

# Oxidation, hydriding, and the buildup of corrosion products (crud) for Zr-based cladding

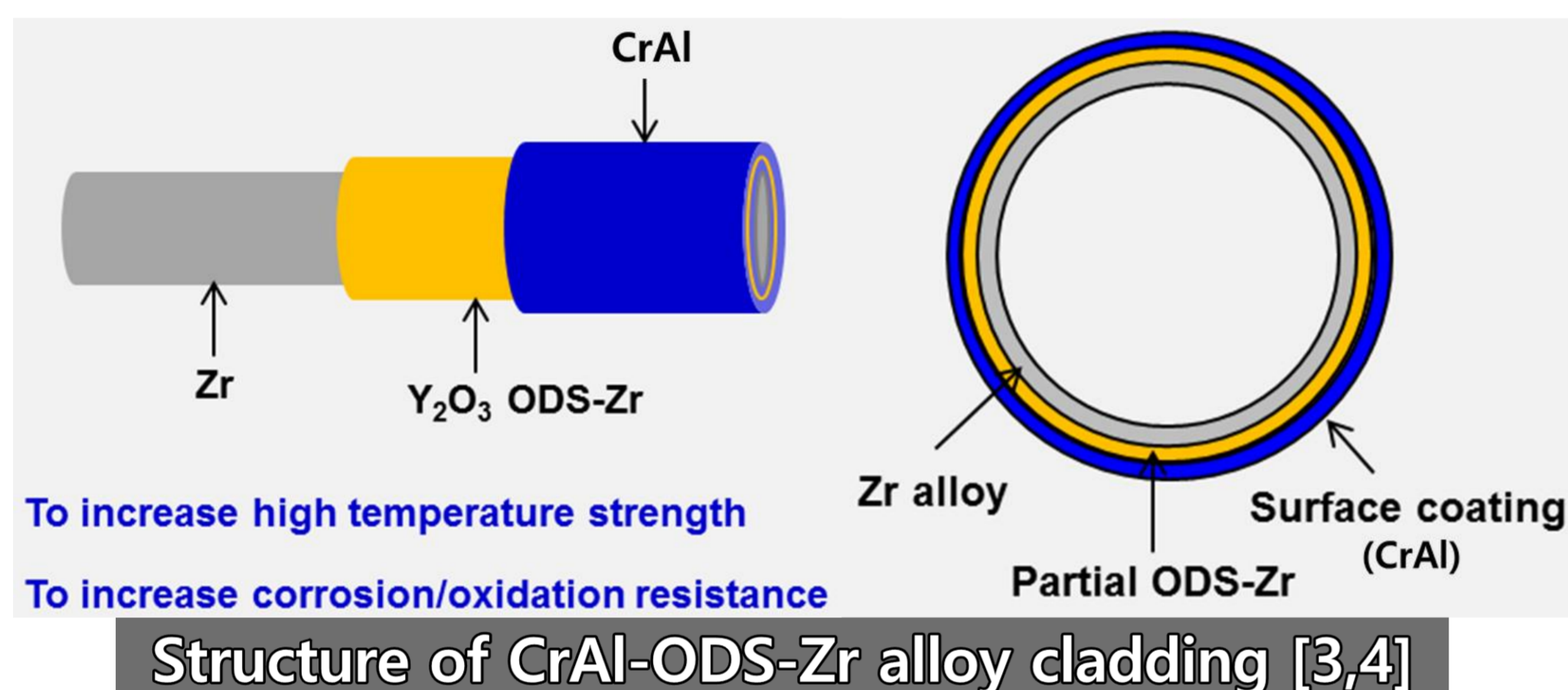
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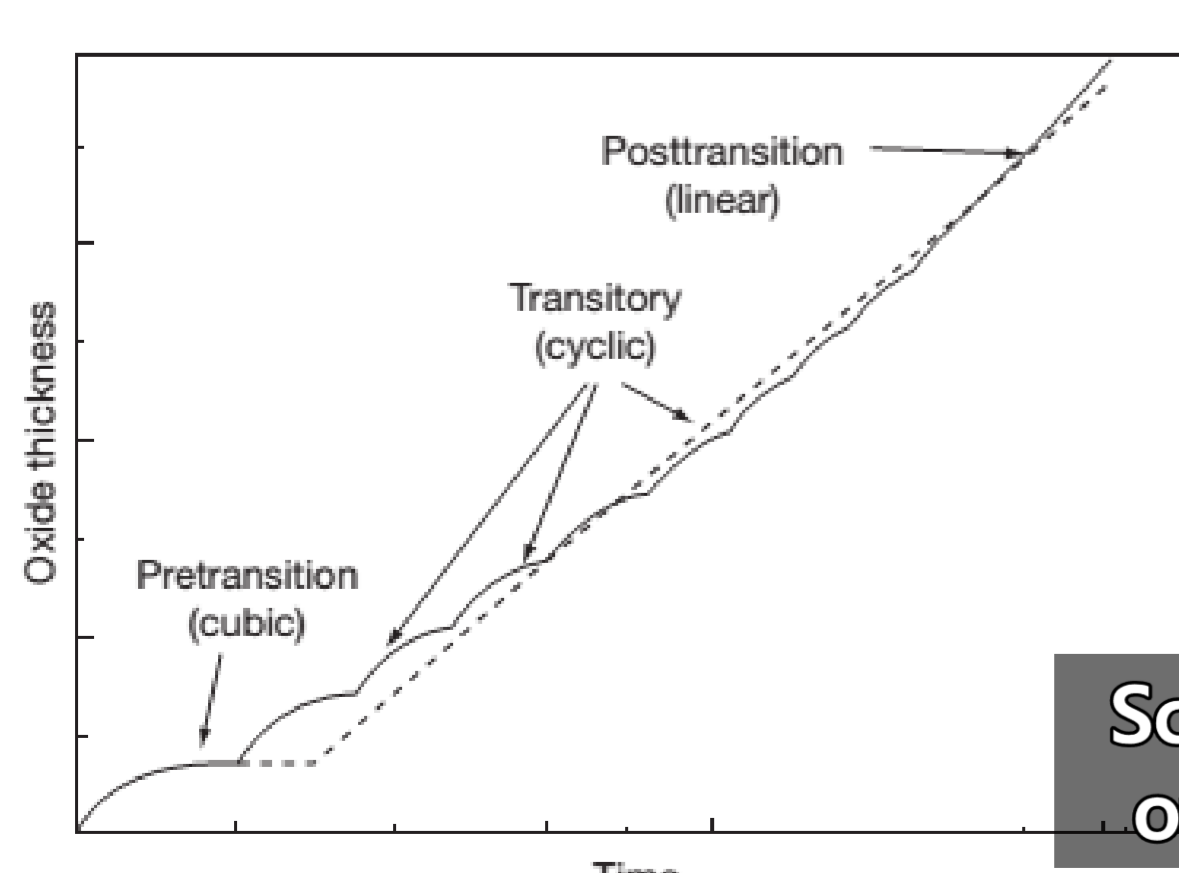
## Introduction

- Oxidation, hydriding, and the buildup of CRUD
  - Degrade cladding ductility, decreases in thermal conductivity and load-bearing thickness, Oxide spallation, etc.
  - Act as a heat transfer barrier => CILC / AOA
  - Acceptance criteria in regulatory SRP 4.2 [1,2]
    - Limited based on mechanical testing to demonstrate that each component maintains acceptable strength and ductility
    - Allowable levels and demonstration of acceptability on SAR
    - Effects in the thermal and mechanical fuel analyses
    - Effect of CRUD on T-H / neutronic (AOA) considerations
- Coated ATF cladding
  - Couldn't simply apply existing limits due to limited relevant knowledge & limited data
- In this study, those of ATF cladding (CrAl-ODS-Zr alloy) is qualitatively studied and its effect on fuel in-reactor behavior is discussed for PIRT development study
  - CrAl-ODS-Zr alloy ATF cladding [3,4]
    - CWSR Zry-4 cladding + Partial ODS treatment ( $Y_2O_3$ ) by laser beam scanning (LBS) + CrAl coating by arc ion plating (AIP)



## Oxidation, hydriding, and the buildup of corrosion products (crud) for Zr-based cladding

- Oxidation & Hydriding
  - Dependent on the various parameters (e.g. temperature,  $Zr(Fe,Cr)_2$ , hydrogen segregation at oxide/matrix interface, dissolved oxygen, irradiation, Li concentration)
  - Design limit at EOL [5]
    - : 100  $\mu m$  (Oxide) and 500–600 ppm (Hydrogen)
  - Limiting parameter the length of time that fuel rod can safely be left in reactors
  - Garzarolli's model : Approximated pre-transition region (cubic rate law) and post-transition region (linear rate law)
    - Most of models on the fuel performance codes (e.g. FRAPCON, EPRI/KWU/CE, ESCORE, EPRI SLI, NE PLC etc.)
  - Hydriding : constant HPUF (hydrogen pickup fraction)
    - On FRAPCON, they depend on the material type (e.g. 0.15 for Zry-4, 0.1 for M5, 0.175 for ZIRLO/Opt. ZIRLO) [8]



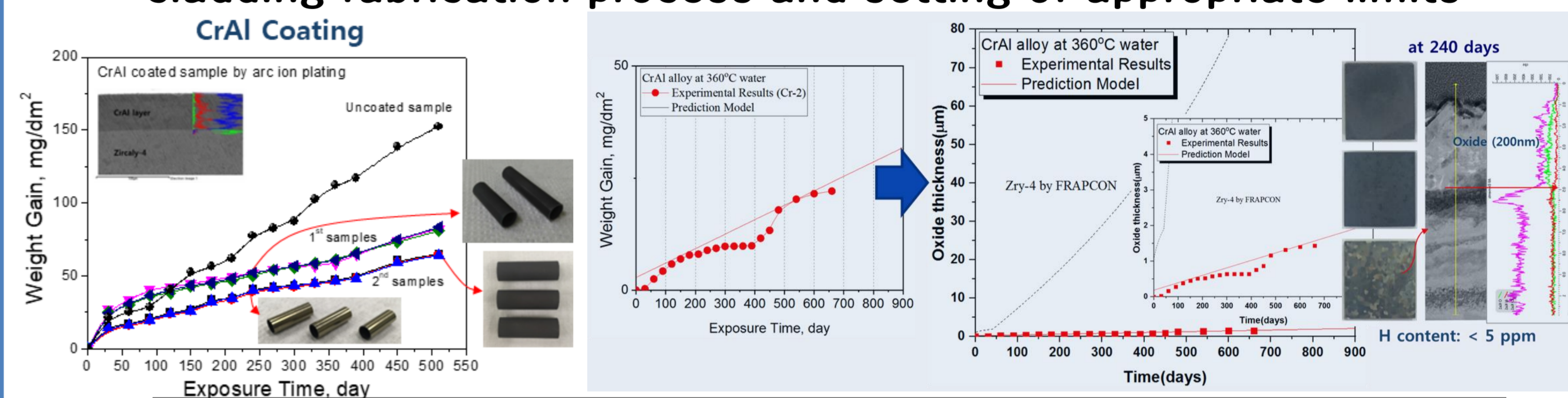
Schematic diagram of the oxidation rate of Zr-alloy during normal operation [7]

- CRUD
  - No relevant design limit
  - On FRAPCON, reflect CRUD effect on temperature analysis (no deposition model)

## Oxidation, hydriding, and the buildup of corrosion products (crud) for CrAl-ODS-Zr alloy ATF cladding

### • Oxidation & Hydriding

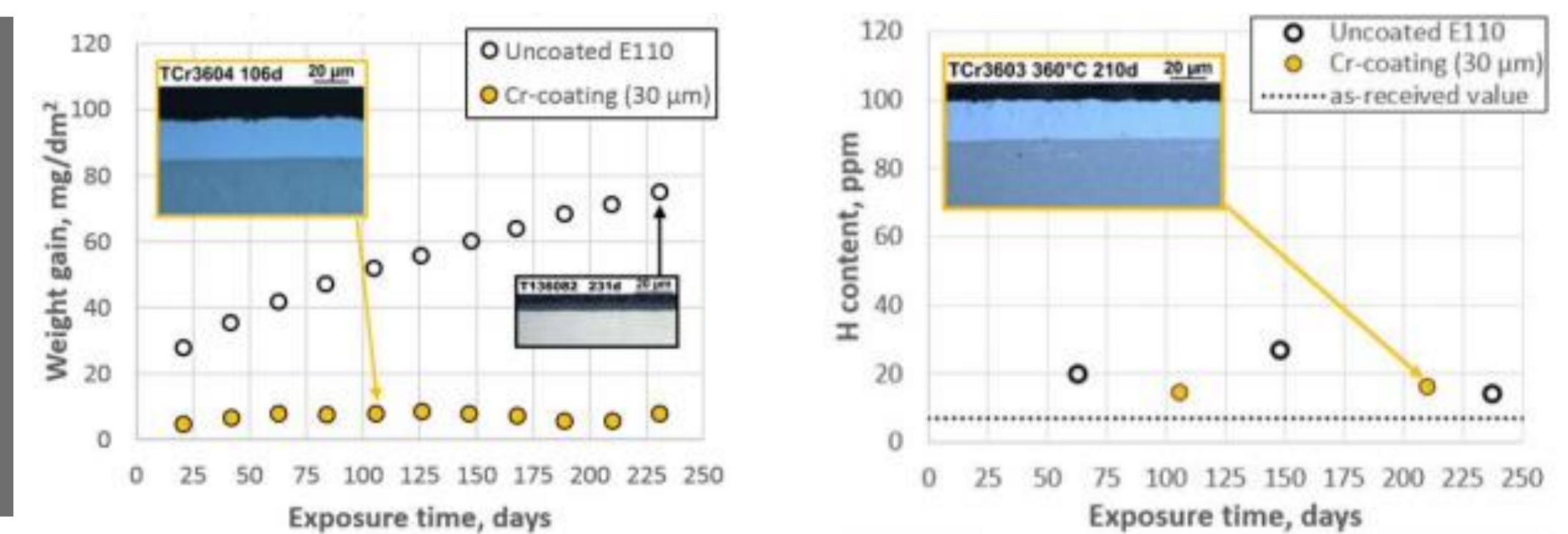
- Only outermost layer (CrAl) exposed to primary water need to be considered as long as coating layer maintains intact
  - Highly improved oxidation resistance without local flaking and galvanic corrosion
  - Prediction model : Considering only uniform corrosion
- Most of Cr/CrAl data based on ex-reactor test (need to confirm by PIE of LTRs & evaluated based on in-reactor data)
- Coating cracking and defects can be solved by optimization of cladding fabrication process and setting of appropriate limits



Oxidation properties of CrAl coated cladding (a) Autoclave test under 360°C simulated PWR environment, (b) Prediction model [10,11]

- Hydriding : protective  $Cr_2O_3$  prevent to diffuse hydrogen into Zr matrix and very low hydrogen pickup is anticipated
  - (M. Ševeček et al) high hydrogen pickup fraction for Cr-coated
  - Scatter? Need further examinations and in-reactor tests

Ex-reactor oxidation and hydriding properties of Cr-coated E110 cladding (360°C, 197 bar, simulated WWER env.) [12]



### • CRUD

- Significantly decreases the deposition rate for CrAl coated Zry-4 cladding using static autoclave at 360°C for 200 days
- Need additional ex-reactor and in-reactor test
- Limits for CrAl-ODS-Zr alloy ATF cladding
  - Zr-thickness is maintained => Existing design limits could be similarly applicable to Zr matrix with additional margin
    - + limits for preventing coating cracking/delamination
  - Or separate limits based on the oxidation/mechanical test
  - No necessity for specific limit of CRUD buildup, but should be evaluated by PIE of LTRs and monitored in plants

## Conclusion

- Superior resistance for oxidation and hydriding (need to confirm by PIE of LTRs and evaluated based on in-reactor data)
- Existing design limits could be similarly applicable to Zr matrix, with additional margin & coating cracking/delamination consideration
- Or separate limits based on the oxidation/mechanical test
- No necessity for specific limit of CRUD buildup, and CRUD deposition rates should be evaluated and monitored in plants

## Acknowledgments & References

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- [1] KINS, Safety review guidelines for light water reactors. (Revision 6), KINS/GE-N001
- [2] US NRC, Standard review plan 4.2, NUREG-0800
- [3] H.G. Kim et al, Top fuel 2016, 17526
- [4] J.-D. Hong, J.Y. Kim, 2021 KNS spring meeting
- [5] S.S. Kang et al, KAERI/CM-1034/2007, 2008.2.
- [6] F. Garzarolli et al, EPRI NP-2789 (1982)
- [7] E. Hillner, D.G. Franklin, J.D. Smee, J. Nucl. Mater. 278 (2000) 334
- [8] K.J. Geelhood et al, PNNL-19418, Vol.1 Rev.2, September 2019
- [9] K.G. Geelhood, W.G. Luscher, PNNL-28437 Revision 1, June 2019
- [10] J.-D. Hong et al, KAERI/TR-6510/2016
- [11] C.H. Shin et al, KAERI/TR-8284/2020
- [12] J. Krejčí et al, Top fuel 2018, A0233
- [13] Z. Karoutas et al, Top Fuel 2019, Seattle, WA, Sep. 22–27, 2019