

Preliminary Study on Thermal Margin of External Reactor Vessel Cooling Using MARS-KS1.4 Code with Newly Implemented CHF Correlations

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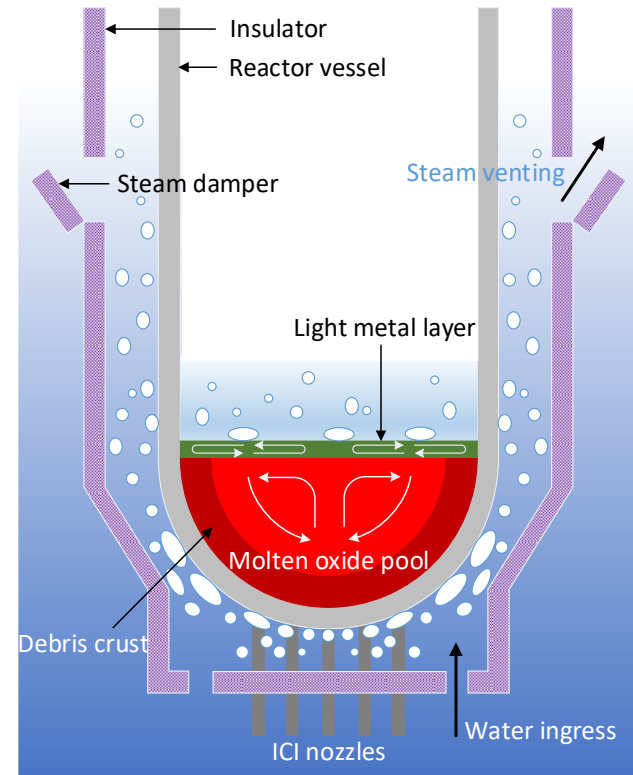
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❖ External reactor vessel cooling (ERVC)

- Severe accident management strategy adopted by APR1400 to arrest the molten core debris by flooding the reactor cavity and submerging the reactor vessel
 - Specific insulation design to promote natural circulation and heat removal
 - Principal failure mechanism : occurrence of **boiling crisis**

ERVC analysis via T/H system codes

- High-fidelity prediction of two-phase natural circulation flows, but
- **No CHF model for downward-facing hemispheres** (lower CHF than that predicted by the default model)



External reactor vessel cooling

❖ Research objectives

To implement CHF correlations proper for the downward-facing hemisphere into the MARS-KS 1.4 code to better predict the thermal margin of ERVC w/ APR1400 as the reference plant

Reviewed experimental studies on CHF for ERVC

Test	ULPU-III test	Toshiba's test	SULTAN test
Organization	University of California, Santa Barbara	Toshiba Energy Systems & Solutions Corporation	CEA
Geometry	Hemisphere	Flat plate	Flat plate
Test Facility			

❖ Selected correlations for downward-facing hemisphere

Name	Correlations	Ranges
ULPU-III correlation¹⁾	$q''_{CHF} = 490 + 30.2\theta - 8.88 \cdot 10^{-1}\theta^2 + 1.35 \cdot 10^{-3}\theta^3 - 6.65 \cdot 10^{-5}\theta^4$	$0^\circ < \theta < 90^\circ$
Toshiba correlation²⁾	$q''_{CHF} = -3626.79P^2 - 2.45025 \cdot 10^{-4}G^2 - 434757x^2 + 0.0610736\theta^2 + 2263.69P + 0.914268G - 14657.4x + 0.300264\theta + 35.5521P\theta - 2.30392 \cdot 10^{-3}G\theta + 136.071x\theta + 0.0152043PG - 1993.24Px - 6.65384Gx - 88.0463$	$50^\circ < \theta < 90^\circ$ $0.1 < P < 0.6 \text{ MPa}$ $360 < G < 1900 \text{ kg/m}^2\text{s}$ $-2.6e-2 < x < 3.1e-3$
SULTAN correlation³⁾	$q''_{CHF} = A0(E, P, G) + A1(E, G) \cdot x + A2(E) \cdot x^2 + A3(E, P, G, X) \cdot \theta + A4(E, P, G, X) \cdot \theta^2$	$\theta = 10^\circ, 45^\circ, 90^\circ$ $0.1 < P < 0.5 \text{ MPa}$ $10 < G < 5000 \text{ kg/m}^2\text{s}$ $0 < \text{Subcooling} < 50 \text{ K}$

P: pressure, *G*: mass flux, *x*: quality,
E: channel gap

Flow effect on CHF reflected



- 1) T.G. Theofanous et al., Nuclear Engineering and Design 169 (1997)
- 2) C. Iwaki et al., Journal of Nuclear Science and Technology 57 (2020)
- 3) S. Rouge et al., Workshop on in-vessel core debris retention and coolability (1998)

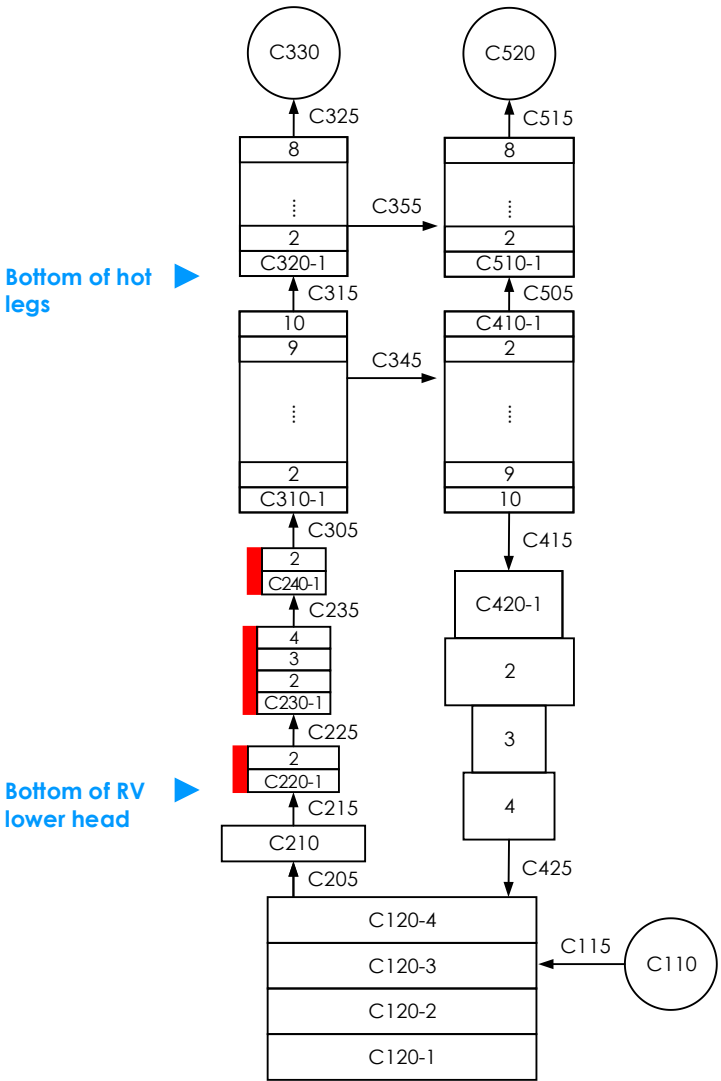
❖ Implementation into MARS-KS1.4

Three subroutines for the selected CHF correlations were added to source files of the MARS-KS 1.4 code → convective boundary condition types in ‘heat structure’

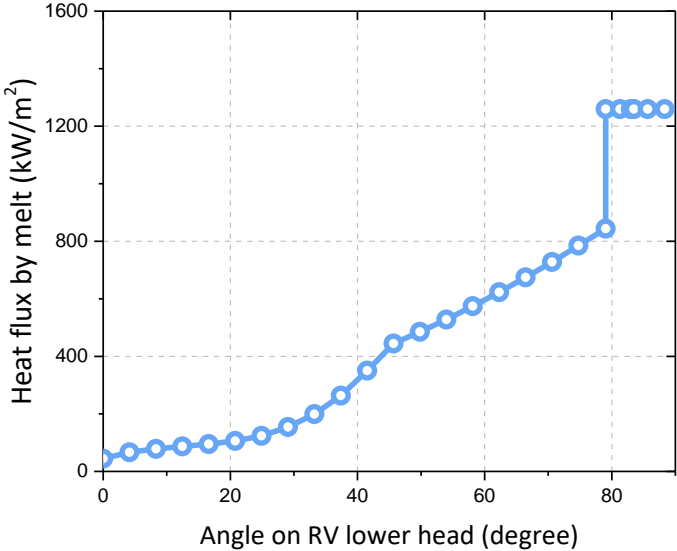
Modified convection boundary type in heat transfer package

Index	Geometry type	
1, 100, 101	Default	
102	Parallel plates	
...	...	
135	Helical S/G shell side	
190	Downward -facing hemisphere	ULPU-III correlation
191		Toshiba correlation
192		SULTAN correlation

MARS-KS Simulation



Nodalization of the natural circulation flow channels during ERVC

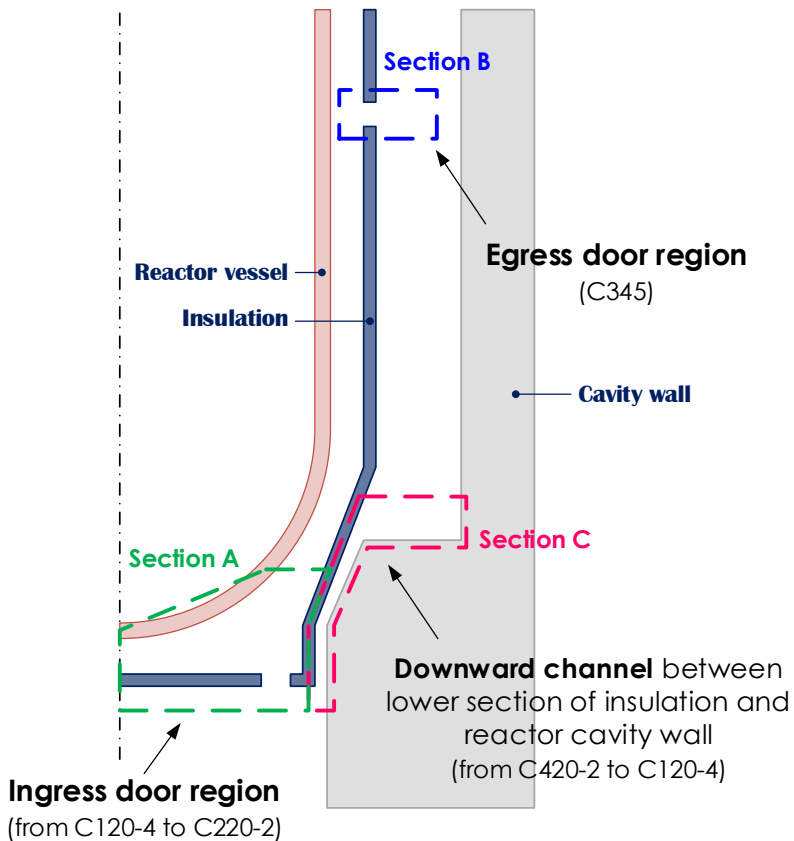


Heat flux profile by relocated core melt

Boundary & initial conditions

Parameters	Value
Containment Pressure	2.5 bar
Total heat load	23.3 MW
Initial water temperature	48.9 °C
Initial water level	Bottom of CL
BAMP makeup rate	170 GPM

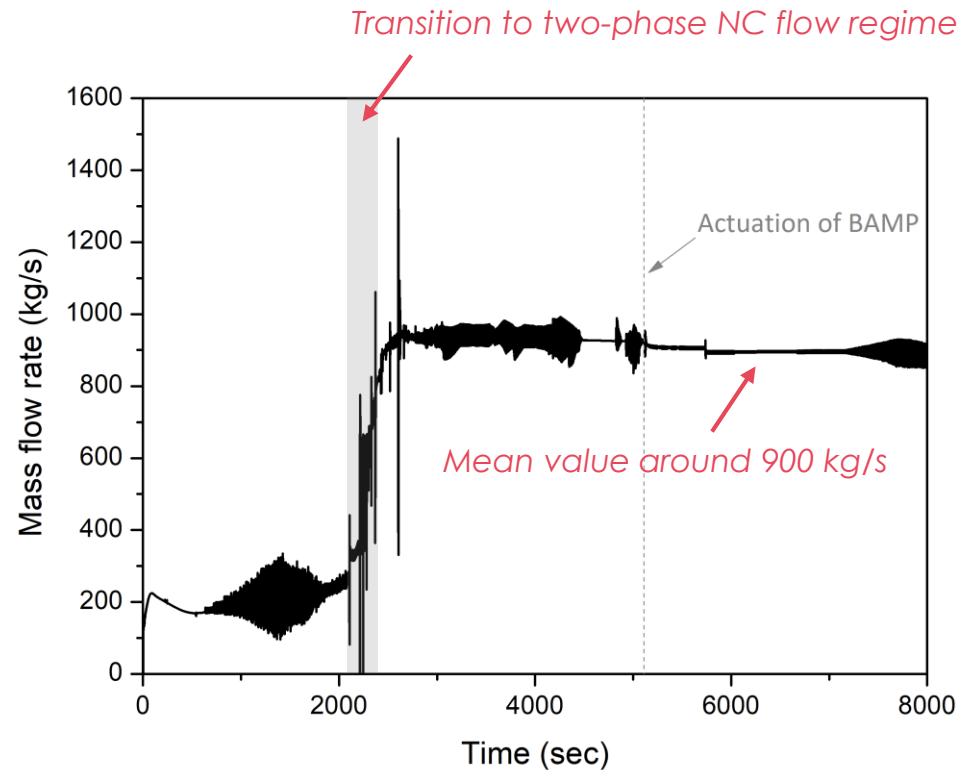
❖ Natural circulation flow rate



Locations of significant minor pressure drops

Loss coefficient at dominant minor loss points

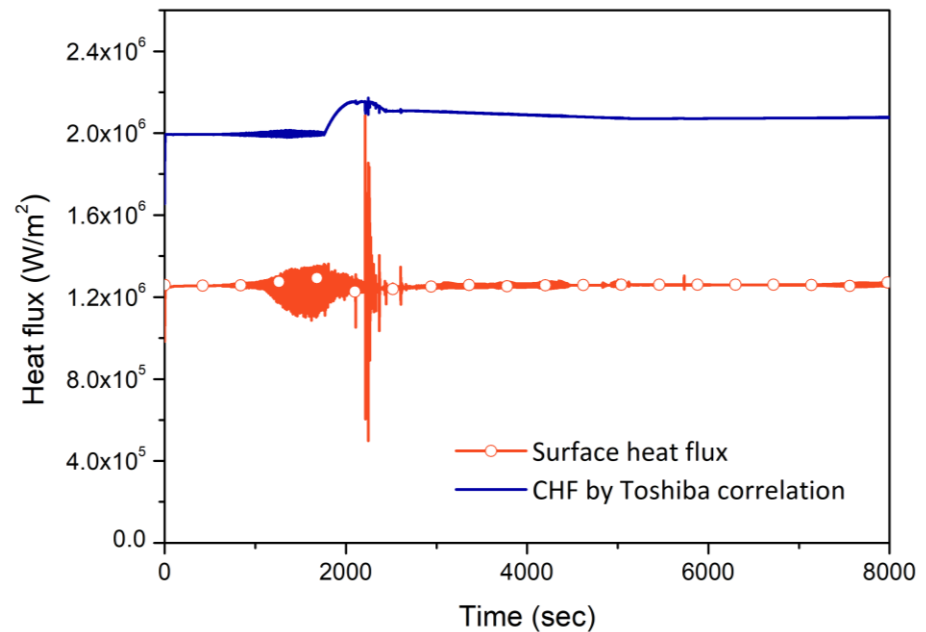
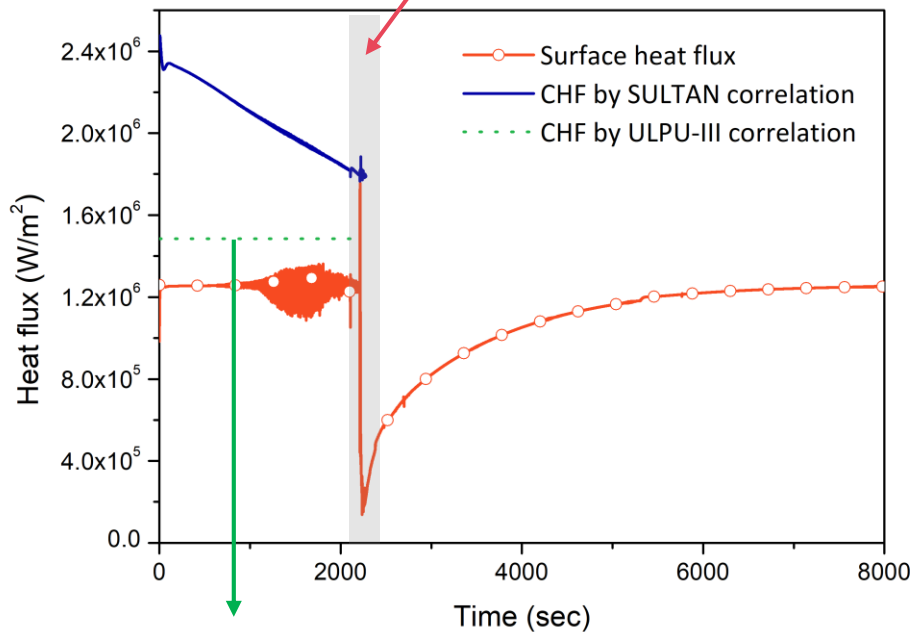
→ estimated based on CFD analysis at the single-phase liquid state before significant void generation



❖ Surface heat flux & CHF per applied correlation

- ULPU-III or SULTAN correlation: boiling regime transition to the **post-DNB** region
- Toshiba's correlation: subcooled nucleate boiling regime sustained

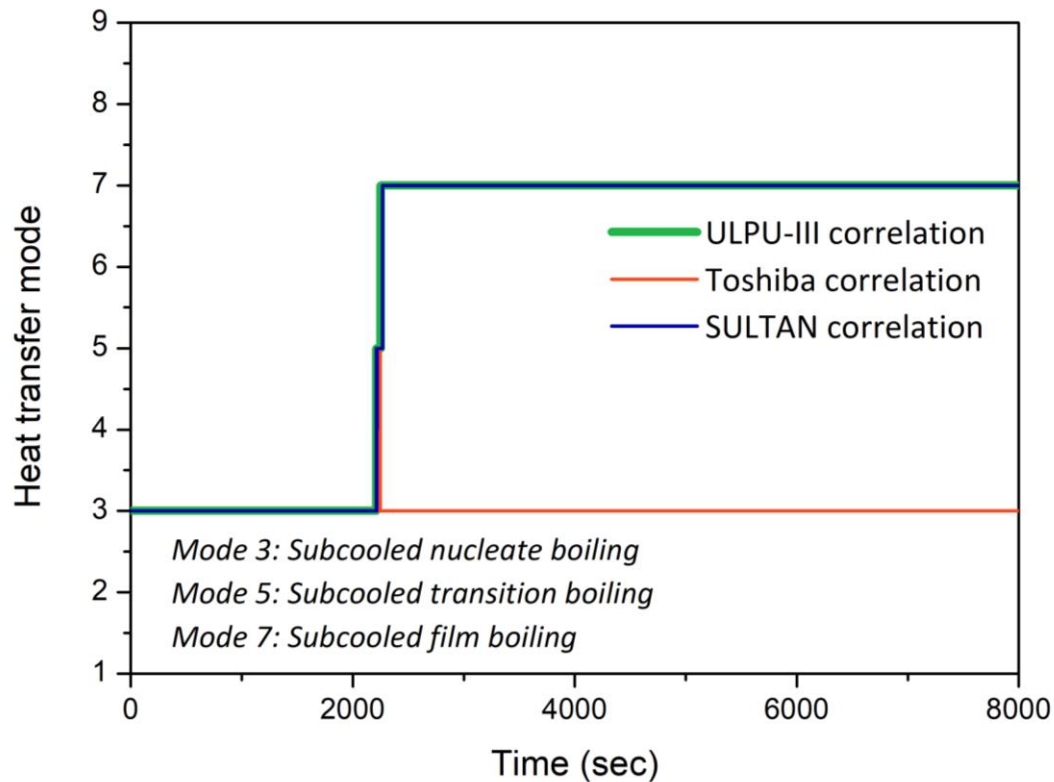
Significant flow oscillations due to transition to two-phase regime



No flow effect considered ← only a function of polar angle

❖ Natural circulation flow rate

Different conclusions about the thermal margin of ERVC relying upon the selected CHF model for downward-facing hemisphere



Concluding Remarks

- ❖ Three CHF correlations for the lower head of the reactor vessel was newly implemented into MARS-KS1.4 code to better predict the thermal margin of ERVC of the APR1400. Predicted boiling regimes were different per the selected correlation.
- ❖ Future works
In-depth review of CHF tests for user recommendations for ERVC simulation
Coupling with the smoothed-particle hydrodynamics code, named SOPHIA⁴⁾, to propose a new analysis method for in-vessel retention

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4) S. H. Park et al, the Korean Nuclear Society Virtual Spring Meeting, July 9-10, 2020

Thank you for your interest!

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