point is to perform numerical differentiation while changing all the parameters one by one. However, this method requires p number of operations for Jacobian, p^2 number of operations for Hessian calculation. It can be requiring too much computational cost.

Adjoint method is the way to calculates the sensitivity by solving a duality problem, without calculating the problem directly. This chapter introduces how to obtain Jacobian and Hessian through the adjoint method.

2.2.1. Jacobian construction

Define the parameters to analyze the sensitivity \mathbf{p} , dependent variables \mathbf{x} , and the given problem $\mathbf{f}(\mathbf{x}, \mathbf{p})$ as shown in Equations (1) to (3).

$$\mathbf{p} = (p_1, p_2, \dots, p_N)^T \dots (1)$$

$$\mathbf{x} = (x_1, x_2, \dots, x_M)^T \dots (2)$$

$$\mathbf{f}(\mathbf{x}, \mathbf{p}) = (f_1(\mathbf{x}, \mathbf{p}), f_2(\mathbf{x}, \mathbf{p}), \dots, f_M(\mathbf{x}, \mathbf{p}))^T \\ = (0, 0, \dots, 0)^T \dots (3)$$

When objective function as g . Then the sensitivity is defined as Equation (4).

$$\frac{dg}{d\mathbf{p}} = g_p + g_x \mathbf{x}_p \dots (4)$$

The \mathbf{x}_p term requires a calculation of \mathbf{p} times in a direct numerical difference method. This may require excessive computational cost. However, as the sensitivity vector of the parameter of defined \mathbf{f} is always 0, \mathbf{x}_p can be calculated without additional computation. (See Equation (5))

$$\frac{d\mathbf{f}}{d\mathbf{p}} = \left(\frac{d\mathbf{f}}{dp_1}, \frac{d\mathbf{f}}{dp_2}, \dots, \frac{d\mathbf{f}}{dp_N} \right) = 0 \\ \frac{d\mathbf{f}}{dp_i} = \frac{\partial \mathbf{f}}{\partial p_i} + \sum_j \left(\frac{\partial \mathbf{f}}{\partial x_j} \frac{\partial x_j}{\partial p_i} \right) \\ \therefore \frac{d\mathbf{f}}{d\mathbf{p}} = \mathbf{f}_p + \mathbf{f}_x \mathbf{x}_p = \mathbf{0} \\ \mathbf{x}_p = -\mathbf{f}_x^{-1} \mathbf{f}_p \dots (5)$$

Substituting Equation (5) into Equation (4) yields Equation (6).

$$\frac{dg}{d\mathbf{p}} = g_p + g_x \mathbf{x}_p = g_p - g_x (\mathbf{f}_x^{-1} \mathbf{f}_p) = g_p - (g_x \mathbf{f}_x^{-1}) \mathbf{f}_p \\ = g_p - \lambda^T \mathbf{f}_p \dots (6) \\ \text{when } \mathbf{f}_x^T \lambda = g_x^T$$

This is the adjoint method.

2.2.2. Hessian construction

Under the same conditions as Equations (1)~(3), the Hessian matrix for object function g is defined as Equation (7).

$$\mathbf{H} = \left(\frac{d}{dp_1} \left(\frac{dg}{d\mathbf{p}} \right)^T, \frac{d}{dp_2} \left(\frac{dg}{d\mathbf{p}} \right)^T, \dots, \frac{d}{dp_N} \left(\frac{dg}{d\mathbf{p}} \right)^T \right) \dots (7)$$

In a similar way as 2.2.1, predefined hessian matrix can be written as equation (8) without calculating computationally complex term.

$$\mathbf{H} = g_{pp} - \lambda_1^T \mathbf{f}_p - \mathbf{f}_p^T \lambda_1 - \lambda_3^T \mathbf{f}_p \\ + \left(\begin{array}{c} -\lambda_0^T \left\{ \begin{array}{c} \frac{\partial}{\partial p_1} (\mathbf{f}_p) + \sum_i \frac{\partial \mathbf{f}_p}{\partial x_i} \frac{dx_i}{dp_1} \\ + \left[\frac{\partial}{\partial p_1} (\mathbf{f}_x) + \sum_i \frac{\partial \mathbf{f}_x}{\partial x_i} \frac{dx_i}{dp_1} \right] (-\mathbf{f}_x^{-1} \mathbf{f}_p) \end{array} \right\} \\ -\lambda_0^T \left\{ \begin{array}{c} \frac{\partial}{\partial p_2} (\mathbf{f}_p) + \sum_i \frac{\partial \mathbf{f}_p}{\partial x_i} \frac{dx_i}{dp_2} \\ + \left[\frac{\partial}{\partial p_2} (\mathbf{f}_x) + \sum_i \frac{\partial \mathbf{f}_x}{\partial x_i} \frac{dx_i}{dp_2} \right] (-\mathbf{f}_x^{-1} \mathbf{f}_p) \end{array} \right\} \\ \vdots \\ -\lambda_0^T \left\{ \begin{array}{c} \frac{\partial}{\partial p_N} (\mathbf{f}_p) + \sum_i \frac{\partial \mathbf{f}_p}{\partial x_i} \frac{dx_i}{dp_N} \\ + \left[\frac{\partial}{\partial p_N} (\mathbf{f}_x) + \sum_i \frac{\partial \mathbf{f}_x}{\partial x_i} \frac{dx_i}{dp_N} \right] (-\mathbf{f}_x^{-1} \mathbf{f}_p) \end{array} \right\} \end{array} \right) \dots (8)$$

2.3 Levenberg-Marquardt algorithm

To apply the calculated sensitivity to the optimization, an appropriate optimization methodology is needed. The Levenberg-Marquardt algorithm [3] (also known as the damped least-square method) was used in this study.

The gradient descent method, which is the general 1st order optimization scheme and the Gauss-Newton method, which is general the 2nd order scheme, are given by Equations (9) ~ (10).

$$\text{Gradient Descent Method: } \mathbf{p}_{k+1} = \mathbf{p}_k - \lambda J \dots (9)$$

$$\text{Gauss - Newton Method: } \mathbf{p}_{k+1} = \mathbf{p}_k - H^{-1} J^T \dots (10)$$

The gradient descent method stably converges, but it may require too many calculations. The Gauss-Newton method quickly finds the optimal point. However, Gauss-Newton method can be unstable if the starting point is misplaced. The Levenberg-Marquardt algorithm, is a method that uses the Newton method at a point far from the optimal point, and gives damping near the optimal point to switch to the Gradient descent method smoothly. This method combines advantages of two methods. When the damping coefficient is defined as μ , the Levenberg-Marquardt algorithm is shown in Equation (11).

$$\mathbf{p}_{k+1} = \mathbf{p}_k - [H + \mu * \text{diag}(H)]^{-1} J^T \dots (11)$$

If the result of \mathbf{p}_{k+1} is not better or even worse than the result computed at \mathbf{p}_k , the calculation returns to k th iteration without further sensitivity analysis, then assign larger μ and compute \mathbf{p}_{k+1}' until the value become better that of the k th iteration. In this process, the larger the damping coefficient is, the more the behavior of Equation (11) becomes similar to that of Equation (9). On the contrary, the smaller μ is, the more the behavior of Equation (11) resembles Equation (10).

2.4 Sensitivity Analysis Result

At the calculated optimal point, sensitivity of whole design parameters was calculated. Analyzed parameters list and their sensitivity are shown in Table 2. The unit of sensitivities is differences of efficiency per 1 percent point changes of each parameter. Calculation did in general PC condition.

The time consumption for calculating those 14 parameters' sensitivity is ~0.3 sec at PC. This result is 42 times faster than traditional direct numerical differences method. For Hessian matrix calculation, the developed method consumes 6.8 sec. This is more than 100 times faster than direct numerical difference method.

Table 2. Sensitivity of design parameters

| | Parameters | Value | Sensitivity (D/%) |
|-----------------|------------------------------|-------|-------------------|
| System | Maximum Temperature (oC) | 505 | 2.49E-03 |
| | Maximum Pressure (kPa) | 20000 | 1.05E-03 |
| | Minimum Temperature (oC) | 31.3 | -7.73E-04 |
| Turbine | Eff (-) | 0.9 | 3.56E-03 |
| Main compressor | Eff (-) | 0.8 | 7.74E-04 |
| Re compressor | Eff (-) | 0.8 | 6.87E-04 |
| Cooler | Pressure drop (kPa) | 20 | -3.12E-06 |
| HTR | Eff (-) | 0.95 | 1.32E-03 |
| | Cold side presure drop (kPa) | 60 | -1.18E-05 |
| | Hot side presure drop (kPa) | 30 | -1.49E-05 |
| LTR | Eff (-) | 0.95 | 2.27E-03 |
| | Cold side presure drop (kPa) | 40 | -5.61E-06 |
| | Hot side presure drop (kPa) | 20 | -9.45E-06 |
| IHX | Pressure drop (kPa) | 50 | -9.80E-06 |

2.5 Optimization Result

Based on the developed fast sensitivity analysis, sensitivity based optimization was performed. In the 1E-06 precision level, the optimization was finished within 6 times of sensitivity analysis. To obtain the same precise solution, traditional brute-force algorithm or genetic algorithm may need physically impossible time.

By the Jacobian and Hessian sensitivities described from section 2.2, the optimized result of S-CO₂ Recompression Brayton cycle is shown in Figure 2.

Validation for optimized point also progressed. Points of each iterative calculation and response surface for recompression Brayton cycle is obtained and shown in

Figure 3. This result shows that the obtained design point is actually an optimum point.

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//////////////////////////////////// Result summary //////////////////////////////////////
Mass flow rate (kg/sec)                1892.9643
IHX name                               Inlet Heat(MW)
IHX                                    349.922
Efficiency (%)                          42.8665
Net work (MW)                           149.9993

//////////////////////////////////// Condition info //////////////////////////////////////
Working fluid                           CO2
Heatsource target temperature(K)        778.16
Cooler target temperature(K)            304.46
Maximum compressor target pressure(kPa)  20000
Error Bound condition                   1e-07

//////////////////////////////////// Channel info //////////////////////////////////////
Channel ID   Channel T(oC)   Channel P(MPa)   Channel H(kJ/kg)   Channel S(kJ/kg-K)
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1            505             19.88            979.572            2.67282
2            396.452        7.74264          863.661            2.69221
3            171.909         7.71264          608.745            2.22947
4            63.1958         7.69264          468.133            1.86449
5            63.1958         7.66264          468.515            1.86614
6            31.3            7.64264          299.936            1.32595
7            59.0662         20              322.194            1.39939
8            164.149         19.96           545.828            1.9257
9            160.264         19.96           539.803            1.91873
10           354.326         19.9            794.718            2.40662
11           63.1958         7.66264          468.515            1.86614
12           153.827        19.96           529.597            1.895

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Figure 2. Optimization result

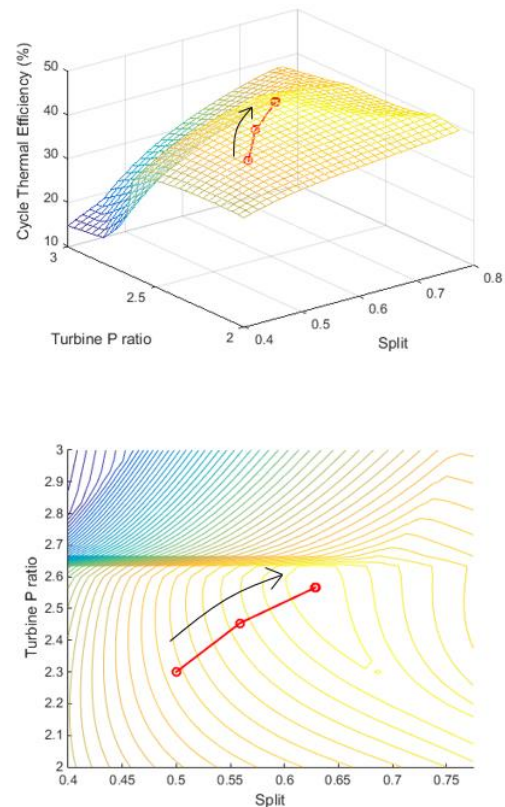


Figure 3. Points of each iterative calculation and response surface for recompression Brayton cycle

3. Conclusions

This study suggested the adjoint sensitivity analysis and optimization process of S-CO₂ recompression Brayton cycle for SFR application. Developed methodology showed the ability to obtain optimal point with short computational time and high precision. In the view point of sensitivity analysis, the suggested adjoint based sensitivity analysis methods are 42 times faster for the 1st order Jacobian analysis and more than 100 times faster for the 2nd order Hessian analysis. This fast sensitivity analysis is applied to the cycle optimization. With the adjoint sensitivity analysis, the authors can optimize given cycle layout with high precision and low computational cost. If the same optimization problem is solved with a traditional method, it would be very demanding in terms of computational resources.

Another strong point of the suggested methodology is the computational resource independence of the number of parameters to be optimized. It shows the possibility to apply for the optimization of an off-design control strategy problem, which is nearly impossible to solve precisely because of the large number of control parameters.

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