

# **Effects of Ground Motion Input on Responses of Structure and Equipment**

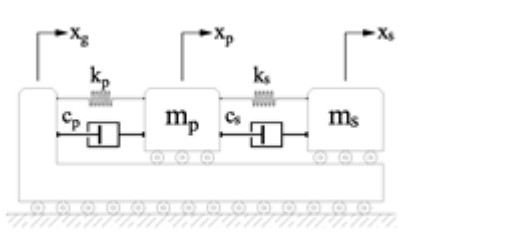
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*Korea Atomic Energy Research Institute*

Korean Nuclear Society Spring Meeting

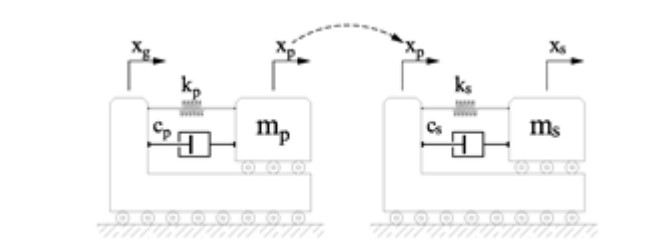
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# Introduction

- Coupled model & uncoupled model



*Coupled model*



*Uncoupled model*

- Decoupling error in ASCE-4 criteria

	Natural Frequency	Response (to earthquake RG 1.60)	
	Structure	Structure	Equipment
Max. Decoupling Error	10 %	26 %	141 %
Graph			

# Harmonic Excitation (1)

- Ground motion input is considered as simple harmonic motion.

$$\ddot{x}_g(t) = e^{i\omega t}$$

- Relative displacements and accelerations of the structure and equipment

$$y_p(t) = H_{y_p}(\omega)e^{i\omega t}, \quad \ddot{x}_p(t) = H_{\ddot{x}_p}(\omega)e^{i\omega t}$$

$$y_s(t) = H_{y_s}(\omega)e^{i\omega t}, \quad \ddot{x}_s(t) = H_{\ddot{x}_s}(\omega)e^{i\omega t}$$

- Transfer functions for the uncoupled model

$$H_{y_p}(\omega) = \frac{-1}{-\omega^2 + 2i\zeta_p\omega_p\omega + \omega_p^2}$$

$$H_{\ddot{x}_p}(\omega) = -(2i\zeta_p\omega_p\omega + \omega_p^2)H_{y_p}(\omega)$$

$$H_{y_s}(\omega) = \frac{-H_{\ddot{x}_p}(\omega)}{-\omega^2 + 2i\zeta_s\omega_s\omega + \omega_s^2}$$

$$H_{\ddot{x}_s}(\omega) = -(2i\zeta_s\omega_s\omega + \omega_s^2)H_{y_s}(\omega)$$

# Harmonic Excitation (2)

- Transfer functions for the coupled model

$$H_{y_p}(\omega) = \frac{\omega^2 - i\omega(1+\mu)2\zeta_s\omega_s - (1+\mu)\omega_s^2}{\Delta}$$

$$H_{y_s}(\omega) = \frac{-i\omega 2\zeta_p\omega_p - \omega_p^2}{\Delta}$$

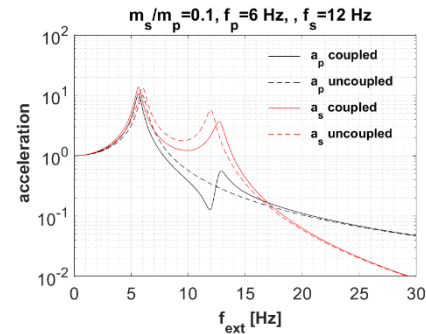
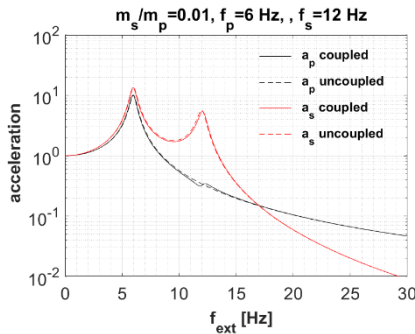
$$H_{\ddot{x}_p}(\omega) = \frac{-i\omega^3 2\zeta_p\omega_p - \omega^2(\omega_p^2 + 4\zeta_p\zeta_s\omega_p\omega_s) + i\omega(2\zeta_p\omega_p\omega_s^2 + 2\zeta_s\omega_s\omega_p^2) + \omega_p^2\omega_s^2}{\Delta}$$

$$H_{\ddot{x}_s}(\omega) = \frac{-\omega^2 4\zeta_p\zeta_s\omega_p\omega_s + i\omega(2\zeta_p\omega_p\omega_s^2 + 2\zeta_s\omega_s\omega_p^2) + \omega_p^2\omega_s^2}{\Delta}$$

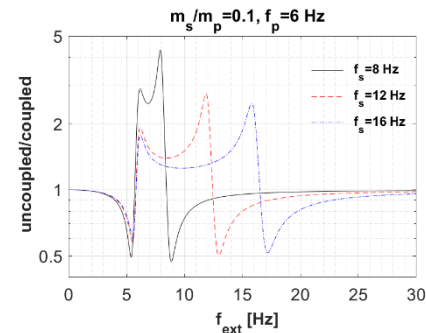
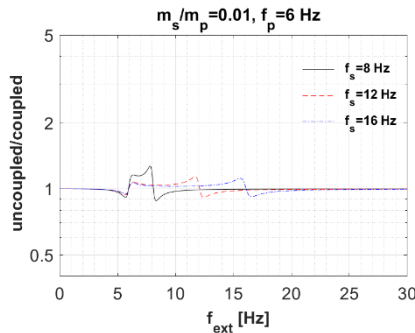
$$\Delta = \omega^4 - i\omega^3 [2\zeta_p\omega_p + 2(1+\mu)\zeta_s\omega_s] - \omega^2 [\omega_p^2 + (1+\mu)\omega_s^2 + 4\zeta_p\zeta_s\omega_p\omega_s] + i\omega [2\zeta_p\omega_p\omega_s^2 + 2\zeta_s\omega_s\omega_p^2] + \omega_p^2\omega_s^2$$

# Response to Harmonic Excitation

- Response and decoupling error depends on excitation frequency, mass ratio, and frequency ratio.
- Response acceleration has peaks due to resonance.



- Decoupling error due to resonance.



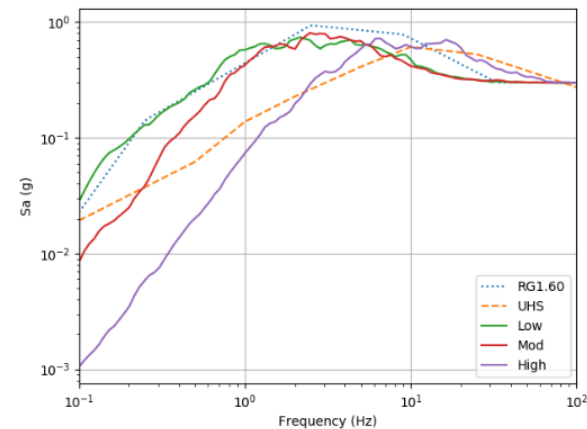
	$m_s/m_p = 0.01$		
	$f_s/f_p = 1.33$	$f_s/f_p = 2.0$	$f_s/f_p = 2.67$
Peak Error	27%	14%	12%

	$m_s/m_p = 0.1$		
	$f_s/f_p = 1.33$	$f_s/f_p = 2.0$	$f_s/f_p = 2.67$
Peak Error	331%	173%	146%

# Seismic Input with Different A/V Ratios

- Peak ground acceleration to velocity (A/V) ratios
  - High A/V group has more 5~40 Hz components than other group.

Group	A/V (g/m/s)
Low	< 0.8
Moderate	0.8 ~ 1.2
High	> 1.2



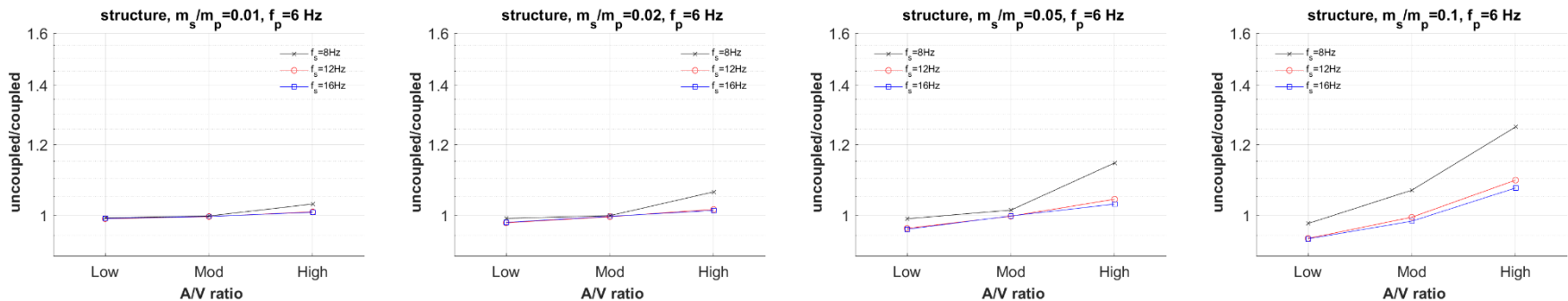
Acceleration spectrum with different A/V ratio

## • Method

A/V ratio	Low, Moderate, High
Model	Coupled, Uncoupled
Damping ratio	5% for structure 3% for equipment
Mass ratio	0.01, 0.02, 0.05, 0.1
Frequency ratio	1.33, 2.0, 2.67

# Response to Input with Different A/V Ratios (1)

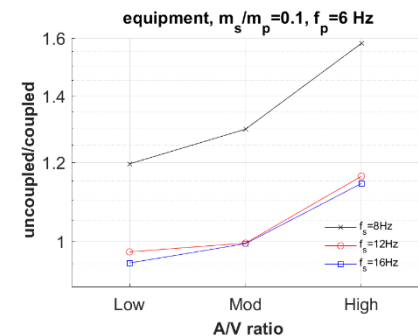
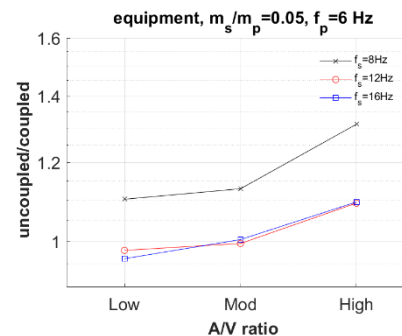
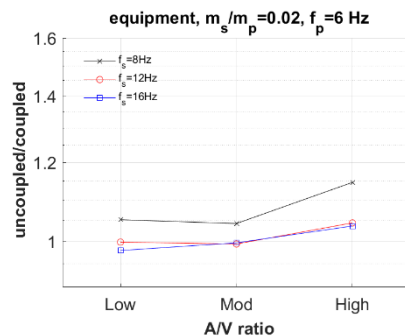
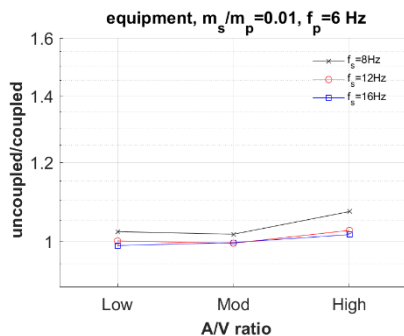
- Decoupling error - structure
  - The response error increases as the A/V ratio changes from “Low” to “High”.
  - The A/V ratio is dominant in the response error when the mass ratio increases.
  - Max. decoupling error is 26% due to resonance. ( $f_p=6$  Hz,  $f_s=8$  Hz, High A/V input=5~40 Hz)
  - The high-frequency earthquakes increase the response error of the uncoupled model.



*Response error of the uncoupled model structure*

# Response to Input with Different A/V Ratios (2)

- Decoupling error - equipment
  - Decoupling error of equipment is larger than that of structure.
  - Max. decoupling error is 58% due to resonance. ( $f_p=6$  Hz,  $f_s=8$  Hz, High A/V input=5~40 Hz)



Response error of the uncoupled model equipment