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# Natural convection heat transfer of two heating spheres with pitch-to-diameter ratio

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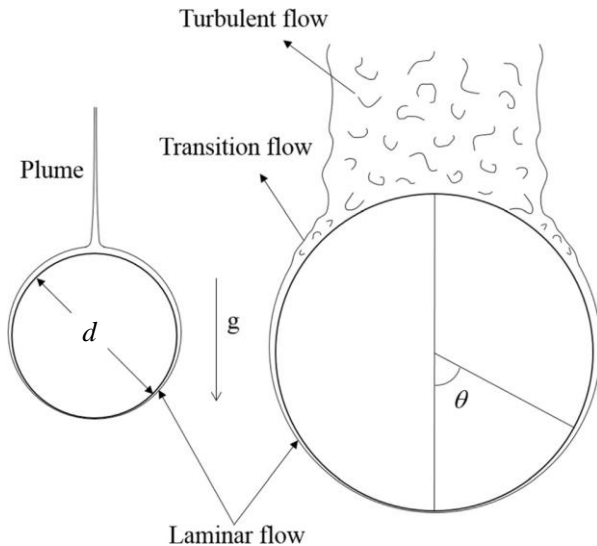
# Introduction

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- **Applications of packed bed**
  - Pebble fuel of nuclear reactors, thermal energy storage, catalytic reactors, heat exchanger, etc.
- **The investigation on the interaction between adjacent spheres in the packed bed for natural convective flow is needed.**
- **In this study,**
  - Measurement of natural convection heat transfer of two heating spheres with different arrangement.
  - Visualization experiment of plating patterns appearing on two spheres.



# Natural convection of a single heating sphere



Natural convection on a sphere  
[Lee et al., 2017]

- **Natural convection of a single heating sphere**
  - The buoyant flow starts at the bottom along the surface of the sphere.
  - It separates the plume from the upper part of the sphere.
- **For small  $Ra_d$** 
  - For low  $Ra_d$ , the laminar boundary layer is formed.
  - The plume rises from the uppermost part
- **For large  $Ra_d$** 
  - For high  $Ra_d$ , the transition to turbulence occurs.
  - The plume rises from at the upper part of the sphere which is relatively lower.
  - Critical  $Ra_d = 3 \times 10^8$

# Experimental Methodology

- Analogy between heat transfer and mass transfer

[ Governing equations ]

Heat transfer	Mass transfer
$\frac{\partial u}{\partial x} + \frac{\partial u}{\partial y} = 0$	
$\rho \frac{Du}{Dt} = -\frac{\partial P}{\partial x} + \mu \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right) + X$	
$\frac{DT}{Dt} = \alpha \nabla^2 T$	$\frac{DC}{Dt} = D \nabla^2 C$

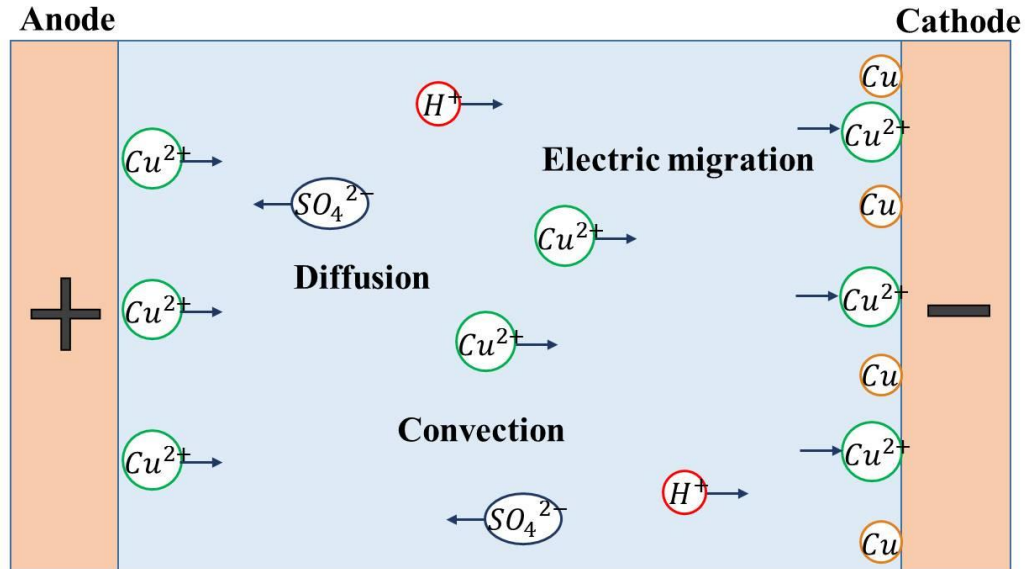
[ Dimensionless numbers ]

Heat transfer		Mass transfer	
$Nu$	$\frac{hd}{k}$	$Sh$	$\frac{h_m d}{D_m}$
$Pr$	$\frac{\nu}{\alpha}$	$Sc$	$\frac{\nu}{D_m}$
$Ra$	$\frac{g \beta \Delta T d^3}{\alpha \nu}$	$Ra$	$\frac{g d^3 \Delta \rho}{D_m \nu \rho}$



# Copper electroplating system

- Mass transfer in a cupric acid-copper sulfate



$$h_m = \frac{(1-t_n)I_{lim}}{nF(C_b - C_s)}$$

1. Electric migration ( $N_m$ )  $\rightarrow$  not in heat transfer system ( $H_2SO_4$ )

2. Diffusion ( $N_d$ )

3. Convection ( $N_c$ )  $\rightarrow N_t - N_m = N_d + N_c = \frac{(1-t_n)I_{lim}}{nF} = h_m(C_b - C_s)$

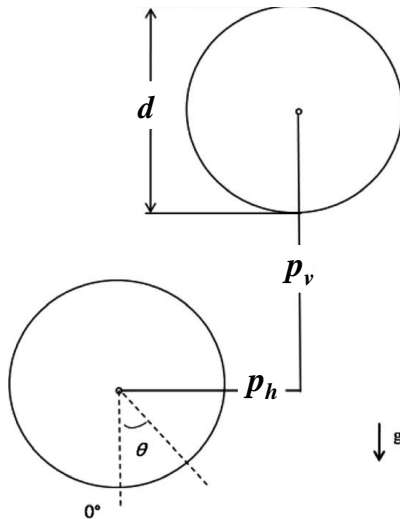
# Test matrix

Test matrix

$Sc$	$d$ (mm)	$Ra_d$	Position	
			$P_h/d$	$P_v/d$
2,014	6,	$1.83 \times 10^7$ ,	0	1.06, 1.5, 2, 3, 5, 7
			0.47	1.06, 1.5, 2, 3, 5, 7
	15.8,	$3.35 \times 10^8$ ,	0.76	1.06, 1.5, 2
			1.06	1.06, 1.5, 2
25	$1.33 \times 10^9$			

$P_h/d$  : Horizontal pitch-to-diameter

$P_v/d$  : Vertical pitch-to-diameter

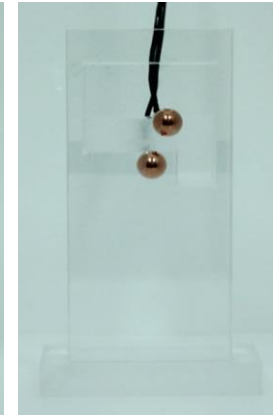


Arrangement of two spheres

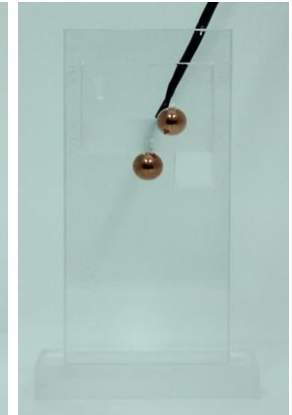
Varying  $P_h/d$



$P_h/d = 0$



$P_h/d = 0.47$



$P_h/d = 0.76$

Varying  $P_v/d$



$P_v/d = 1.06$

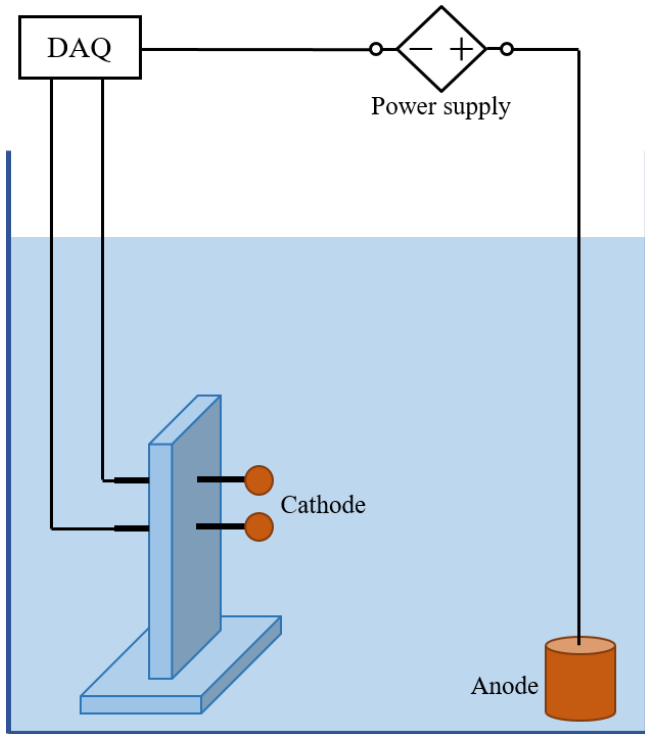


$P_v/d = 1.5$



$P_v/d = 3$

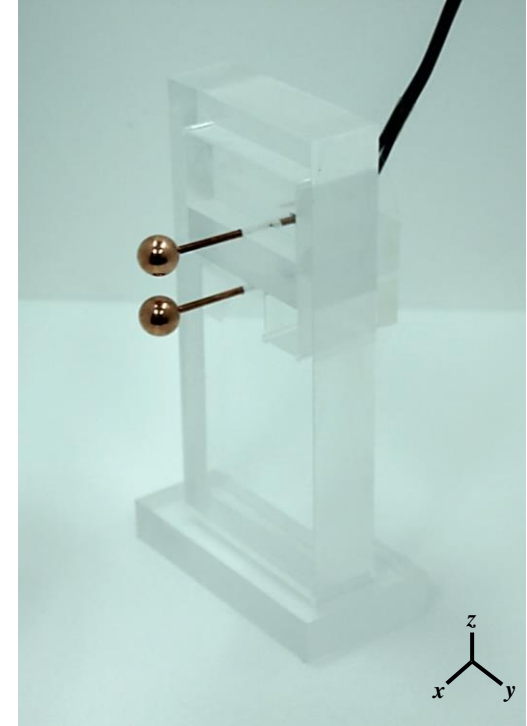
# Experimental setup



**Schematic electric circuit**

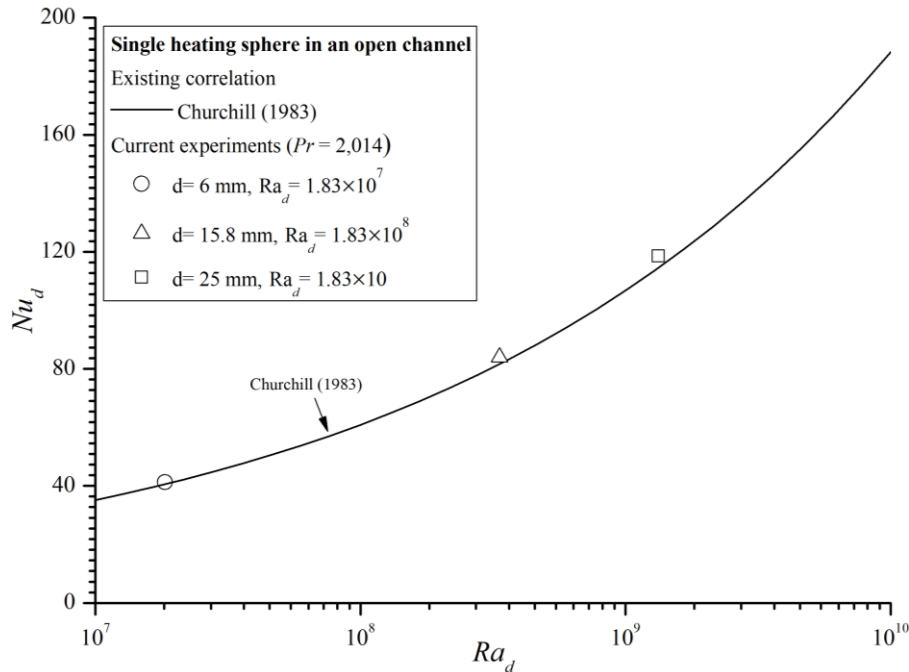


**Front view**



**Side view**

# Results : Single sphere



Churchill (1983)	
Correlation	Range
$Nu_d = 2 + \frac{0.589 Ra_d^{0.25}}{[1 + (0.469 / Pr)^{9/16}]^{4/9}}$	$Ra_d < 10^{11}$

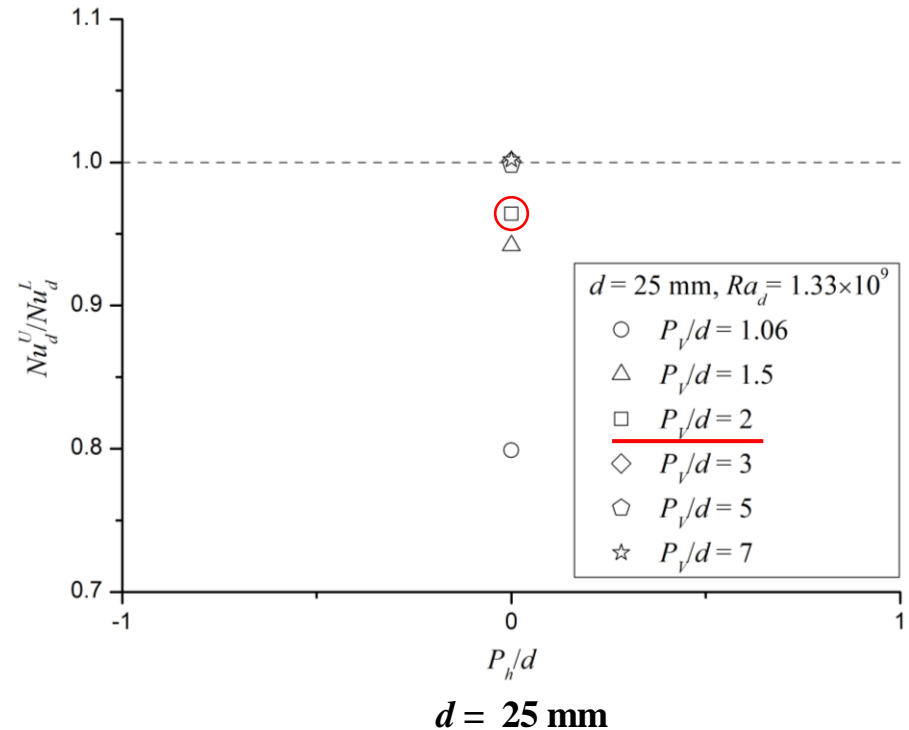
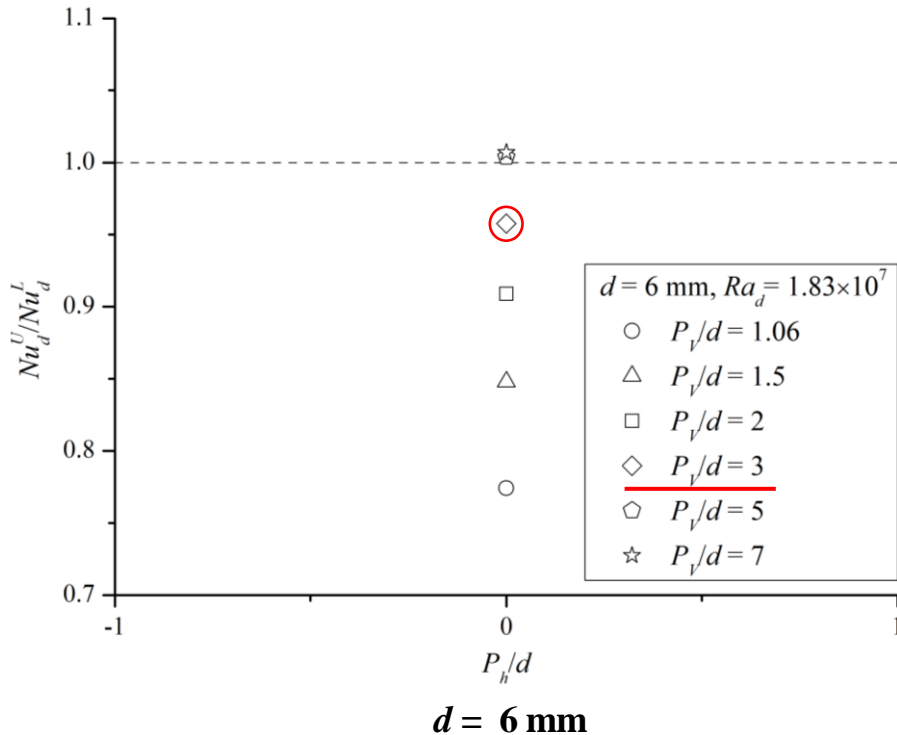
## Comparison of experimental results with existing correlation

- The experimental results were compared with correlation of Churchill (1983).
  - Average error = 2.7 %



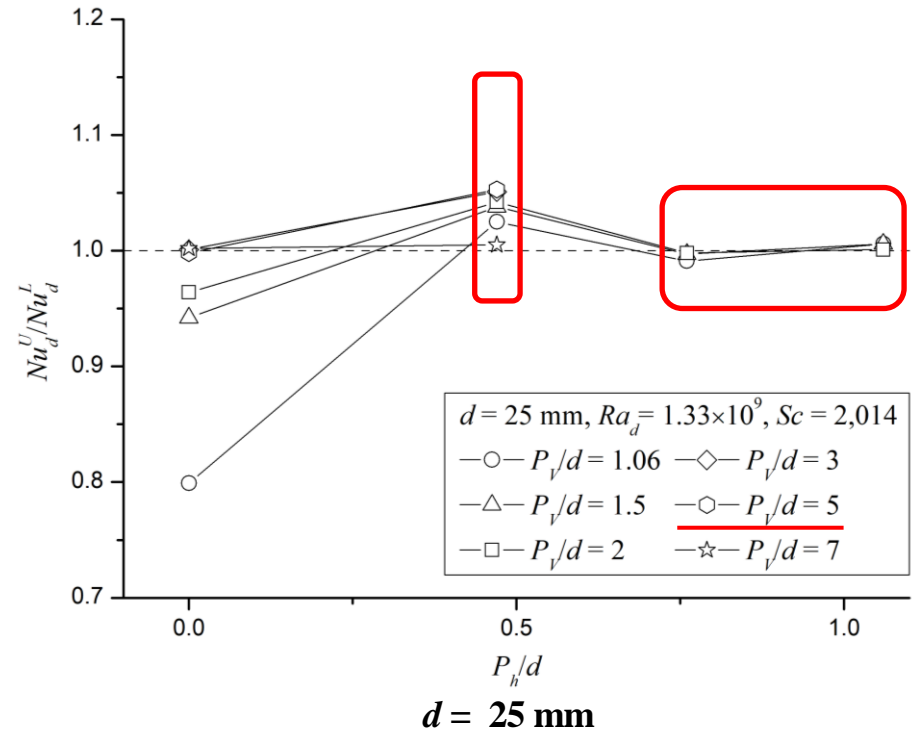
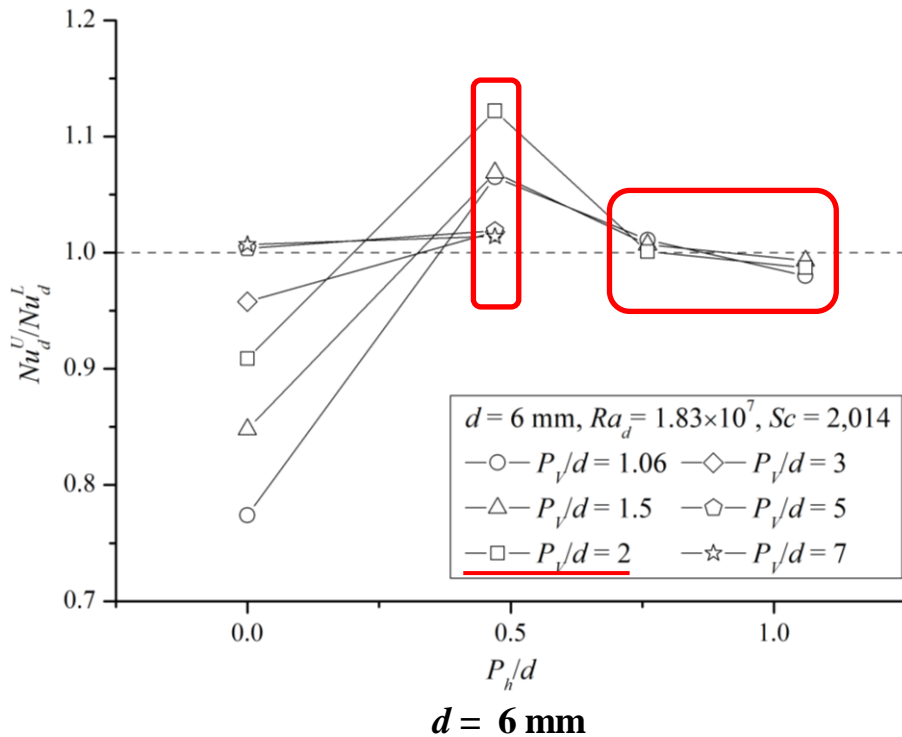


# Results : Two inline spheres



- The heat transfer of the upper sphere was declined by the decrease of the  $P_v/d$ .
  - This is due to **preheating effect** and **stagnant flow effect**.
  - Up to  $P_v/d = 3$  (6 mm, 15.8 mm), up to 2 (25 mm).

# Results : Two staggered spheres



- For  $P_h/d = 0.47$ , the heat transfer of the upper sphere is higher than the lower sphere
  - This is due to **side flow effect**.
  - Up to  $P_v/d = 2$  (6 mm), up to  $P_v/d = 3$  (15.8 mm), up to  $P_v/d = 5$  (25 mm).

# Results : Plating patterns appearing on lower sphere

$$Ra_d = 1.33 \times 10^9$$



**Lower sphere**

$$Ra_d = 1.35 \times 10^9$$

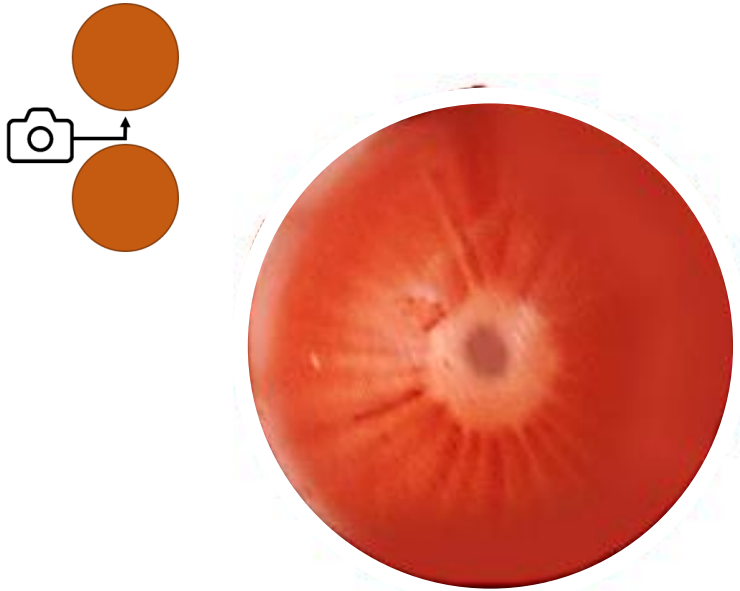


**Single sphere**  
[Lee et al., 2017]

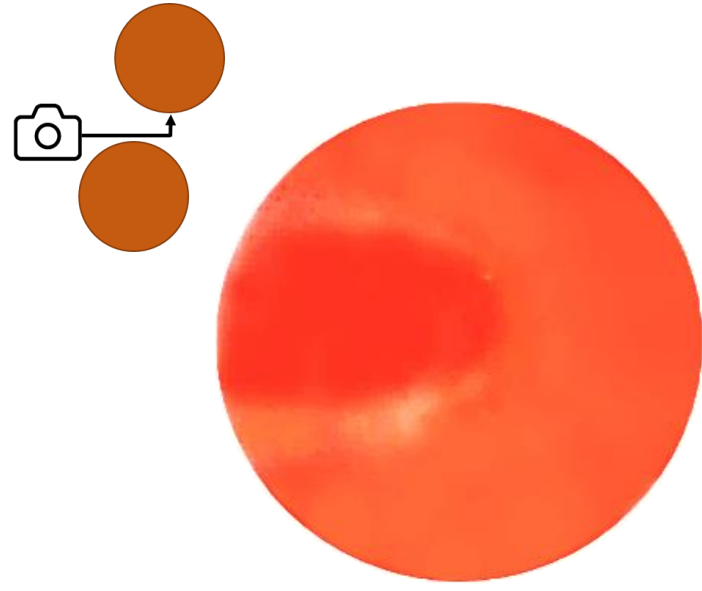
- The plating patterns of the lower sphere was the same as that of a single sphere.

# Results : Plating patterns appearing on upper sphere

$P_v/d = 1.06$ , upper sphere ( $Ra_d = 1.33 \times 10^9$ )



$P_h/d = 0$



$P_h/d = 0.47$

- At  $P_h/d = 0$ , the upper sphere was influenced by **stagnant flow**.
- At  $P_h/d = 0.47$ , the upper sphere was affected by **side flow**.

# Conclusions and further studies

## Conclusion

- **Natural convection heat transfer of two spheres with various pitch-to-diameter was performed using mass transfer experiment.**
  - **Two inline spheres**
    - ✓ When  $P_v/d$  is small, the heat transfer of the upper sphere was declined due to **preheating effect** and **stagnant flow effect**.
  - **Two staggered spheres**
    - ✓ As  $P_h/d$  increases, **side flow effect** occurred and heat transfer of the upper sphere increased.

## Further studies

- **Experiments for extended test matrix**
  - Sphere diameter corresponding to turbulent flow regime ( $Ra_d > 1.83 \times 10^9$ )
- **Analysis of the geometrical effect for the influence of pitch-to-diameter on natural convection heat transfer**
  - 2D (Two cylinders) vs. 3D (Two spheres)



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**Thank you for attention.**

