Toward the Robust and Resilient Nuclear System for the Highly Improbable Event

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#### Analysis of Pressurizer Surge Line Flow Effect on TMI-2 Severe Accident Progression

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### Introduction



#### □ TMI-2 원전 중대사고 개요

|          | TMI-2                        |
|----------|------------------------------|
| 원전 소재    | 미국 펜실바니아                     |
| 노형       | 가압경수로( <mark>PWR</mark> )    |
| 설계자      | Babcock & Wilcox             |
| 출력       | 906 MWe                      |
| 상업운전 개시일 | 1978.12.30                   |
| 사고발생일    | 1979.03.28                   |
| 사고원인     | 설비 결함과 인적 실수                 |
| 사망자 및 영향 | 없음                           |
| 사고 특이사항  | 노심용융,<br>원자로용기 및 격납건물 건전성 유지 |

### TMI-2 Plant



### Plant Data of TMI-2

| Reactor                           | Data      | Core & Fuel<br>Assemblies | Number |
|-----------------------------------|-----------|---------------------------|--------|
| Design Heat Output                | 2,272 MWt | Fuel Assemblies           | 177    |
| Vessel Coolant Inlet Temperature  | 292 °C    | Fuel Rods per Fuel        | 208    |
| Vessel Coolant Outlet Temperature | 320 °C    | Assemblies                | 200    |
| Core Coolant Outlet Temperature   | 321 °C    |                           |        |
| Average Core Fuel Temperature     | 649 °C    | Tubes per Assembly        | 16     |
| Core Operating Pressure           | 15 MPa    |                           |        |

#### **Detailed TMI-2 Main Events**

| Time (s) | Main Events   |  |
|----------|---|--|
| 0        | Turbine and main feedwater pump trip (Total Loss of Feed Water) |  |
| 3        | Pressurizer PORV opening (15.5 MPa)                             |  |
| 8        | Reactor scram on high pressure signal                           |  |
| 13       | No Pressurizer PORV closing (15.2 MPa) (SBLOCA)                 |  |
| 41       | Operation of 1 (of 3) makeup pump 1B                            |  |
| 122      | HPI operation   |  |
| 278      | Stop of HPI   |  |
| 480      | Auxiliary feedwater startup                                     |  |
| 552      | Core boiling begins   |  |
| 4,440    | Shutdown B-loop RCP (end of phase 1)                            |  |
| 6,000    | Shutdown A-loop RCP   |  |
| 6,184    | Core uncovery   |  |
| 7,742    | Cladding oxidation begins (T= 1,000K)                           |  |
| 7,719    | Cladding failure (T=1,117K)                                     |  |
| 8,340    | Close of the PORV line block valve                              |  |
| 9,014    | Fuel melting  |  |
| 10,440   | Restart one B-loop RCP (end of phase 2)                         |  |
| 11,580   | Shutdown of the B-loop RCP                                      |  |
| 12,000   | Start of primary system feed and bleed                          |  |
| 13,440   | Core material slumping (end of phase 3)                         |  |
| 18,000   | General emergency declared (end of phase 4)                     |  |

#### End State in TMI-2





#### TMI-2 사고의 최종 모습

### **Research Needs & Objective**

- The surge In the TMI-2 severe accident, the break location was the PORV (Pilot Oprated Relief Valve), which was located top of the pressurizer.
- A flow path through the the surge line between the hot leg and the pressurizaer was generated and the water level of pressurizer was very high, which resulted in the melt progression in the core.
- The surge line modeling effect on the core melt progression in the TMI-2 severe accident was analyzed using the CINEMA computer code.

## **CINEMA Development in Korea**

 An integrated severe accident analysis computer code (CINEMA) has been developed by the collaboration in Korea.



CINEMA: Code for INtegrated severe accidEnt Management Analysis

#### **CINEMA Nodalization for TMI-2**

- Using TMI-2 Design Data
- Based on SCDAP/RELAP5 Input



**CINEMA-CSPACE** Nodalization

### **Steady State Results**

| Parameter                      | Plant Operating<br>Condition | CINEMA<br>Results |
|--------------------------------|------------------------------|-------------------|
| Reactor Power (MW)             | 2700.0                       | 2700              |
| Primary System Pressure (MPa)  | 15.2                         | 15.3              |
| Cold Leg Temperature 1A (K)    | 561.0                        | 571.0             |
| Cold Leg Temperature 2A (K)    | 548.0                        | 571.0             |
| Hot Leg Temperature Loop A (K) | 592.0                        | 598.0             |
| Hot Leg Temperature Loop B (K) | 592.0                        | 598.0             |
| Feedwater Temperature (K)      | 513.0                        | 513.0             |
| SG A Pressure (MPa)            | 7.31                         | 5.85              |
| SG B Pressure (MPa)            | 7.24                         | 5.85              |
| SG A Steam Temperature (K)     | 586.0                        | 578.0             |
| SG B Steam Temperature (K)     | 585.0                        | 579.0             |



## **Pressurizer Water Level**



#### PORV의 Critical Flow 모델(New HF 모델)



#### Measured Data and SCDAP/RELAP5 Results

#### **CINEMA Results**

#### **Pressurizer Pressure**





#### **Fuel Cladding Temperature**



**CINEMA Results on No CCFL** 

CINEMA Results on Strong CCFL in Pressurizer Surge Line

#### Conclusions

- The surge line flow modeling effect on the core melt progression in the TMI-2 severe accident was analyzed using the CINEMA.
- The CCFL input parameters in CINEMA affect the pressurizer water drain to the core through the pressurizer surge line.
- The CINEMA results on strong CCFL model are very similar to the TMI-2 data in general.
- More CINEMA analysis for a melted fuel relocation and quenching process in the core and lower plenum are necessary to simulate the late phase of the TMI-2 severe accident.

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# **Thank You!**

