

# Heat Load Estimation of the Cryomodule for 200 MeV Energy Upgrade at KOMAC

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## ■ 우주 / 대기 방사선 환경

### □ 우주 방사선 환경

- Proton: 1~500 MeV,  $10^3 \sim 10^9$  p/cm<sup>2</sup>/s, SEE
- Heavy ion: (He~Fe), multi GeV/n,  $10^5$  ions/cm<sup>2</sup>/s

### □ 대기 방사선 환경 (Neutron flux at atmosphere with energy > 10 MeV)

- 6000 n/cm<sup>2</sup>/hr (@ 12 km high)
- 20 n/cm<sup>2</sup>/hr (@ sea level)

## ■ 최근 반도체의 고 집적화로 인해 위의 대기 / 우주 방사선에 의한 반도체 영향평가가 중요해짐

### □ 반도체에의 영향

- Single Event Effect, Total Ionizing Dose, Displacement Damage

### □ 반도체의 우주 / 대기 방사선 영향시험 국제기준

- JEDEC JESD 89A: 14 MeV neutron, 50~60MeV proton, 90~100MeV proton, min. **200 MeV proton**
- ESA ESCC 25100: 20~**200 MeV proton**
- **200 MeV 양성자**를 이용하여 중성자를 발생시키는 경우 대기 방사선 스펙트럼의 90%이상을 구현할 수 있음

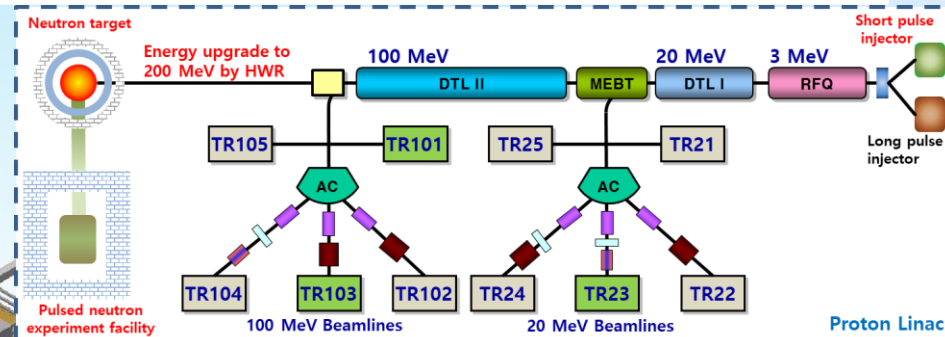


# 200-MeV Energy Upgrade

## 200-MeV 에너지

- 대기 방사선의 90% 이상을 cover 할 수 있음
- 국제 시험 기준을 만족하는 전용 시설로 구축 가능
- 단일 구조의 초전도 가속기 사용 가능 (200-MeV 이상에서는 elliptical cavity + klystron 이 유리함)
- 기존 100-MeV 가속기 터널을 대규모 증축하지 않고 가속기를 설치할 수 있음

Included in the National R&D roadmap



Facility site plan

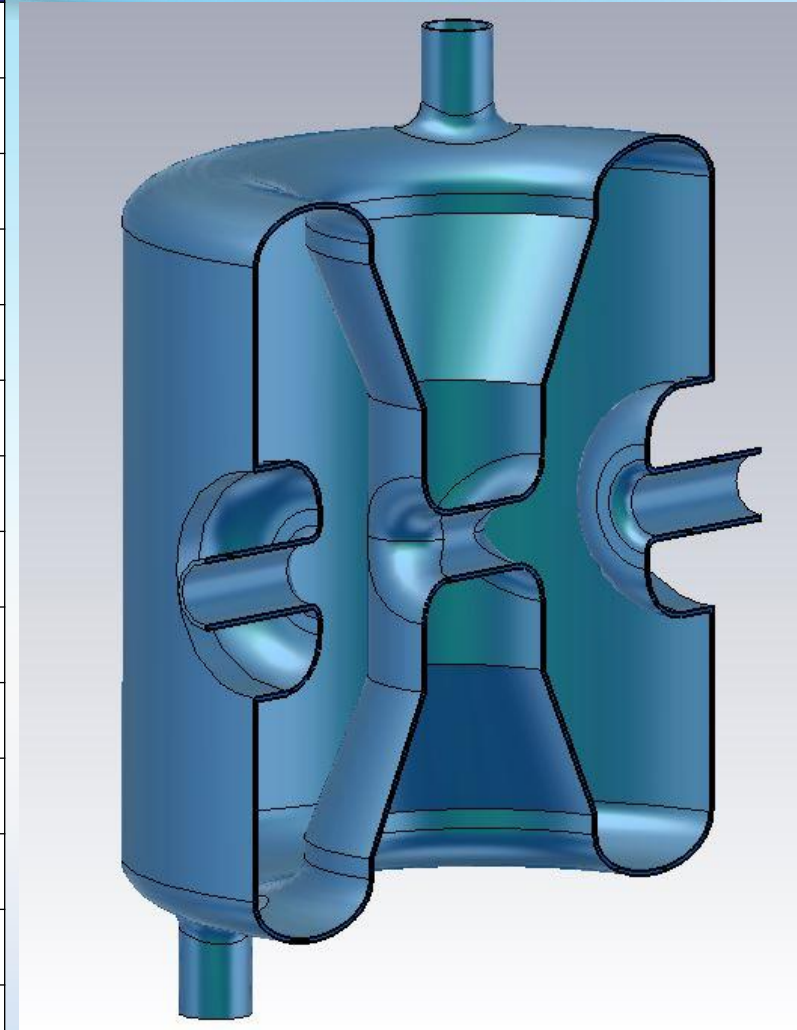


- Frequency: 350 MHz
- Beam energy: 100 MeV ~ 200 MeV
- Peak current: 20 mA
- RF duty: 10%
- Length: ~45 m
- Optimum beta: 0.56
- Eacc: 7.5 MV/m ( $E_p < 35$  MV/m,  $B_p < 70$  mT)
- Operation temperature: 2 K
- HWR per CM: 4 HWRs / cryomodule
- Total no. of CM: 9 sets
- Total no. of HWR: 36 sets
- Focusing: Normal conducting doublet



# HWR Cavity Design

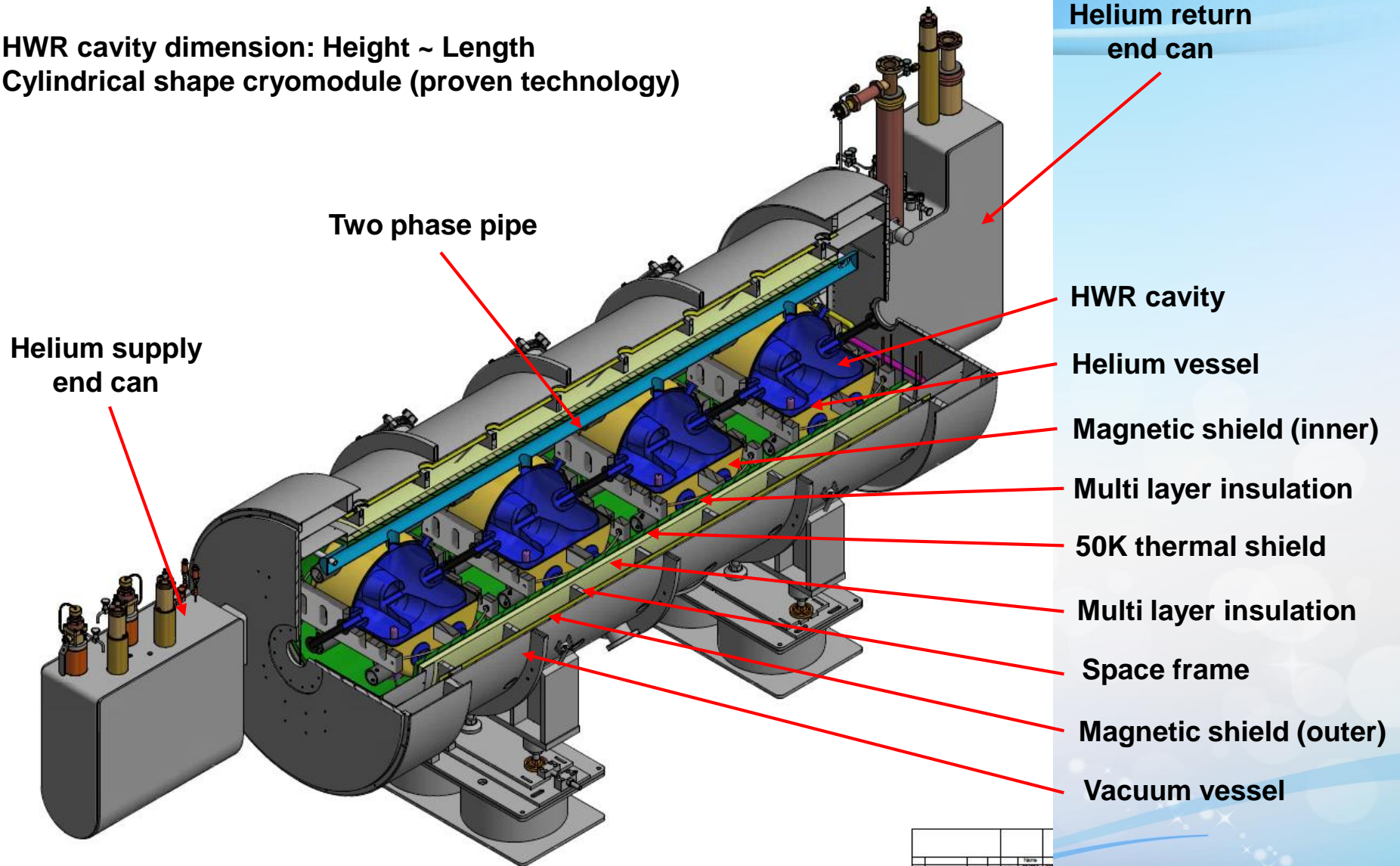
Parameter	Unit	Value
Optimum beta ( $\beta_{opt}$ )	-	0.56
$V_{acc}$ (@ $\beta_{opt}$ )	MV	3.61
$E_{acc}$ (@ $\beta_{opt}$ )	MV/m	7.53
$E_{pk}$	MV/m	29.08
$B_{pk}$	mT	61.66
$E_{pk} / E_{acc}$	-	3.86
$B_{pk} / E_{acc}$	mT/(MV/m)	8.19
$V_0$	MV	4.14
$E_0$	MV/m	8.63
$R/Q$ (@ $\beta_{opt}$ )	Ohm	256.6
$G$	Ohm	116.1
$Q_0$ (@ $R_s=20$ n $\Omega$ )	-	5.81E+9
Cavity loss (@ $R_s=20$ n $\Omega$ )	W	8.75
Stored energy	J	23.1
Cavity diameter	m	0.45



- **Concept: Use well proven technology**
- **Cylindrical cryomodule (based on SNS CM)**
  - **Cavity dimension: height ~ diameter**
  - **Focusing: External normal conducting doublet**
  - **Widely used in large facilities (ex. CEBAF, SNS, ESS and so on)**
- **HWR operating temperature: 2 K**
- **HWR cavities / cryomodule: 4**
- **HWR fixing and alignment: Space frame**

# Cryomodule

HWR cavity dimension: Height ~ Length  
Cylindrical shape cryomodule (proven technology)

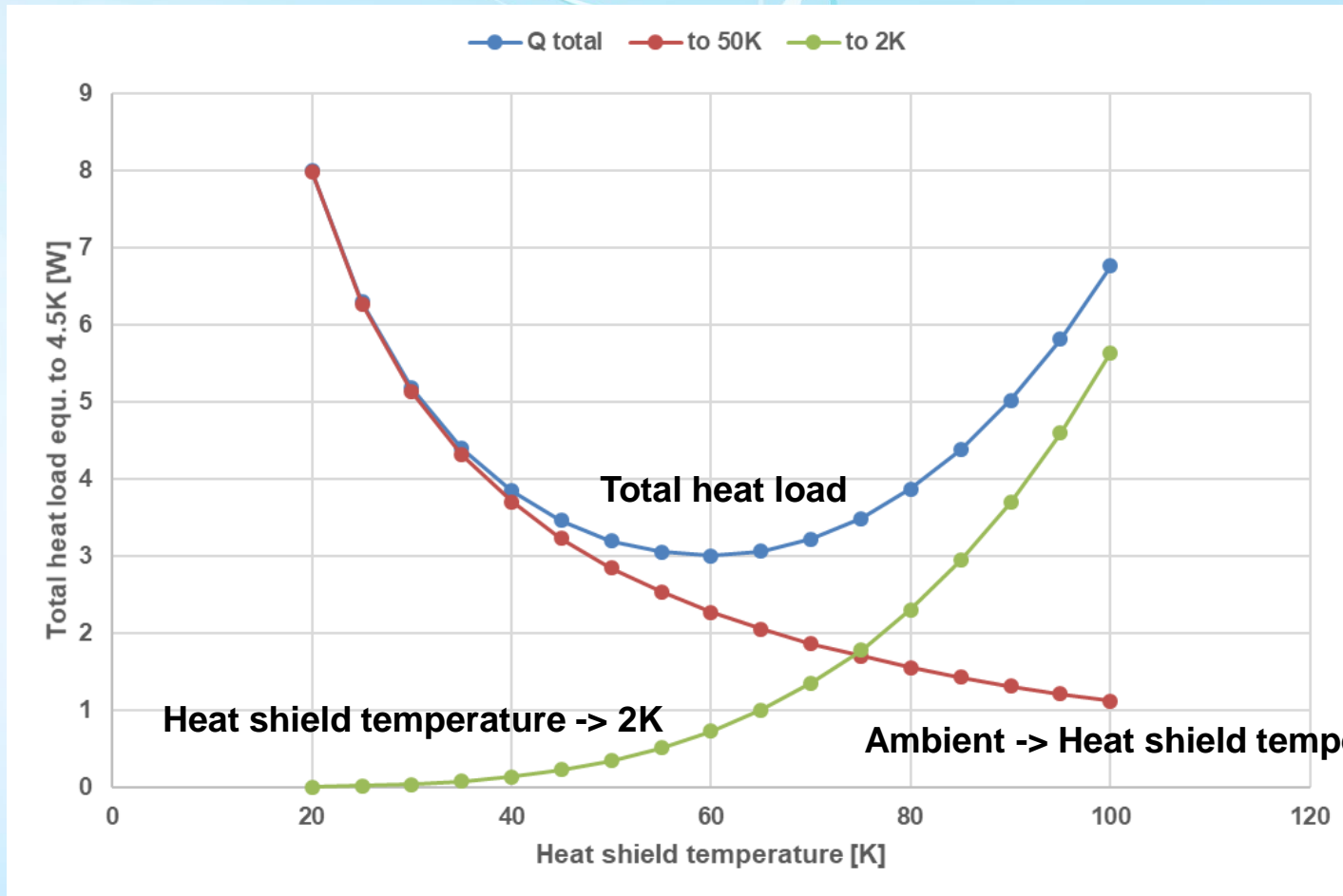




# Static Heat Load - Radiation

- Worst case in radiation heat transfer\*

300 K -> 50 K: 2.5 W/m<sup>2</sup>, 50 K -> 2 K: 94 mW/m<sup>2</sup>





# Static Heat Load - Conduction

$$\bar{k}(T1, T2) = \bar{k}(0, T2) - \bar{k}(0, T1)$$

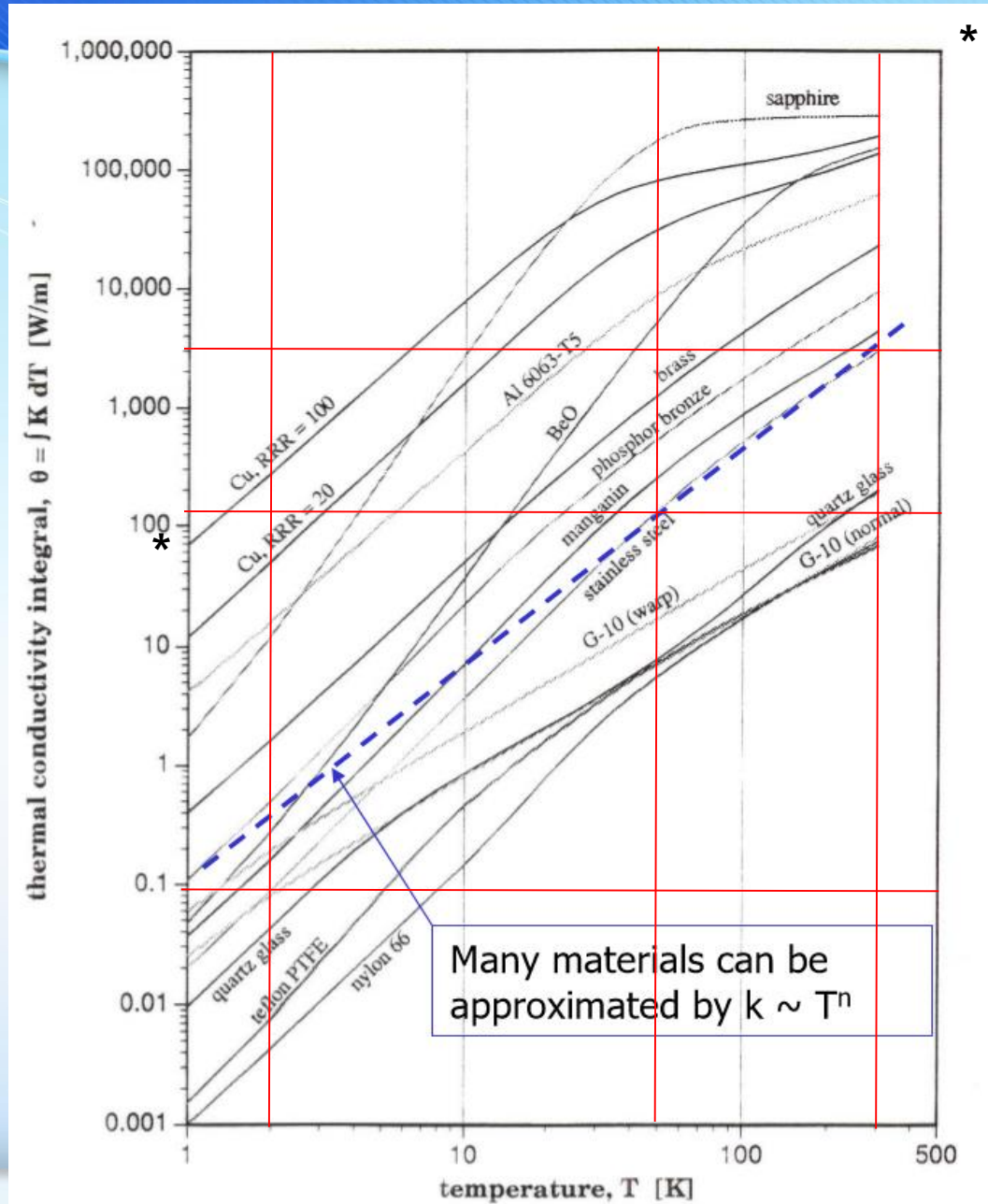
For example, stainless steel

$$\bar{k}(2, 300) = 3,000 - 0.09 = 3,000 \text{ [W/m]}$$

$$\bar{k}(2, 50) = 120 - 0.09 = 120 \text{ [W/m]}$$

$$\bar{k}(50, 300) = 3,000 - 120 = 2,880 \text{ [W/m]}$$

- In general, a pressure of  $10^{-6}$  mbar or less is sufficient vacuum to eliminate all convective heat transfer
  - The cold wall of the vacuum space acts as a cryopump for residual gas
  - But need another pump to reduce the pressure near  $10^{-6}$  mbar prior to cool down the cryostat



$$P_c = \frac{E_{acc}^2 d^2}{Q_0} \frac{1}{R/Q} DF = \frac{V_{acc}^2}{Q_0 R/Q} DF$$

$$V_{acc} = 3.61 \text{ MV}$$

$$R/Q = 256.6 \text{ ohm}$$

$$Q_0 = 5.81E9$$

$$P_c = 8.74 \text{ W / cavity @ 100\% duty}$$

$$P_c = 0.874 \text{ W / cavity @ 10\% duty}$$

$$P_c = 3.5 \text{ W / cryomodule @ 10\% duty}$$

# Heat Load per Cryomodule

KOMAC HWR Cryomodule heat load (200708)

	SNS Medium	SNS High	KOMAC
Slot length [m]	5.839	7.891	
CM length [m]	4.239	6.291	3.582
CM diameter (OD) [m]	1.22	1.22	1.154
CM outer surface are [m2]	18.585	26.450	15.078
Conversion factor from SNS to KOMAC			0.811

Calculated heat load

	Qty	2.1K	50K	Qty	2.1K	50K	Qty	2.1K	50K
Static [W]	1	9.7	131.0	1	11.5	161.0	1	11.0	143.6
U tube & Allotment [W]	1	10.0	24.0	1	10.0	30.0	1	10.0	24.0
Dynamic [W]	1	8.3	0.0	1	17.1	0.0	1	8.1	0.0
Total heat load per CM [W]		28.0	155.0		38.6	191.0		29.1	167.6
Budget per CM		39.0	170.0		48.0	200.0		36.2	175.5

**130 W / CM @ 4.5 K equivalent**

Dynamic contribution

Cavity	3	6.0		4	14.0		4	7	
Power coupler	3	0.6		4	0.8		4	0.8	
Bellows	2	0.2		3	0.3		3	0.3	
HOM	3	1.5		4	2.0		0	0	
Total dynamic		8.3			17.1			8.1	

Static contributions

Radiation - HV & Bellows	3	1.1	41.7	4	1.8	65.3	4	1.00	37.75
Power coupler (radiation)	3	2.1		4	2.8		4	2.80	
Tuner	3	0.75		4	1		4	1.00	
He vessel Supports	3	0.2	18	4	0.3	24	4	0.27	24.00
Warm Beam Tube Conduction	2	0.1	2	2	0.1	2.5	2	0.54	12.97
Warm Beam Tube Radiation	2	0.9	0.9	2	0.9	0.9	2	0.90	0.90
Cables (3 per cavity)	1	0.5	1.8	1	0.5	1.8	1	0.50	1.80
Sub total CM		5.65	64.4		7.4	94.5		7.01	77.42
Supply Bayonets	2	1	12	2	1	12		1	12
Radiation	1	0.04	9	1	0.04	9		0.04	9
PC JT Valve	1	0.25	2	1	0.25	2		0.25	2
Subcooler JT Valve	1	0.25	2	1	0.25	2		0.25	2
Shield Relief	2	0	4	2	0	4		0	4
5K Transfer Line	1	0.1	0	1	0.1	0		0.1	0
50K Transfer Line	1	0	3	1	0	3		0	3
Sub total Supply Bayonets		1.64	32		1.64	32		1.64	32
Return Bayonets	2	1.5	6	2	1.5	6		1.5	6
Radiation	1	0.1	11.2	1	0.1	11.2		0.1	11.2
Cooldown / PC Return	1	0.25	10	1	0.25	10		0.25	10
Shield Relief	1	0.3	2	1	0.3	2		0.3	2
Cooldown Valve	1	0.25	2	1	0.25	2		0.25	2
5K Transfer Line	1	0	0	1	0	0		0	0
50K Transfer Line	1	0	3	1	0	3		0	3
Sub total Return Bayonets		2.4	34.2		2.4	34.2		2.4	34.2
Total static		9.69	130.6		11.44	160.7		11.0	143.6



- **Energy upgrade of existing 100 MeV proton linac**
  - **Space / Atmospheric radiation test facility on semiconductor with 200 MeV proton linac**
  - **HWR based superconducting linac**
- **Cryomodule heat load estimation**
  - **Static: radiation, conduction**
  - **Dynamic: cavity**
  - **Total heat load: 130 W / CM @ 4.5 K equivalent**