

Evaluation of the Effect of Uncertainty Expression Method on Material Balance Evaluation for Nuclear Safeguards

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Introduction

- The KINAC has been developing an independent material balance evaluation (MBE) program for national safeguards inspection^[1]
- However, the IAEA's uncertainty expression method for MBE has limitations
- Benchmark MBEs were performed using three different uncertainty expression methods and optimized method was identified

Research Overview

Identifying the measurement system of the facility

Calculating the MUF using general ledger and the LI

Calculate the MUF uncertainty (σ_{MUF}) using different uncertainty expression methods and evaluate the σ_{MUF}

Conventional IAEA's method

Modified IAEA's method

ISO standard method (GUM)

$H_0: MUF = 0$, if $|MUF| \leq t_{\alpha} \sigma_{MUF}$ → Measurement uncertainty (Normal)
 $H_1: MUF \neq 0$, if $|MUF| > t_{\alpha} \sigma_{MUF}$ → Another sources (Abnormal)

Identifying the optimized uncertainty expression method

Material Unaccounted for (MUF): Difference between the book and measured inventory
List of Inventory Items (LI): List of all items in the facility and its measured information

Benchmark Facility Configuration

- The benchmark facility is a fuel fabrication process with 2 plants and 12 key measurement points (KMPs)
 - The facility consists of reconversion, pelletizing, rod insertion and assembling process
 - The facility contains 14,538 items in 15 strata

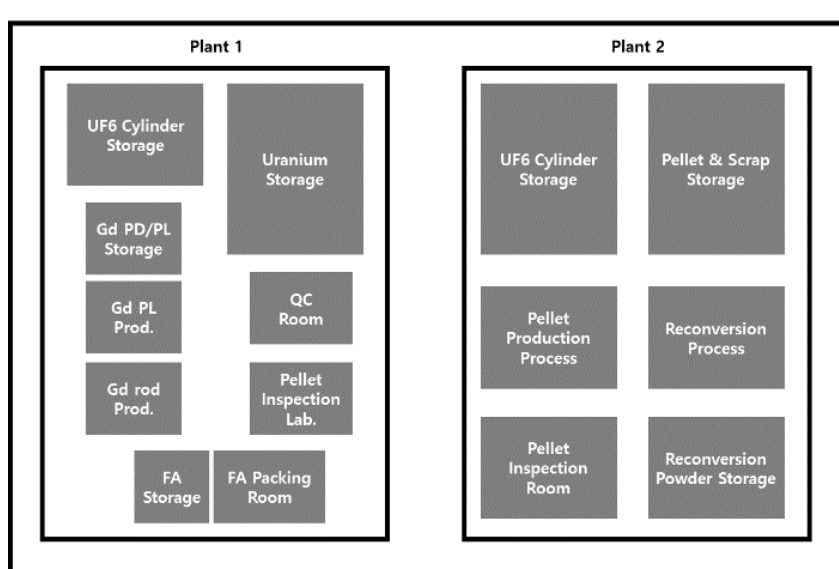


Fig. 1. Facility Configuration

Table 1. KMPs and its description

KMP	Description	Method		
		Weight	U %	wt %
KMP 1	UF ₆	-	-	-
KMP 2	Reconversion process	-	-	-
KMP 3	UO ₂ powder	TGA	TIMS	-
KMP 4	UO ₂ green pellet/scrap	-	-	-
KMP 5	UO ₂ pellet/scrap	TGA	TIMS	-
KMP 6	Uranium nitrate	-	-	-
KMP 7	Fuel rod	-	-	-
KMP 8	Fuel assembly	-	-	-
KMP 9	Scrap (clean/dirty)	TITR	TIMS	-
KMP 10	Solid waste	-	-	-
KMP 11	Liquid waste	-	-	-
KMP 12	Laboratory sample	TITR	TIMS	-

Table 2. Strata information and measurement system

Stratum	Description	Location	Q	P	T(E)	T(I)
FF-11	Fuel Assembly	FA storage	1	0	0	0
FF-BD	Fuel Assembly (Gd)	FA storage	1	0	0	0
FR-11	Fuel Rod	QC Room	2	0	0	0
FR-11	U storage	U storage	3	0	0	0
FR-1G	Fuel rod with Gd	QC Room	2	0	0	0
FR-1G	U storage	U storage	3	0	0	0
HE-1L	UF ₆ Heel	UF ₆ Cylinder Storage - P1	4	0	0	0
UF-1L	UF ₆ Cylinder	UF ₆ Cylinder Storage - P1	4	0	0	0
PD-1L	UO ₂ Powder	Gd pellet/powder Storage	6	1	1	1
PD-1L	UO ₂ Powder	(Re)conversion Process	7	1	1	1
PD-1L	UO ₂ Powder	Recon Powder Storage	7	1	1	1
PL-1L	UO ₂ Pellet(Sintered, pure)	Gd Rod Production Process	9	0	0	0
PL-1L	UO ₂ Pellet(Sintered, pure)	U storage	3	1	1	2
PL-2L	UO ₂ Pellet(Sintered) (Gd)	Gd pellet/powder Storage	6	2	2	2
PL-2L	UO ₂ Pellet(Sintered) (Gd)	U storage	3	2	2	2
SA-1L	Lab. Sample	QC Room	2	0	0	0
SA-1L	Lab. Sample	Pellet Inspection Lab. - P1	12	0	3	0
SA-1L	Lab. Sample	U storage	15	0	3	0
SA-1L	Lab. Sample	Pellet Inspection Lab. - P2	12	0	3	0
SA-1	Lab. Sample(Fuel rod)	QC Room	2	0	0	0
PM-1L	(Re)conversion Products	U storage	3	0	0	0
PM-1L	(Re)conversion Products	(Re)conversion Process	7	0	0	0
SC-1L	Clean Scrap(non-pellet)	Gd Pellet Production Process	12	0	0	0
SC-1L	Clean Scrap(non-pellet)	U storage	3	3	3	3
SC-1L	Clean Scrap(non-pellet)	Pellet & Scrap Storage - P2	7	3	3	3
SC-1L	Clean Scrap(non-pellet)	Pellet Production Process - P2	7	3	3	3
SC-1L	Clean Scrap(non-pellet)	Recon Powder Storage	7	3	3	3
SC-PL	Clean Scrap(Pellet)	Gd pellet/powder Storage	6	3	3	3
SC-PL	Clean Scrap(Pellet)	U storage	3	3	3	3
SC-PL	Clean Scrap(Pellet)	Pellet Production Process - P2	7	3	3	3
SC-PL	Clean Scrap(Pellet)	Pellet & Scrap Storage - P2	7	3	3	3
SD-1L	Dirty Scrap	U storage	3	4	3	4
SD-1L	Dirty Scrap	Recon Powder Storage	7	4	3	4
SD-1L	Liquid Waste	U storage	3	0	0	0

Uncertainty Expression Methods

Methods	Conventional IAEA's method ^[2,3]	Modified IAEA's method ^[2,3]	ISO standard method (GUM) ^[4, 5]
Equation	$V = V_r + V_g + V_s$ $V_r = \sum_{k=1}^K \sum_{l=1}^L \sum_{m=1}^M \frac{\delta_{rkl}^2}{w_{rkl}^2} \left(\frac{\delta_{rkl}^2}{r_{k,m}^2} + \frac{\delta_{rkl}^2}{r_{k,m}^2} + \frac{\delta_{rkl}^2}{c_{rkl}^2} \right)$ $V_g = \sum_{k=1}^K \sum_{l=1}^L \sum_{m=1}^M \frac{\delta_{gkl}^2}{w_{gkl}^2} M_{gkl}^2 + \sum_{k=1}^K \sum_{l=1}^L \sum_{m=1}^M \frac{\delta_{gkl}^2}{w_{gkl}^2} M_{gkl}^2 + \sum_{k=1}^K \sum_{l=1}^L \sum_{m=1}^M \frac{\delta_{gkl}^2}{w_{gkl}^2} M_{gkl}^2$ $V_s = \sum_{k=1}^K \sum_{l=1}^L \sum_{m=1}^M \frac{\delta_{skl}^2}{w_{skl}^2} M_{skl}^2 + \sum_{k=1}^K \sum_{l=1}^L \sum_{m=1}^M \frac{\delta_{skl}^2}{w_{skl}^2} M_{skl}^2 + \sum_{k=1}^K \sum_{l=1}^L \sum_{m=1}^M \frac{\delta_{skl}^2}{w_{skl}^2} M_{skl}^2$ $V_t^* = V_r^* + V_s^*$ $V_t^*(MUF) = \sum_{k=1}^K \sum_{l=1}^L \sum_{m=1}^M \frac{\delta_{t^*kl}^2}{w_{t^*kl}^2} \left(\frac{\delta_{t^*kl}^2}{r_{k,m}^2} + \frac{\delta_{t^*kl}^2}{r_{k,m}^2} + \frac{\delta_{t^*kl}^2}{c_{t^*kl}^2} \right)$ $V_s^*(MUF) = \sum_{k=1}^K \sum_{l=1}^L \sum_{m=1}^M \frac{\delta_{s^*kl}^2}{w_{s^*kl}^2} M_{s^*kl}^2 + \sum_{k=1}^K \sum_{l=1}^L \sum_{m=1}^M \frac{\delta_{s^*kl}^2}{w_{s^*kl}^2} M_{s^*kl}^2 + \sum_{k=1}^K \sum_{l=1}^L \sum_{m=1}^M \frac{\delta_{s^*kl}^2}{w_{s^*kl}^2} M_{s^*kl}^2$ $V^* = V + V_t^*$ $\sigma_{MUF} = \sqrt{V^*}$	$V = V_r + V_g + V_s$ $V_r(MUF) = \sum_{k=1}^K \sum_{l=1}^L \sum_{m=1}^M \frac{\delta_{rkl}^2}{w_{rkl}^2} \left(\frac{\delta_{rkl}^2}{r_{k,m}^2} + \frac{\delta_{rkl}^2}{r_{k,m}^2} + \frac{\delta_{rkl}^2}{c_{rkl}^2} \right)$ $V_g(MUF) = \sum_{k=1}^K \sum_{l=1}^L \sum_{m=1}^M \frac{\delta_{gkl}^2}{w_{gkl}^2} M_{gkl}^2 + \sum_{k=1}^K \sum_{l=1}^L \sum_{m=1}^M \frac{\delta_{gkl}^2}{w_{gkl}^2} M_{gkl}^2 + \sum_{k=1}^K \sum_{l=1}^L \sum_{m=1}^M \frac{\delta_{gkl}^2}{w_{gkl}^2} M_{gkl}^2$ $V_s(MUF) = \sum_{k=1}^K \sum_{l=1}^L \sum_{m=1}^M \frac{\delta_{skl}^2}{w_{skl}^2} M_{skl}^2 + \sum_{k=1}^K \sum_{l=1}^L \sum_{m=1}^M \frac{\delta_{skl}^2}{w_{skl}^2} M_{skl}^2 + \sum_{k=1}^K \sum_{l=1}^L \sum_{m=1}^M \frac{\delta_{skl}^2}{w_{skl}^2} M_{skl}^2$ $\sigma_{MUF} = \sqrt{V}$	$X = \sum_{j(k)=1}^K \left(\sum_{l(jk)=1}^L \left(\sum_{i(jkl)=1}^M Q_{ijlk} \right) \times P_{jk} \times T(E)_{jk} \times T(I)_{jk} \right)$ $u(x_{jk})^2 = \left[\sum_{l(jk)=1}^L \left(\frac{\partial x_{jk}}{\partial Q_{ijlk}} \right)^2 Q_{ijlk}^2 \right] \delta_{ijlk}^2 + \left(\frac{\partial x_{jk}}{\partial P_{jk}} \right)^2 P_{jk}^2 \delta_{P_{jk}}^2 + \left(\frac{\partial x_{jk}}{\partial T(E)_{jk}} \right)^2 T(E)_{jk}^2 \delta_{T(E)_{jk}}^2 + \left(\frac{\partial x_{jk}}{\partial T(I)_{jk}} \right)^2 T(I)_{jk}^2 \delta_{T(I)_{jk}}^2$ $u(x)^2 = \sum_{k=1}^K \sum_{j(k)=1}^L u(x_{jk})^2$ $\sigma_{MUF} = u(X)$

Process	Conventional IAEA's method	Modified IAEA's method	ISO standard method (GUM)
Step 1	Stratification by element	Stratification by element and sub-stratification by isotope	Stratification by measurement system
Step 2	Calculate isotope σ_{MUF} from element analysis	Calculate isotope σ_{MUF} by sub-stratum	Identification of equation to calculate $X(=^{235}U)$ in facility
Step 3	Stratification by isotope	Calculate total σ_{MUF}	Identification of uncertainty sources for measurements in the equation
Step 4	Calculate σ_{MUF} from isotopic measurement		Calculate the σ_{MUF} for each item, stratum and facility
Step 5	Calculate total σ_{MUF}		

Results

Conventional IAEA's method

U235 Weight	Meas. Inventory (kg)	Book Inventory (kg)	MUF (kg)	$\sigma(MUF)$ (kg)	Significance(3 σ)
1101.218	38,572.800	38,548.731	-24.069	43.546	No

Limitations

- Measurement results of the elemental and isotopic analysis is not independent
- Items in the same stratum are not homogeneous
- Inherent limitations from quantifying the systematic error cannot be managed

Modified IAEA's method

U235 Weight	Meas. Inventory (kg)	Book Inventory (kg)	MUF (kg)	$\sigma(MUF)$ (kg)	Significance(3 σ)
1101.218	38,572.800	38,548.731	-24.069	33.7730958	No

Limitations

- Measurement results of the elemental and isotopic analysis is not independent
- Items in the same sub-stratum are not homogeneous
- Inherent limitations from quantifying the systematic error cannot be managed

ISO standard method (GUM)

U235 Weight (KG)	Meas Inventory (kg)	Book Inventory (kg)	MUF (kg)	$\sigma(MUF)$ (kg)	Significance(3 σ)
1101.218	38,572.800	38,548.731	-24.069	13.717	No

Limitations

- The quality of the facilities' measurement system has to be managed with the documented standard processes
- Realistic uncertainty of the GUM method for DA is much bigger than the ITV

Conclusion

- The three uncertainty expression methods (conventional-modified IAEA's method and ISO standard method) have limitations and the limitations of one method is the advantages of the other methods
- The MBE program will adopt ISO standard method since the IAEA's methods limitations cannot be managed

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