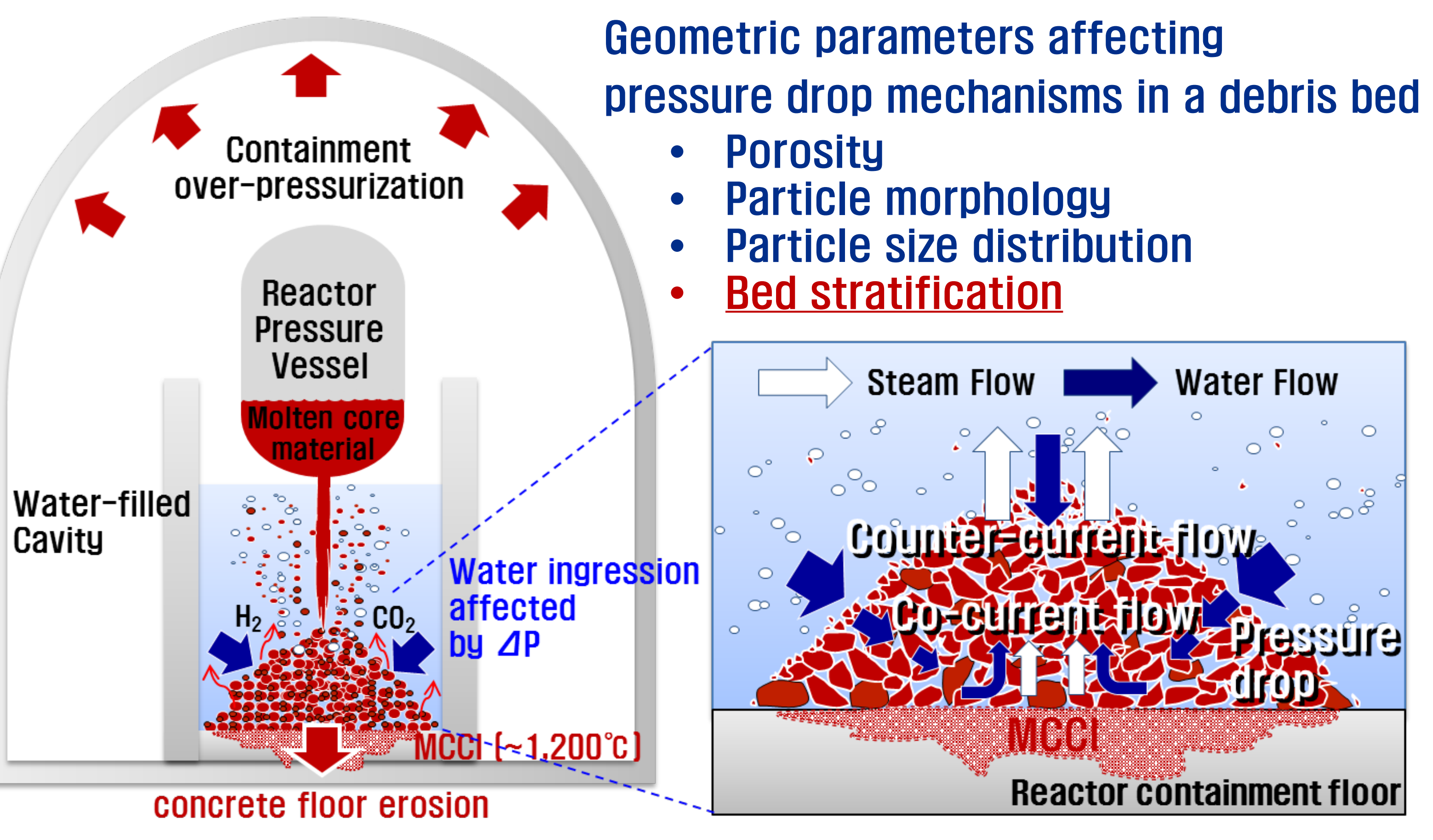


Pressure Gradients of Air and Water/Air Two-Phase Flow in a Stratified Bed

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Introduction



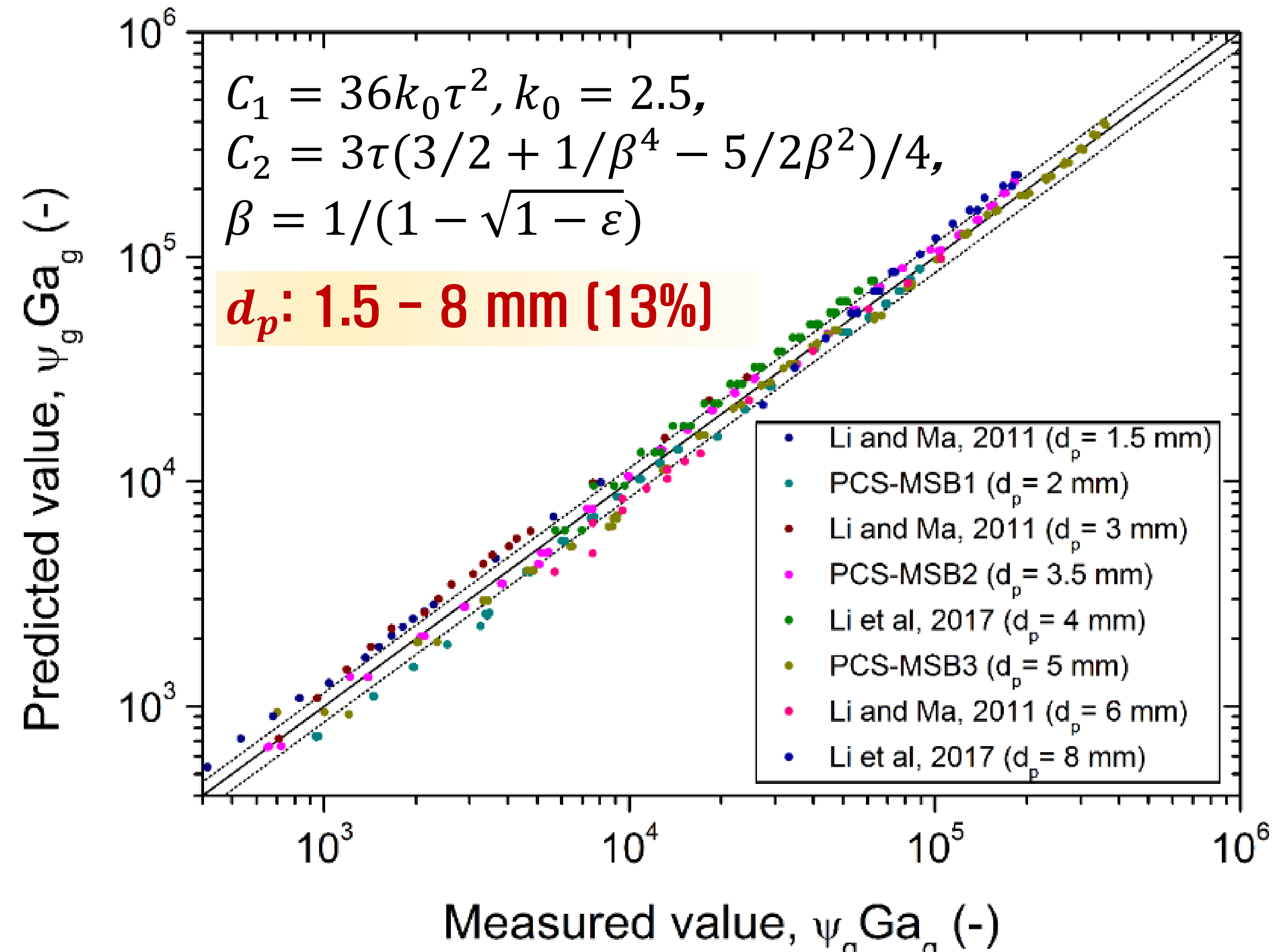
Proposed models through our previous studies

Single-phase flow

$$\frac{-dp/dz - \rho_i g}{\rho_i g} = \psi_i = C_1 \frac{Re_p}{Ga_i} + C_2 \frac{Re_p^2}{Ga_i}$$

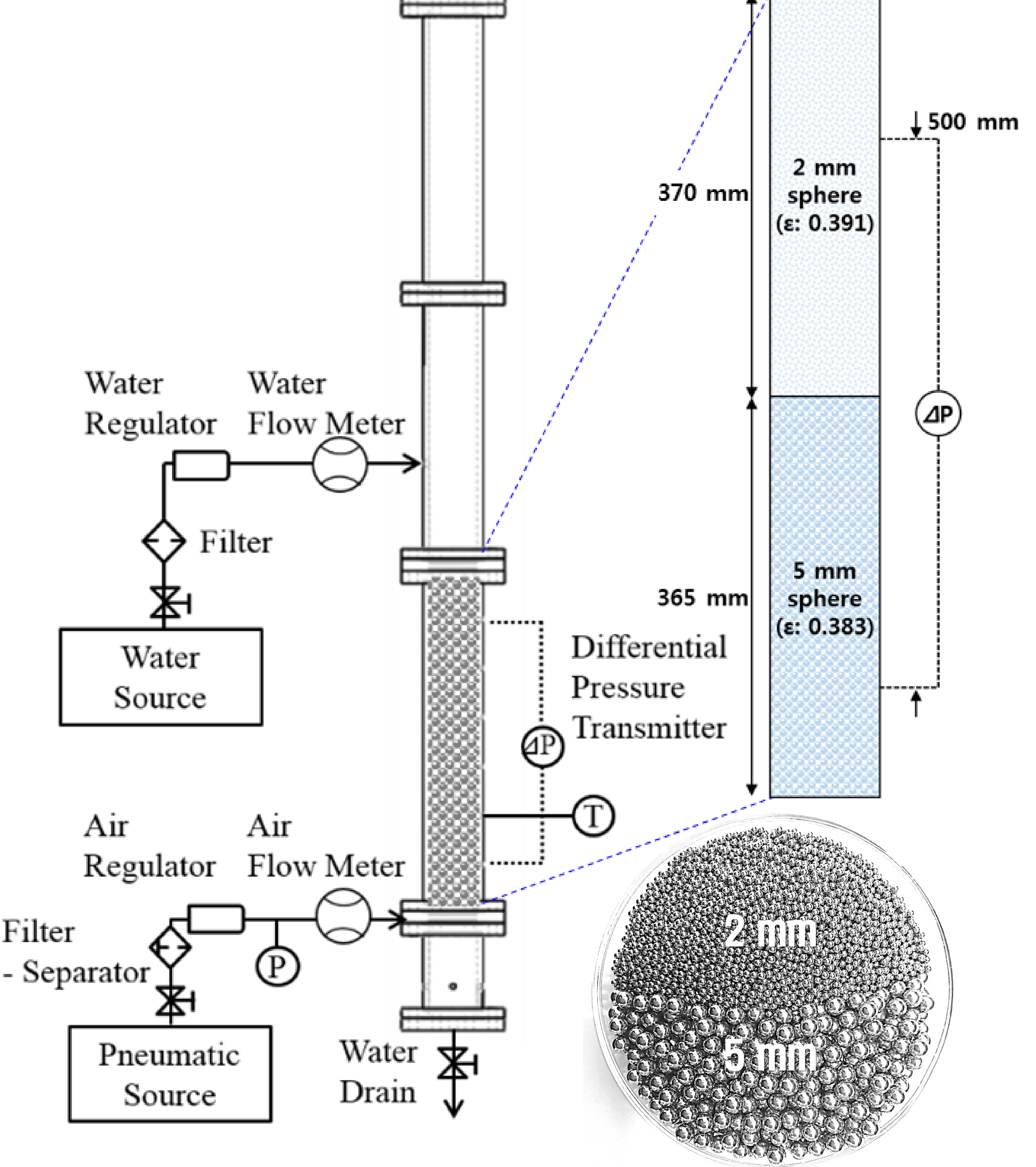
$$Re_p = \frac{\rho_i V_{si} d_p}{\mu_i (1-\epsilon)}, \quad Ga_i = \left(\frac{\rho_i}{\mu_i} \right) g \left(\frac{d_p \epsilon}{(1-\epsilon)} \right)^3$$

$$\tau = \frac{L_t}{L} = \frac{1}{2} \left[1 + \frac{1}{2} \sqrt{1-\epsilon} + \frac{\sqrt{1-\epsilon}}{1-\sqrt{1-\epsilon}} \sqrt{\left(\frac{1}{\sqrt{1-\epsilon}} - 1 \right)^2 + \frac{1}{4}} \right]$$



Experiments

PICASSO experimental facility & Test case



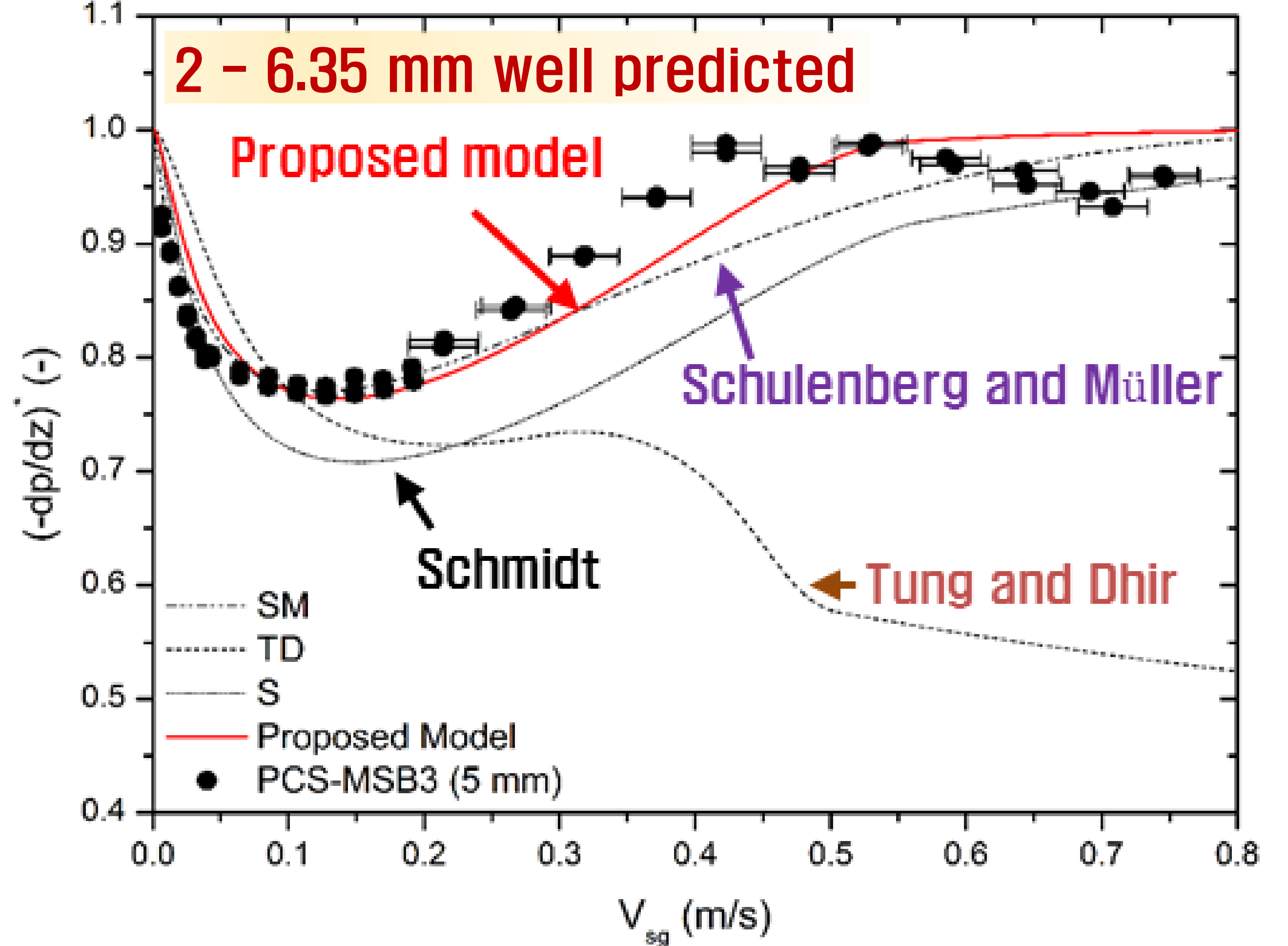
Exp. cases	Particle morphology	Particle size [mm]	Porosity [-]
PCS-SSB1	Sphere	2, 5 (mass 1 : 1)	0.387

Two-phase flow

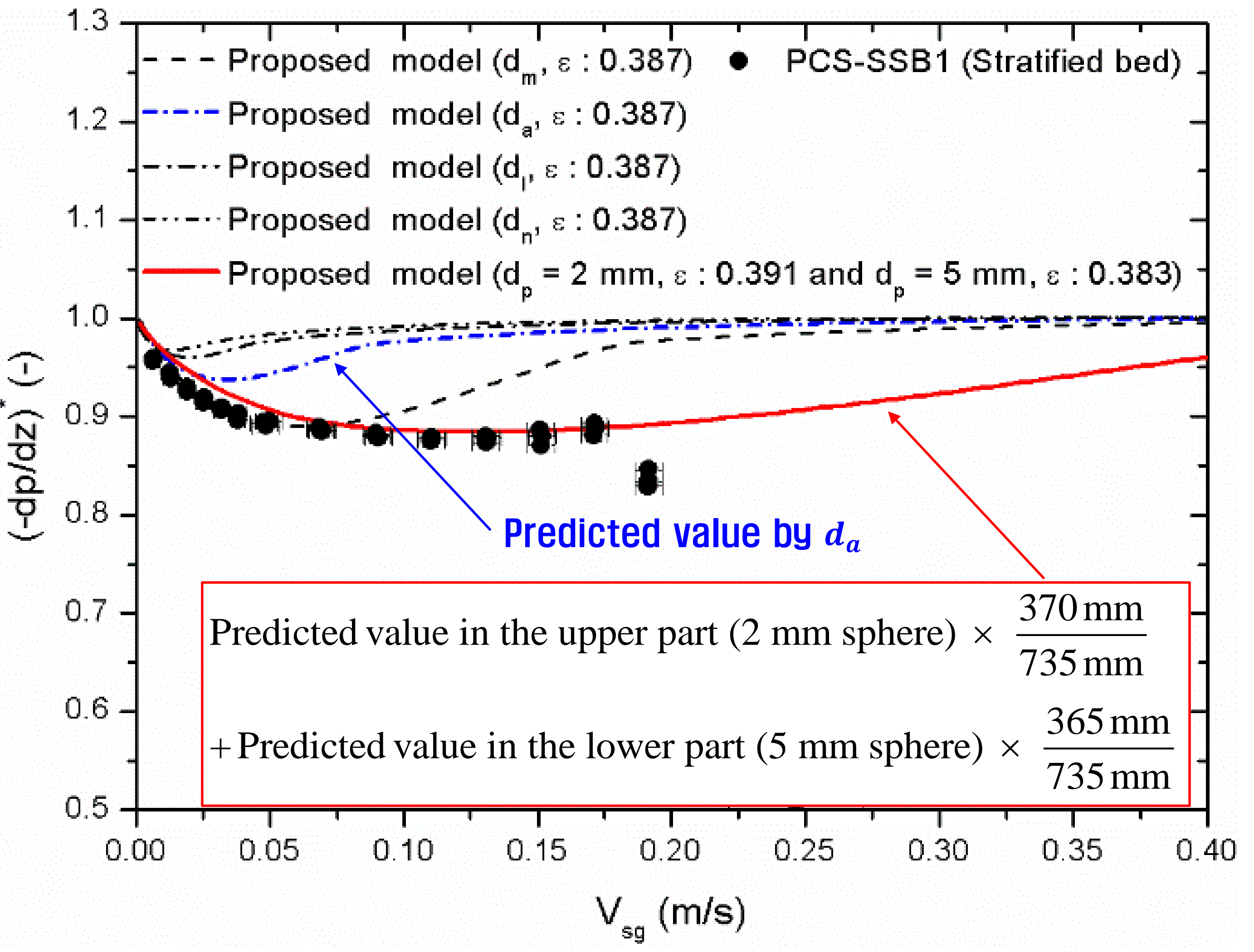
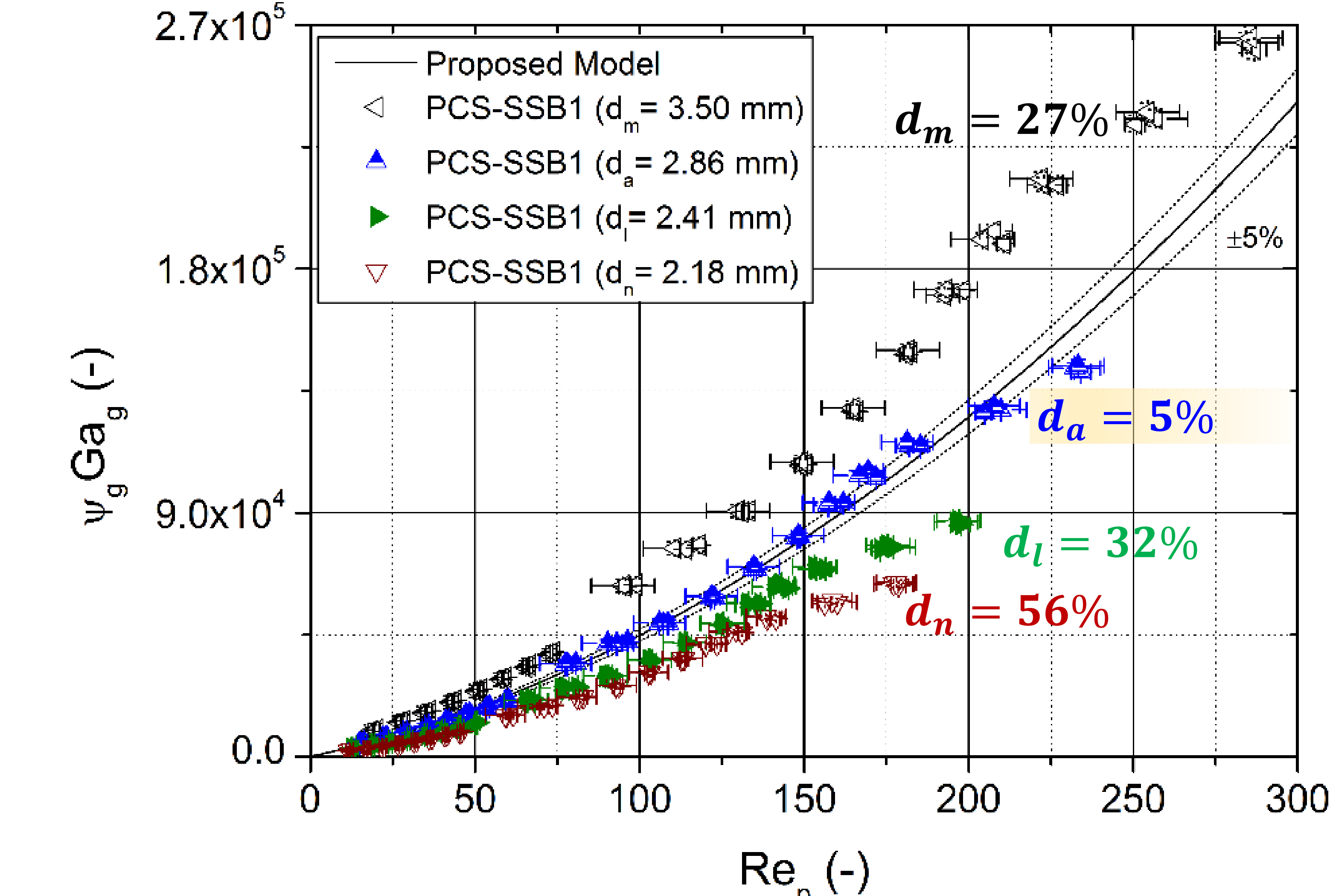
$$\left(\frac{dp}{dz} \right)^* = \frac{-dp/dz}{(\rho_l - \rho_g)g} = \frac{\rho_l g}{(\rho_l - \rho_g)g} + \frac{F_{pl}^*}{s} - \frac{F_i^*}{s} = \frac{\rho_g g}{(\rho_l - \rho_g)g} + \frac{F_{pg}^*}{\alpha} + \frac{F_i^*}{\alpha}$$

$$F^* = \frac{F}{\epsilon(\rho_l - \rho_g)g}$$

$$F_{pl} = \epsilon s \left(\frac{\mu_l}{KK_{rl}} V_{sl} + \frac{\rho_l}{\eta\eta_{rl}} V_{sl} |V_{sl}| \right), \quad F_{pg} = \epsilon \alpha \left(\frac{\mu_g}{KK_{rg}} V_{sg} + \frac{\rho_g}{\eta\eta_{rg}} V_{sg} |V_{sg}| \right)$$



Experimental results and conclusions



- [Air Flow]
 - Proposed model predicts pressure gradients of air flow in a stratified bed within **5%** with d_a .
- [Water/Air Two-Phase Flow]
 - Proposed model **adopting d_n does not predict** pressure gradients of water/air two-phase flow in contrast to air flow results.
 - Proposed model **predicts** pressure gradients of water/air two-phase flow **by means of averaging according to the bed height** after calculating the upper [2 mm sphere, $\epsilon: 0.391$] and lower [5 mm sphere, $\epsilon: 0.383$] parts of the bed.

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