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Dual-energy imaging performance in sandwich detectors for mouse imaging

@2017 KNS spring meeting

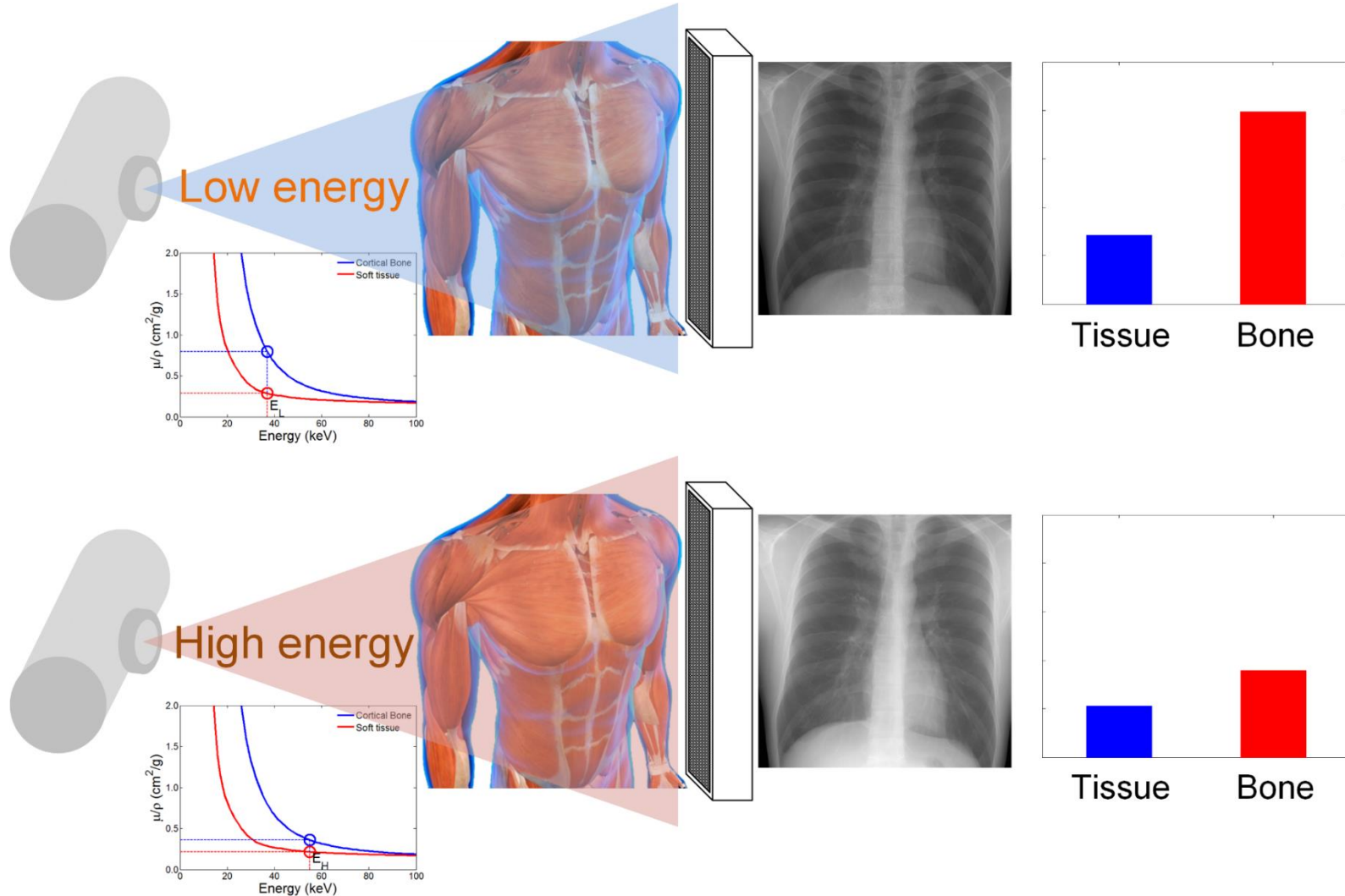
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Outline

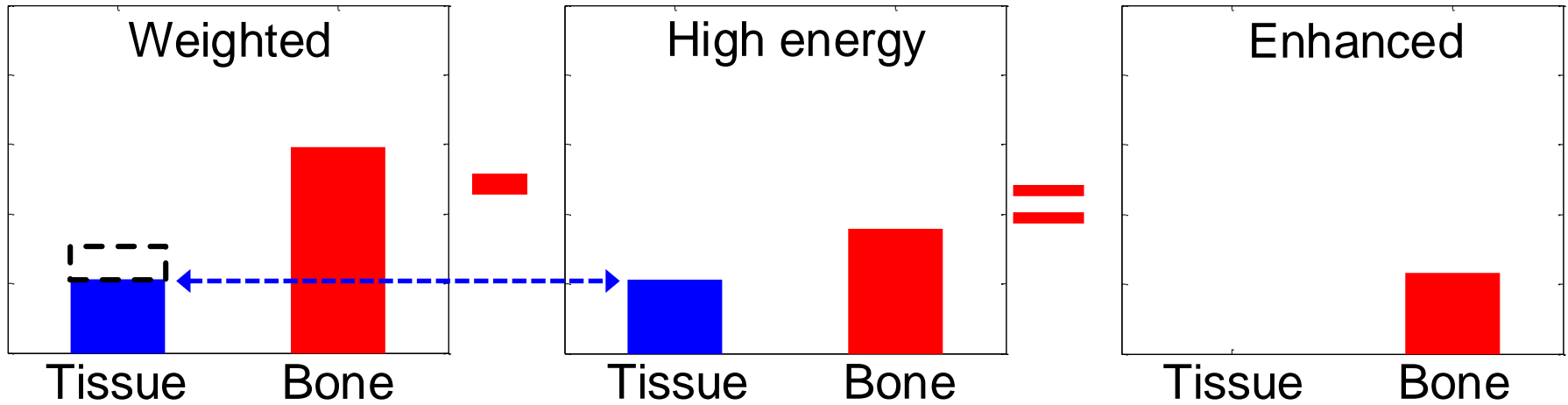
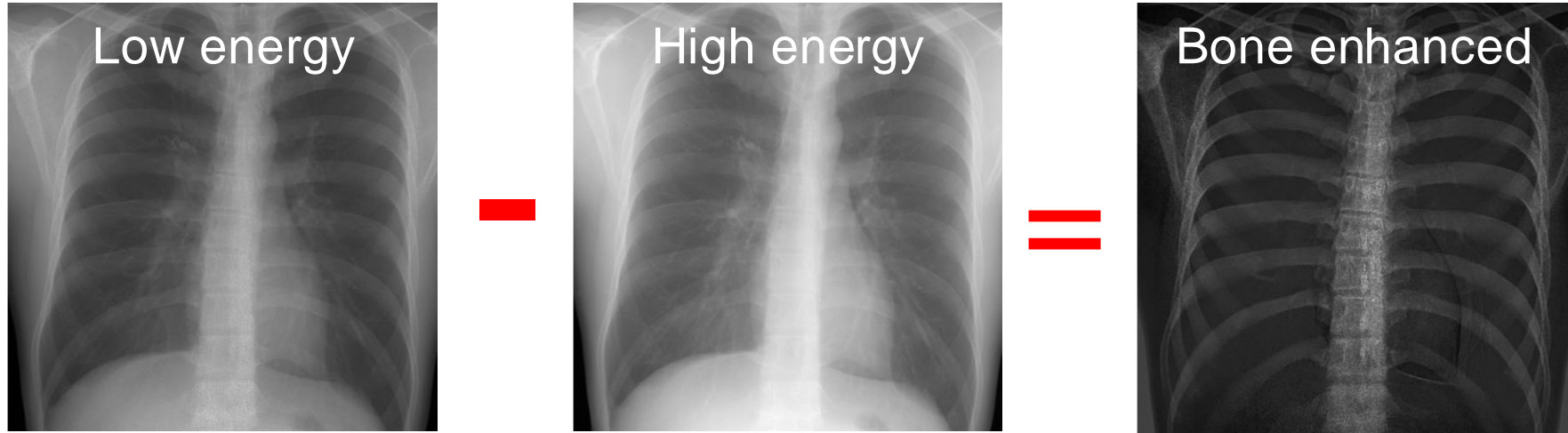
- Introduction
 - Dual-energy imaging
 - Motivation
- Materials & Methods
 - Zero-frequency performance
 - Modeling
- Results
 - Zero-frequency performance
 - Performance of sandwich detectors
 - Optimization
- Conclusion

Dual-energy imaging

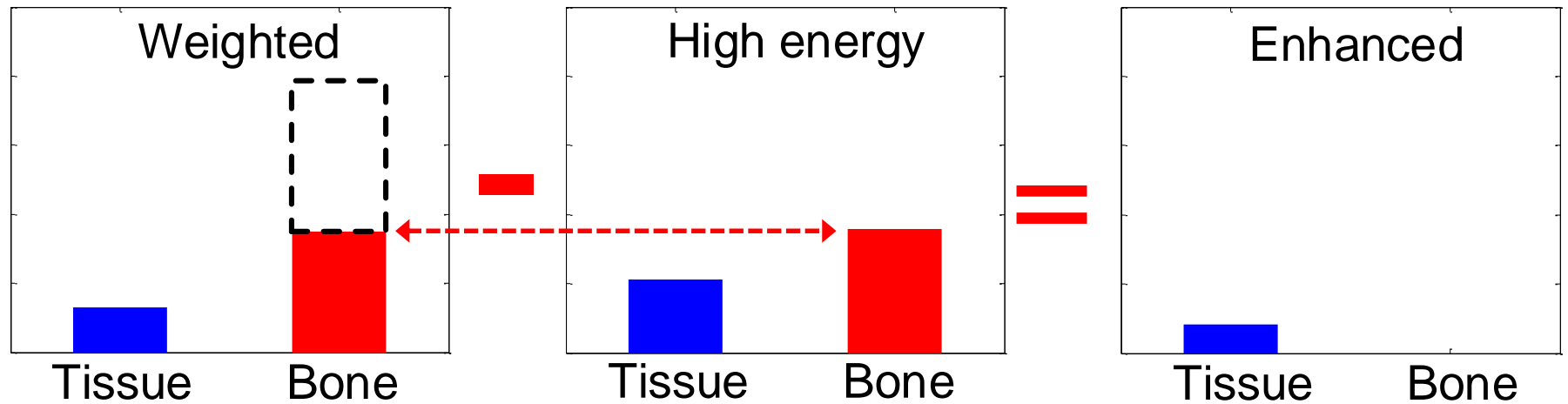
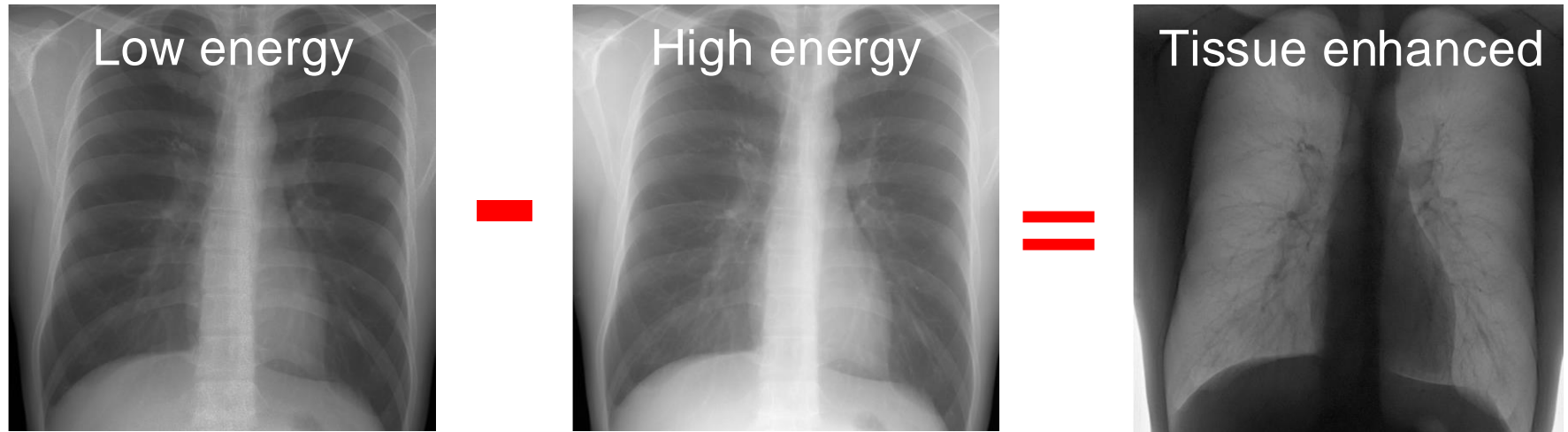


R. E. Alvarez et al., *Med. Phys.* (2004)

Dual-energy imaging

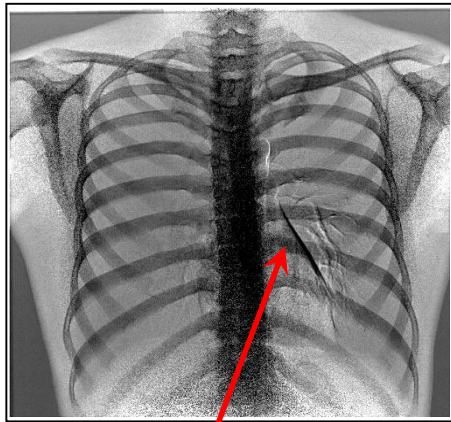


Dual-energy imaging



Motivation

- Dual-energy imaging is vulnerable to motion artifacts during registration of two successive images
- The sandwich detector can avoid motion artifacts by acquiring the high and low images at the same time



Motion artifact

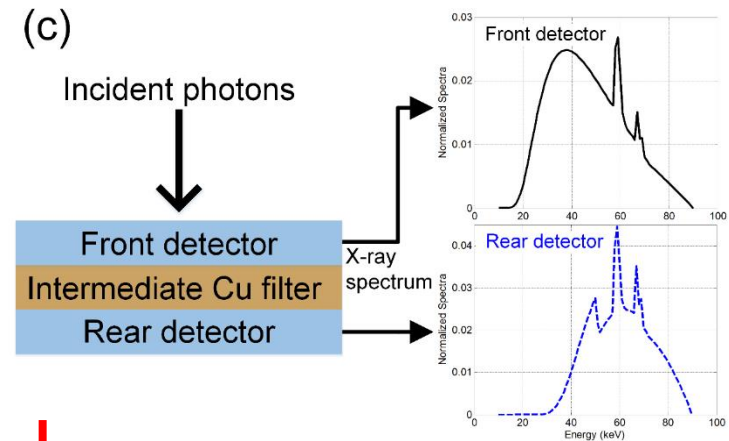
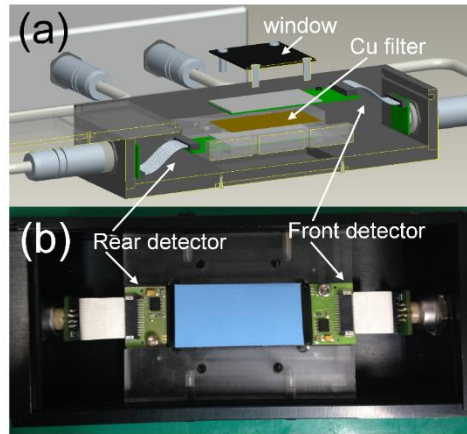
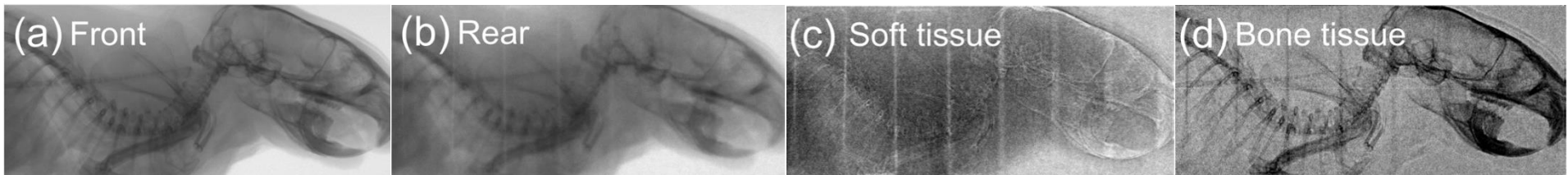
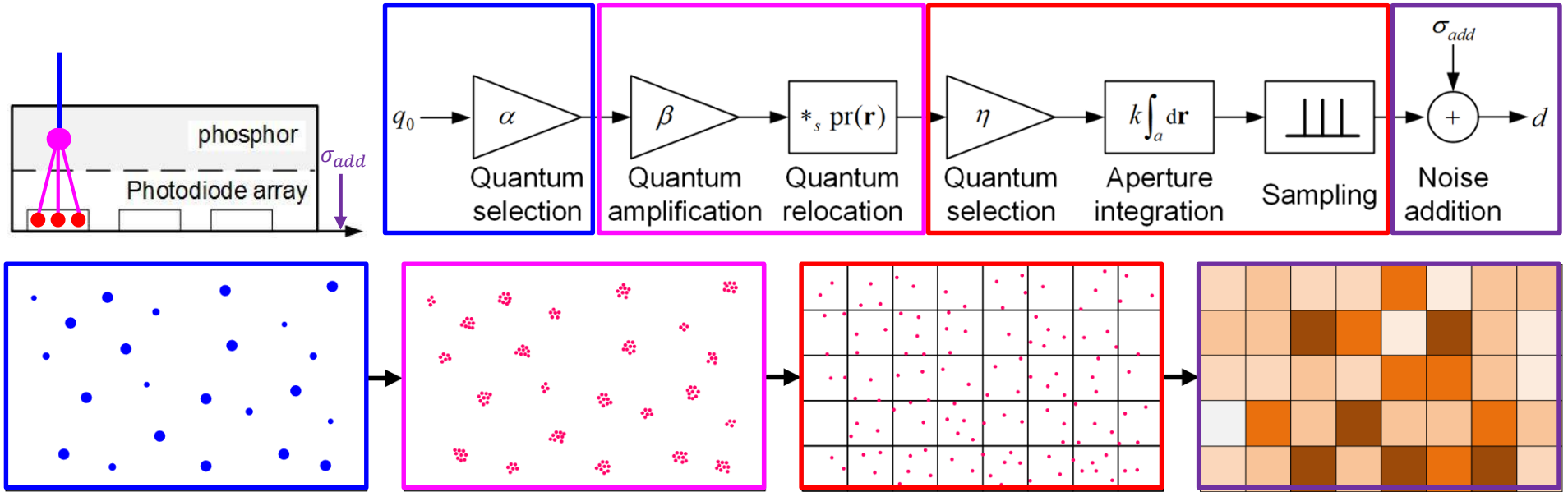


Image quality – kVp, t_{IF}



Modeling

- A simple cascaded-systems model describing the signal and noise propagation in an indirect flat-panel detector



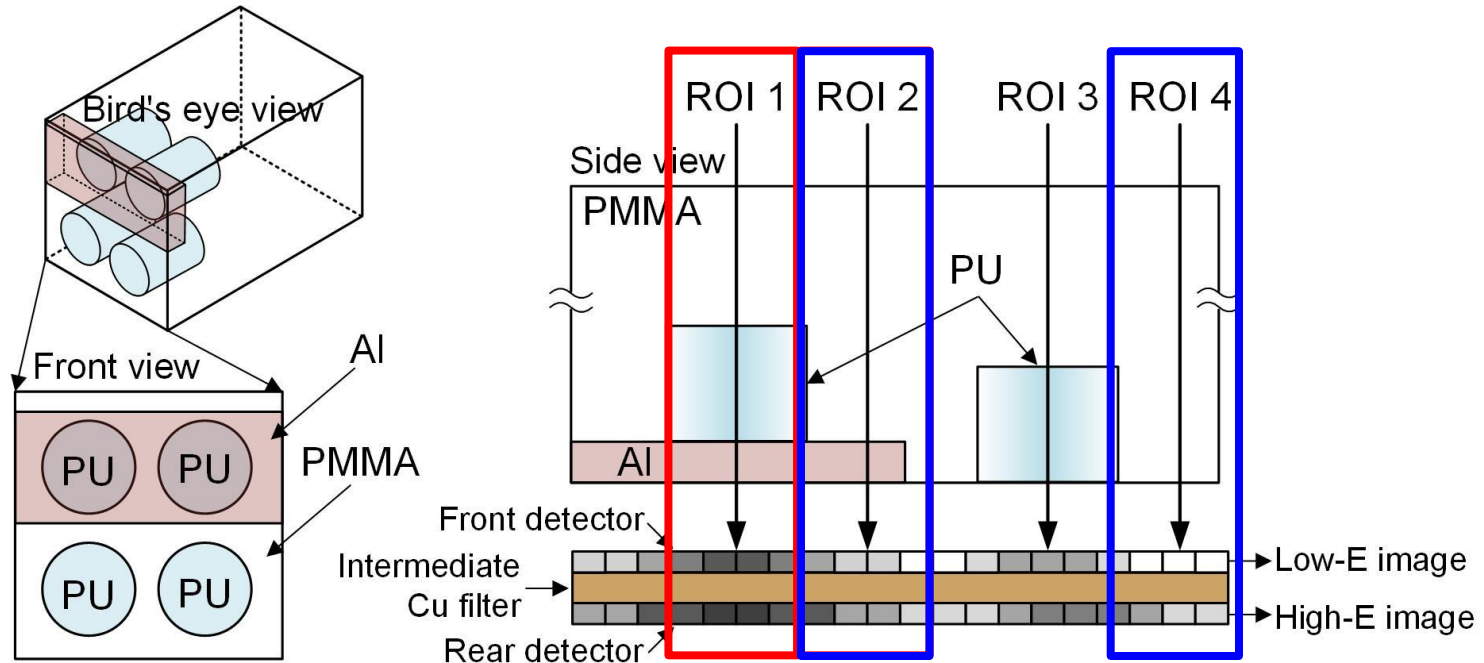
$$\bar{d}_j = ka^2 \bar{q} \bar{\tau}_j \bar{g}_j$$

$$W'_{j,indirect}(u) = \frac{\bar{m}_{j,indirect}^2}{\bar{q}_0 \bar{\tau}_j \bar{g}_j^2} \left[\frac{1}{\gamma \bar{m}_{j,indirect}} + \frac{1}{\bar{\alpha}_j} \left(\frac{1}{I_{F,indirect}} - \frac{1}{\bar{\beta}_j} \right) T_{j,alias}^2(u) \right]$$

$$W'_{j,direct}(u) = \frac{\hat{\alpha}_j \bar{m}_{j,direct}^2}{\gamma \bar{q}_0 \bar{\xi}_j \bar{\tau}_j I_{j,direct} \bar{g}_j^2}, \quad W'_{j,add}(u) = \frac{\sigma_{j,add}^2}{\gamma a^2 \bar{q}_0^2 \bar{\tau}_j^2 \bar{g}_j^2}$$

DE contrast model

- The contrast in DE images may be expressed in attenuation coefficient:



$$p^{DE} = p^H - w \times p^L = \ln \left(\frac{I^H}{I_0^H} \right) - w \times \ln \left(\frac{I^L}{I_0^L} \right) = \mu_M^H (t_M - t_j) + \mu_j^H t_j - w [\mu_M^L (t_M - t_j) + \mu_j^L t_j]$$

- Al-enhanced** $C_{24} = |p_2^{DE} - p_4^{DE}| = |(w\Delta\mu_{AlPMMA}^L - \Delta\mu_{AlPMMA}^H)t_{Al}|$

- PU-enhanced** $C_{12} = |p_1^{DE} - p_2^{DE}| = |(w\Delta\mu_{PUPMMA}^L - \Delta\mu_{PUPMMA}^H)t_{PU}|$

$$\Delta\mu_{jM}^i = \mu_j^i - \mu_M^i$$

DE noise model

S. Richard and J. H. Siewerdsen, *Med. Phys.* (2007)

- The noise in DE images may be expressed in the zero-frequency DQE form:

$$p^{DE} = p^H - w \times p^L = \ln\left(\frac{I^H}{I_0^H}\right) - w \times \ln\left(\frac{I^L}{I_0^L}\right)$$

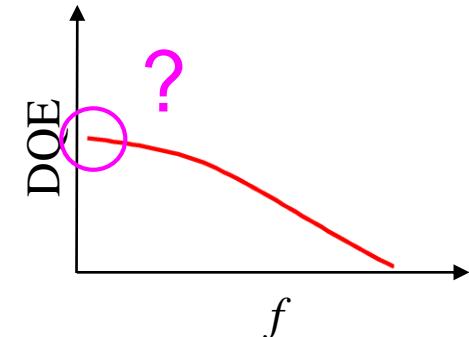
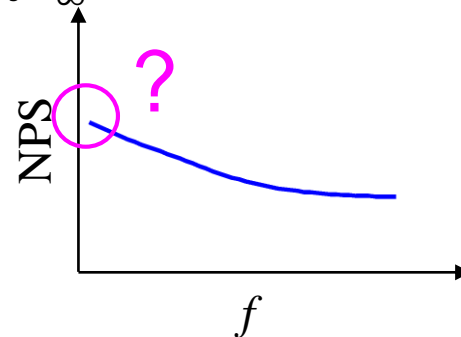
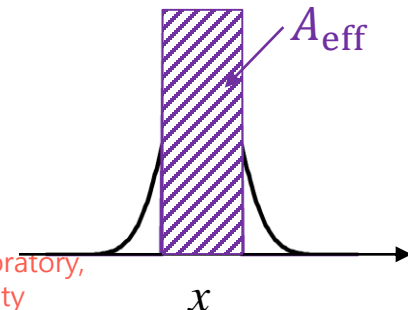
Error propagation

$$\sigma_j^2 = w_j^2 \left(\frac{\sigma^F}{I^F}\right)^2 + \left(\frac{\sigma^R}{I^R}\right)^2$$

$$= \frac{w_j^2}{(\text{SNR}^F)^2} + \frac{1}{(\text{SNR}^R)^2} = \frac{w_j^2}{\text{DQE}^F(0) \bar{q}_0 X A_{\text{eff}}^F} + \frac{1}{\text{DQE}^R(0) \bar{q}_0 X A_{\text{eff}}^R}$$

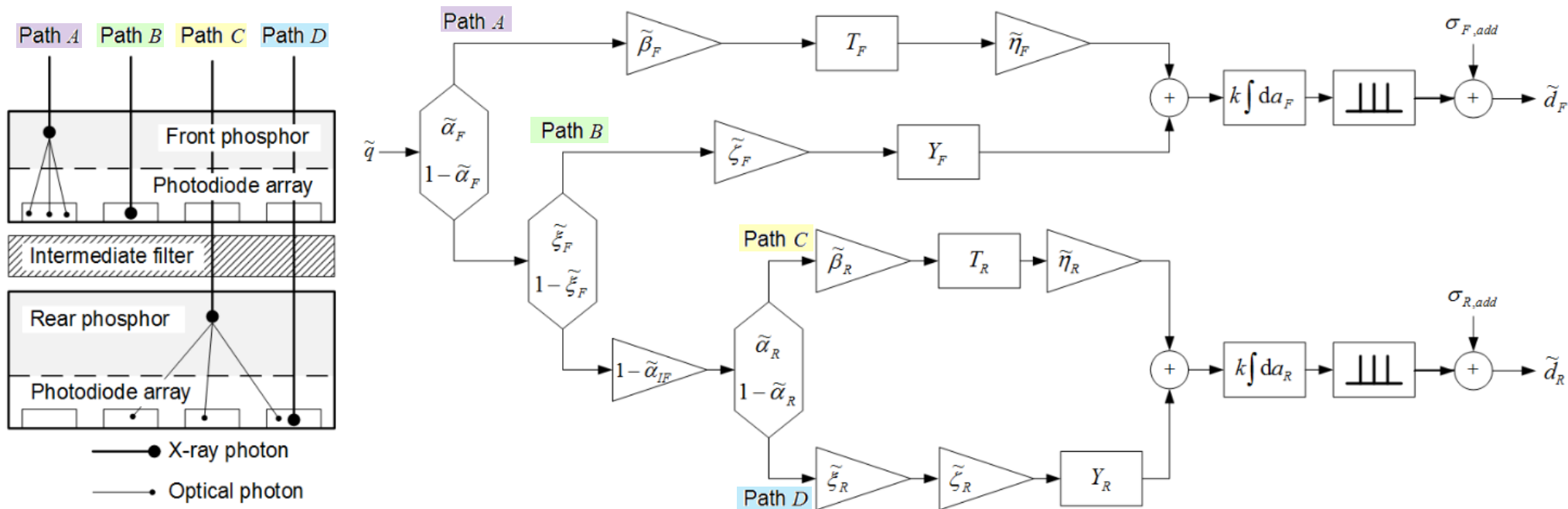
$$\text{SNR} = \frac{\bar{d}^2}{\sigma_d^2} = \text{DQE}(0) \bar{q} A_{\text{eff}} \quad \text{DQE}(0) = \frac{1}{\bar{q} [\text{NPS}(0) / \bar{d}^2]} = \frac{\bar{d}^2}{\bar{q} A_{\text{eff}} \sigma_d^2}$$

$$\text{NPS}(0) = \left[\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \text{MTF}_{\text{pre}}^2(u, v) \, du \, dv \right]^{-1} \sigma_d^2 = A_{\text{eff}} \sigma_d^2$$



Modeling

- A cascaded-systems model describing the signal and noise propagation in sandwich detector
- A model including the direct interaction of x-ray photons with the photodiode layer that is unattenuated by the phosphor



D. W. Kim et al., *J. Instrum.* (2016)

FOM model

- The FOM in DE images using contrast model and noise model:

$$\begin{aligned}
 C_{jM} &= |(w\Delta\mu_{jM}^L - \Delta\mu_{jM}^H)t_j| & \sigma_{obj}^2 &= Kf^{-b}MTF^2(f) \\
 FOM_j &= \frac{CNR_j^2}{X} = C_j^2 \left[X \left\{ w_j^2 \left((\sigma_{det}^F)^2 + (\sigma_{obj}^F)^2 \right) + (\sigma_{det}^R)^2 + (\sigma_{obj}^R)^2 \right\} \right]^{-1} \\
 & & \sigma_j^2 &= w_j^2 \left(\frac{\sigma^F}{IF} \right)^2 + \left(\frac{\sigma^R}{IR} \right)^2 \\
 & & &= \frac{w_j^2}{(SNR^F)^2} + \frac{1}{(SNR^R)^2} = \frac{w_j^2}{DQE^F(0)\bar{q}_0XA_{eff}^F} + \frac{1}{DQE^R(0)\bar{q}_0XA_{eff}^R}
 \end{aligned}$$

Experimental setup

Toshiba E7239X X-ray source

Sandwich detector

50 ~ 90 kVp

SDD = 985 mm

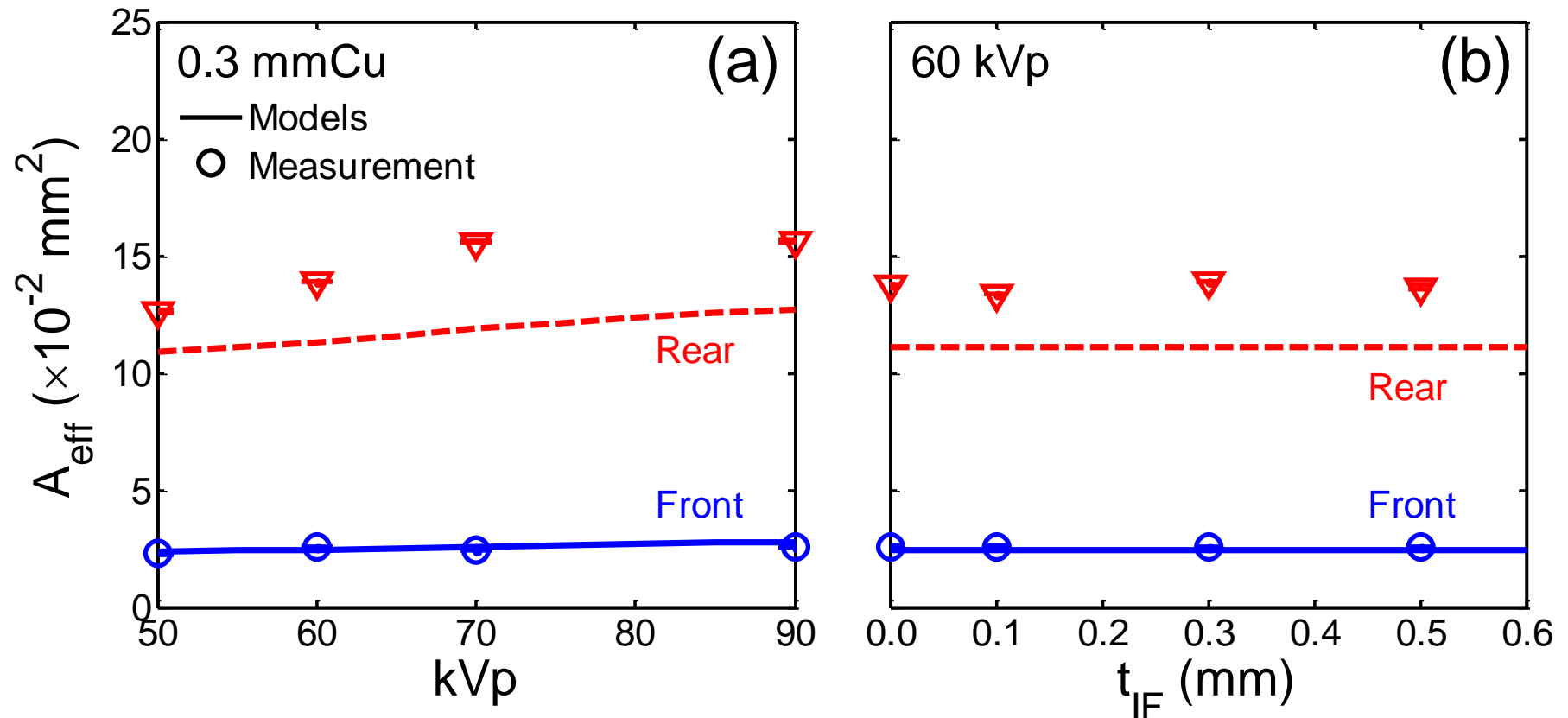
Designed Phantom

X-ray Tube	Toshiba E7239X
Inherent filter	0.9 [eq-mmAl]
Collimator	1.5 [mmAl]
Anode angle	1.6 [°]
Target material	tungsten

Material	Thickness	Density
	cm	g/cm ³
PMMA	3	1.18
Aluminum	0.1	2.699
Polyurethane	0.3	1.18(PD 50 %)

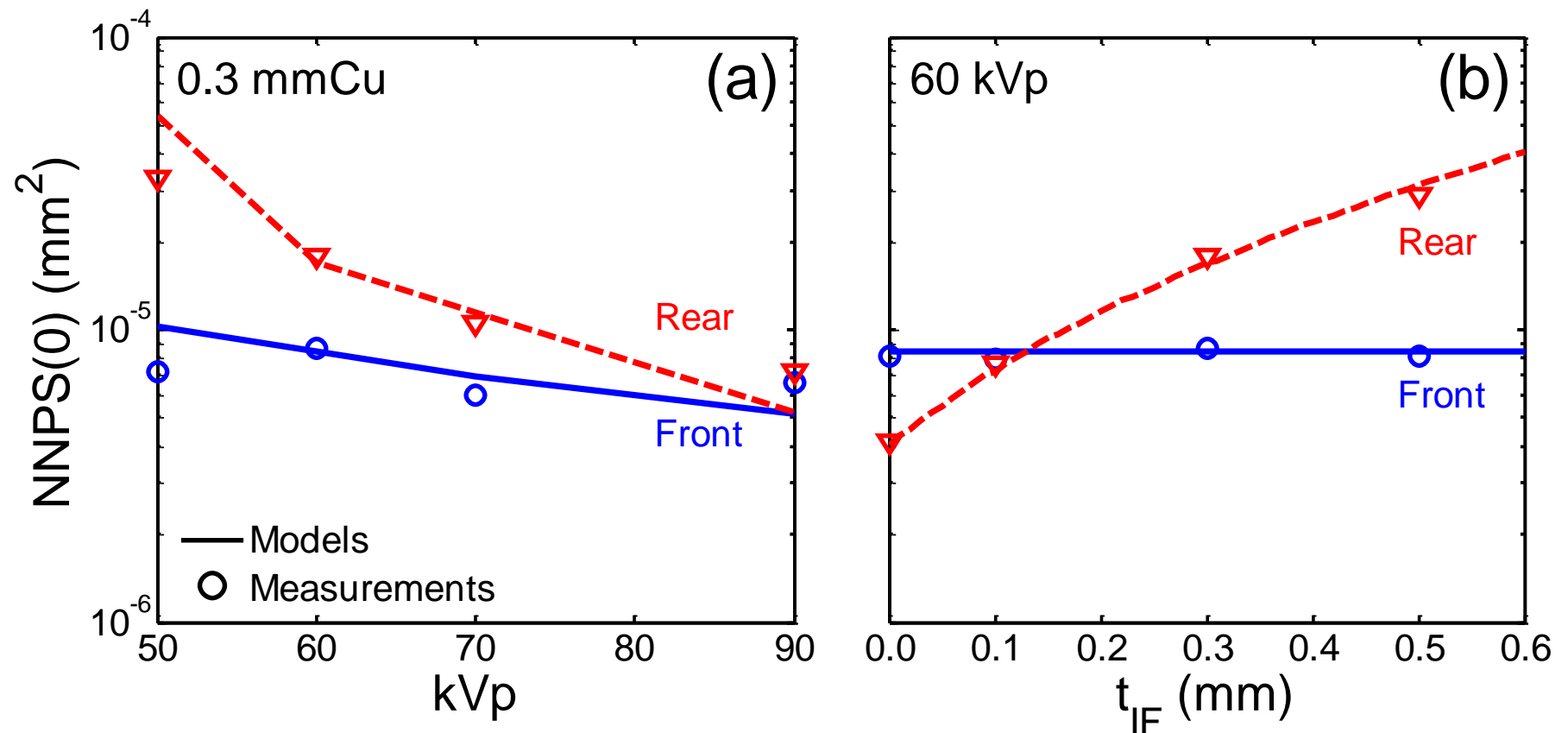
Effective aperture

- Validation between measured in sandwich detector and CSA model
- $A_{\text{eff}} = \left[2\pi \int_0^\infty \text{MTF}_{\text{pre}}^2(f) f df \right]^{-1}$



NNPS(0)

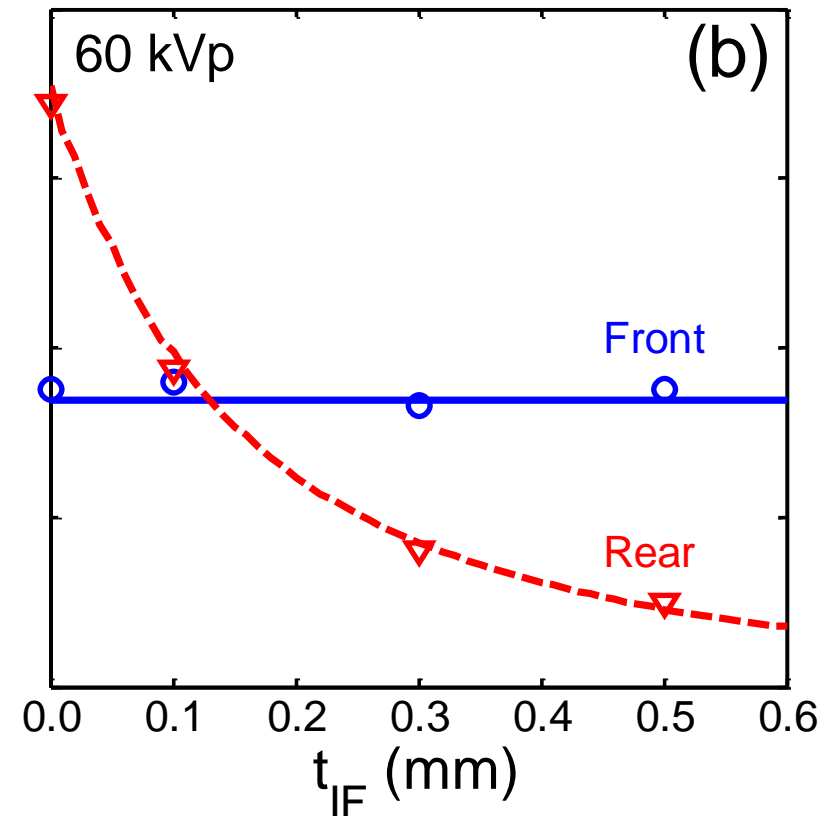
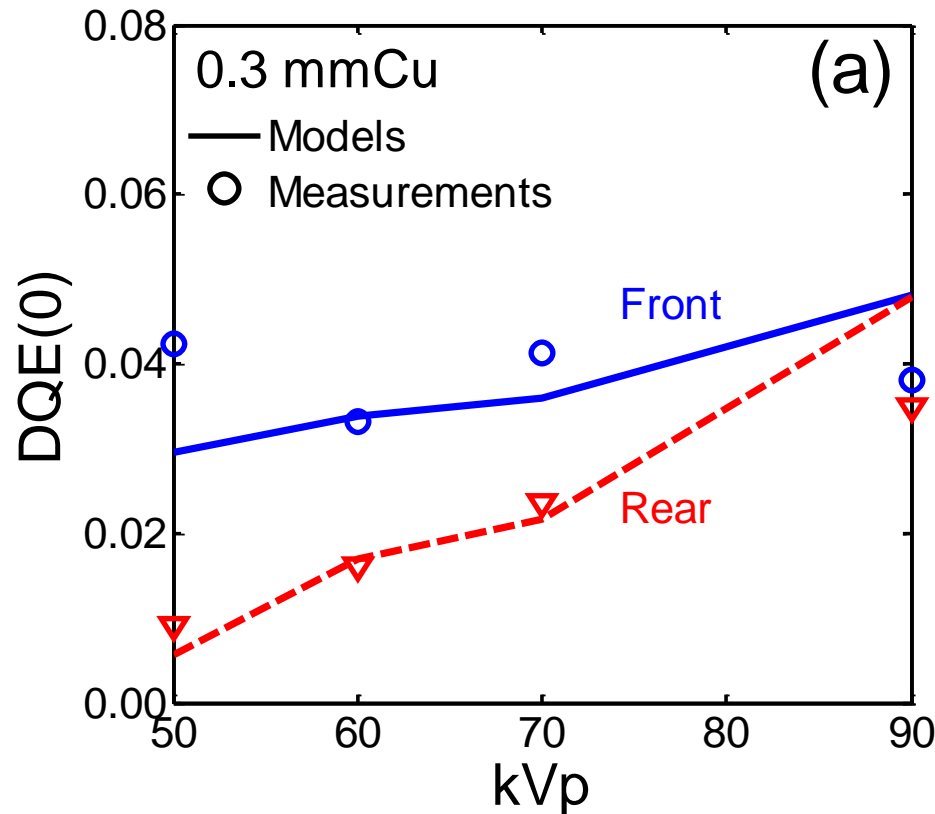
- Validation between measured in sandwich detector and CSA model
- $$\text{NNPS}(0) = \left[\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \text{MTF}_{\text{pre}}^2(u, v) du dv \right]^{-1} (\sigma_d^2 / \bar{d})^2 = A_{\text{eff}} (\sigma_d^2 / \bar{d})^2$$



DQE(0)

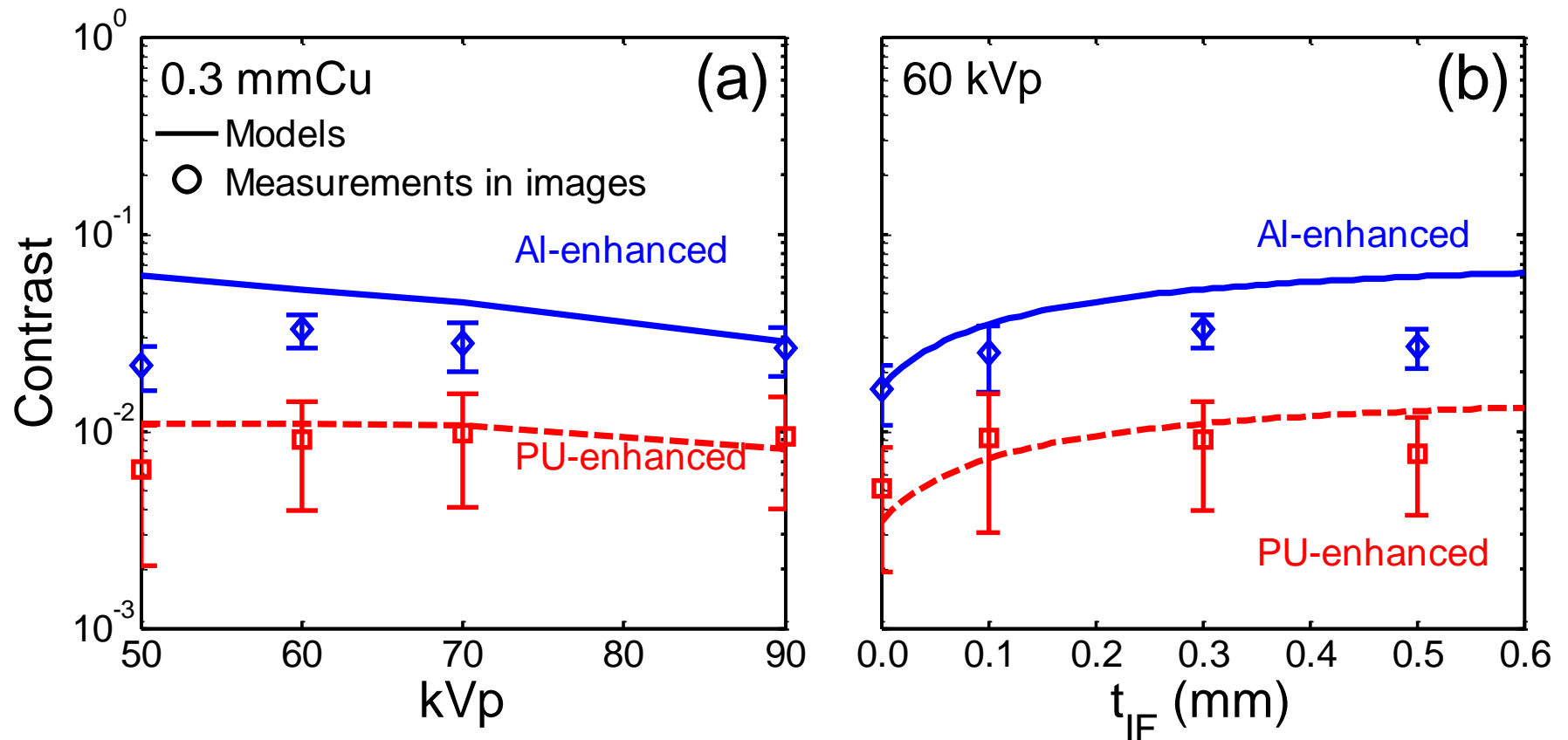
- Validation between measured in sandwich detector and CSA model

- $$DQE(0) = \frac{1}{\bar{q}_{NPS(0)}/\bar{d}^2} = \frac{1}{\bar{q}_{NNPS(0)}}$$



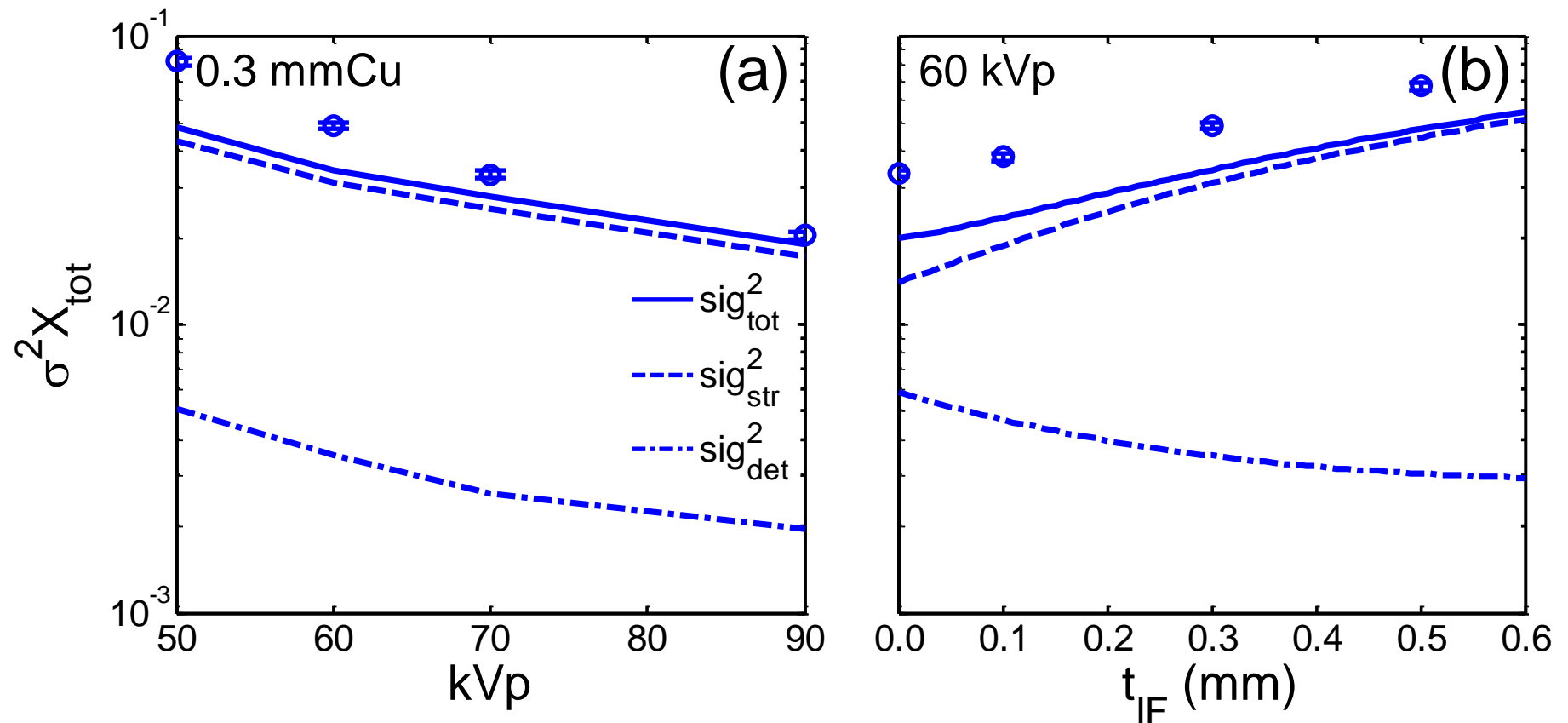
Contrast

- Contrast of single-shot dual-energy imaging with sandwich detector
- $C_j = |p_{jM}^{DE} - p_{jM}^{DE}| = |(w_j \Delta\mu_{jM}^F - \Delta\mu_{jM}^R)t_j + (w_j \Delta\mu_{jM}^F - \Delta\mu_{jM}^R)t_j|$



Noise

- Noise of single-shot dual-energy imaging with sandwich detector
- $\sigma_j^2 = \sigma_{j,\text{det}}^2 + \sigma_{j,\text{obj}}^2$, $\sigma_{j,\text{obj}}^2 = w_j^2 (\sigma_{\text{obj}}^F)^2 + (\sigma_{\text{obj}}^R)^2$



Noise with object noise

- Noise of single-shot dual-energy imaging with sandwich detector considering object noise

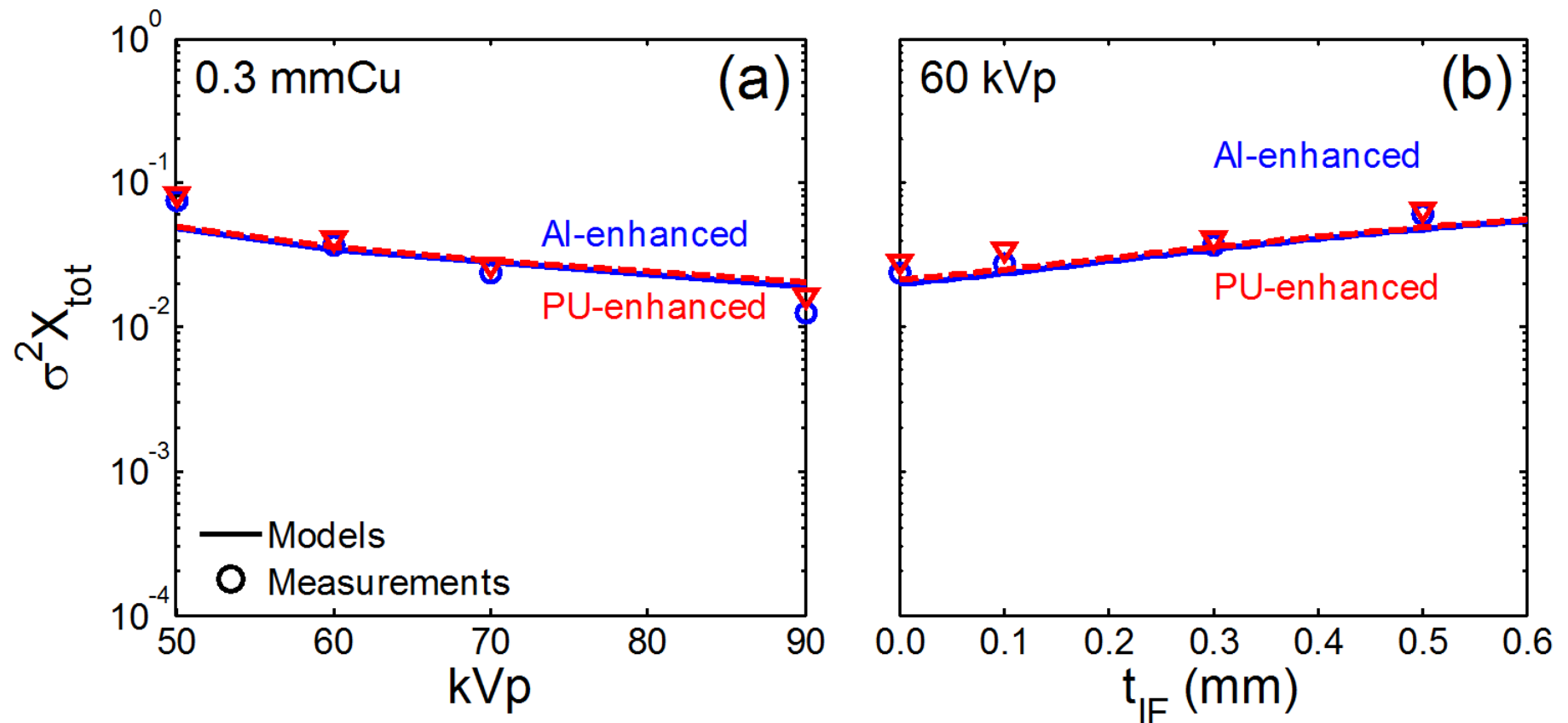
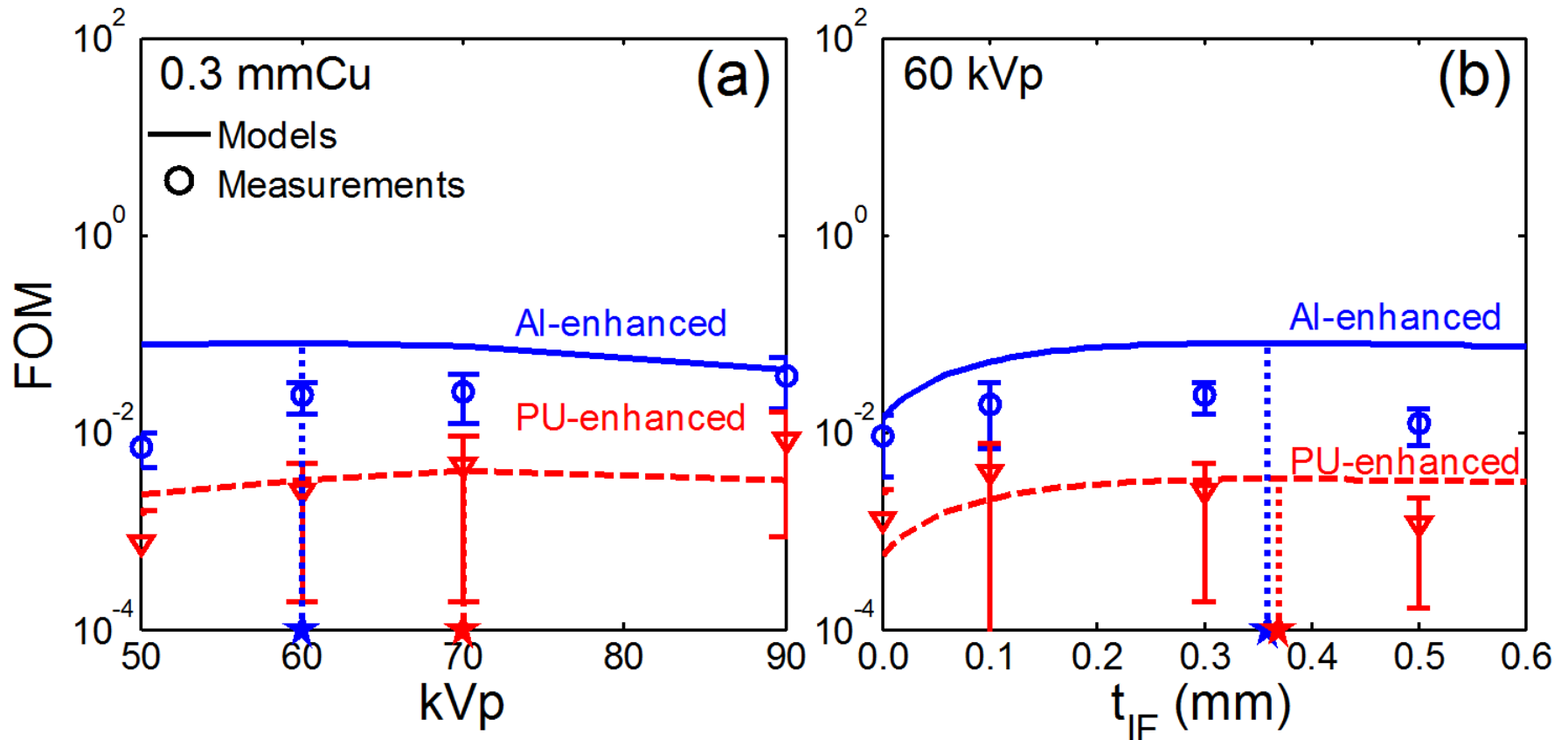


Figure of merit with object noise

- FOM of single-shot dual-energy imaging with sandwich detector considering object noise

$$\text{FOM}_j = \frac{\text{CNR}_j^2}{X} = C_j^2 \left[X \left\{ w_j^2 \left((\sigma_{\text{det}}^F)^2 + (\sigma_{\text{obj}}^F)^2 \right) + (\sigma_{\text{det}}^R)^2 + (\sigma_{\text{obj}}^R)^2 \right\} \right]^{-1}$$



Conclusion

- Noise components in dual-energy images were successfully computed and verified using zero-frequency components
- Using the linear cascaded system, we calculated the contrast and noise in dual-energy images, and developed the FOM model
- Successful validation using FOM model with anatomical structure noise
- The optimal design parameters of sandwich detectors for mouse imaging are tube voltage of 60 kVp and intermediate Cu filter thickness of 0.36 mm
- We plan to apply this model to further study the use of mammography and chest radiography imaging systems