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Comparative analysis of CCI-4 test simulation using COCCI and CORQUENCH



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01 Introduction

❖ Motivation

- **Code Of Corium-Concrete Interaction (COCCI)** is being developed by **KAERI** for **Molten Core Concrete Interaction (MCCI)** analysis with C++ focused on wider usability and improved applicability [1].
- The code is also being connected with Code Of Corium Coolability Analysis (COCCA) by **EN2T** which covers ex-vessel corium behaviors such as jet breakup, spreading, and cooling in the cavity.
- Verification of **MCCI** analysis under **the dry cavity condition** is the most significant for **COCCI** in terms of code connection with COCCA.
 - Under the wet cavity condition, simulation using the connected code would be mainly focused on the corium coolability, which is covered by COCCA.

01 Introduction

❖ Objective

- The comparative **MCCI** analysis of **CCI-4 test (dry cavity condition)** was performed using **COCCI** and **CORQUENCH**.

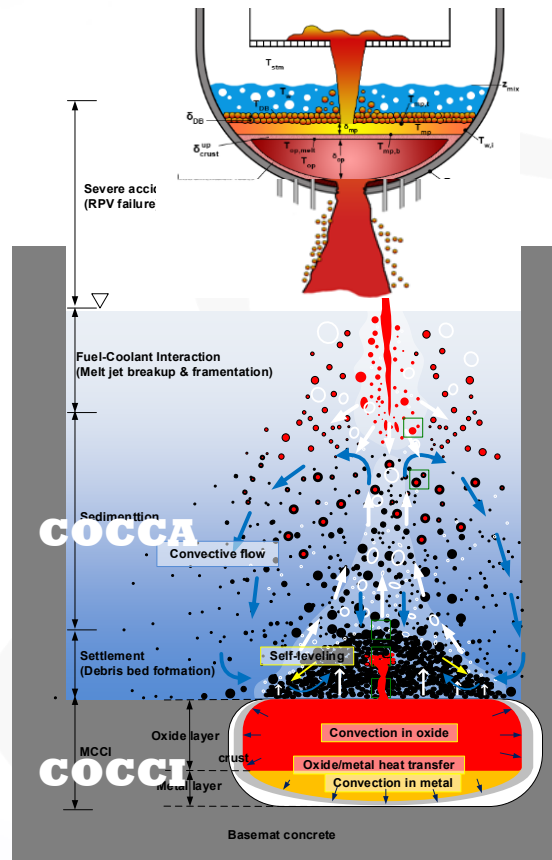


Fig. 1. Schematic of analysis range of COCCI and COCCA

02 Method

❖ MCCI analysis

- There are several codes to simulate **MCCI** such as CORCON, **CORQUENCH**, COSACO, MEDICIS, TOLBIAC-ICB, WECHSL, COCO, MAAP, and so on.
 - All codes can currently analyze the case in which the corium is assumed to be instantaneously spread over the entire floor of the reactor pit under **dry cavity conditions** [2].
- Generally, **the melt/concrete interfacial heat transfer coefficient, the concrete ablation model, and the concrete ablation temperature** are the most important variables for **the dry cavity condition MCCI** analysis.

❖ General characteristics of CORQUENCH

- **CORQUENCH** has been developed based on the MACE and OECD/MCCI experiments by ANL since the early 1990's [3].
- The code is capable of performing either a 1-D or simplified 2-D ablation calculation.
- The melt composition can range from fully metallic to fully oxidic; in all cases, the two phases are assumed to be well mixed (i.e., phase stratification is not modeled).
- In terms of heat transfer at the melt/concrete interface, **CORQUENCH** incorporates a transient concrete ablation/decomposition model based on integral thermal boundary layer theory.
- This model has been upgraded as a part of this work to account for the effects of transient concrete heat-up with simultaneous crust growth following initial melt contact with the concrete.

❖ General characteristics of COCCI

- **COCCI** is being developed to simulate the molten corium and concrete interaction in condition with or without coolant at the top [1].
 - Modeling the physical transient phenomena
 - Various geometry coordinate options
 - Various physical model options.
- By COCCA analysis, the state of the corium which is discharged to the cavity initially can be determined as a liquid or the particle debris.
- The particle debris can be turned into the liquid by the re-melting in the cavity.
- Based on geometry coordinate options, simulations on various experiments and realistic analysis of plant response to **MCCI** in the cavity can be performed.

02 Method

❖ Comparison of CORQUENCH and COCCI

- Same models were used in **CORQUENCH** and **COCCI** for **melt-concrete heat transfer** and **concrete ablation**.

Table 1. Melt-Concrete heat transfer coefficient models and concrete ablation models in CORQUENCH and COCCI

| | CORQUENCH | | COCCI | |
|-----------------------------------|-----------|--|-------|-------------------------------------|
| Melt-concrete heat transfer model | (1) | Kutateladze and Malenkov | (1) | Kutateladze |
| | (2) | CORCON gas film model | (2) | Modified Kutateladze |
| | (3) | CORCON gas film model with a transition to the Bradley model | (3) | Bali |
| | (4) | Sevon heat transfer correlation | (4) | Kutateladze and Malenkov |
| Concrete ablation model | (1) | Quasi-steady concrete decomposition | (1) | Quasi-steady concrete decomposition |
| | (2) | Fully developed | (2) | Fully developed |
| | (3) | Transient concrete dry-out | - | - |

02 Method

❖ Description of CCI-4 test

- CCI tests were performed in ANL by OECD from 2002 to 2010 after the end of MACE tests [5].
- There were total 6 tests, the purpose was obtaining the **MCCI** data such as ablation rate and temperature to build the simulation code.
- 100% oxide corium was used in CCI-1, 2, and 3 tests, however, about 8 w/o metal was included in the corium in **CCI-4 test** to verify the effect of the metal on the concrete ablation and corium coolability.
- From **CCI-4 test**, corium temperature and ablation depth under the dry cavity condition were mainly obtained.
- The facility for the test was used as 2-D notch-geometry with two opposing, ablating walls.

02 Method

❖ CCI-4 test simulation conditions

- Same material properties were used in **CORQUENCH** and **COCCI**.

Table 2. CCI-4 test simulation conditions for CORQUENCH and COCCI

| Variable | Contents |
|---|---|
| Floor size [cm × cm] | 50 × 40 (only two opposing side walls can be ablated) |
| Concrete type | Limestone/common sand |
| Concrete decomposition temperature [K] | 1,500 |
| Concrete decomposition enthalpy [MJ/kg] | 1.84 |
| Weight fraction of H ₂ O gases in concrete | 0.0706 |
| Weight fraction of CO ₂ gases in concrete | 0.2402 |
| Initial total corium mass [kg] | 299.67 [UO ₂ : Zr : ZrO ₂ : Fe : SiO ₂ : Cr : CaO : Al ₂ O ₃ : MgO = 0.565 : 0.046 : 0.215 : 0.030 : 0.041 : 0.047 : 0.037 : 0.005 : 0.14] |
| Initial melt temperature [K] | 2,250 |
| System pressure [bar] | 1.0 |
| Power [kW] | 95 |
| Simulation time [s] | 20,000 |
| Water injection time [s] | (no water injection) |

03 Result

❖ Comparison of ablation depth and temperature

- Both **CORQUENCH** and **COCCI** predicts **ablation depth** larger than experiment.
 - If **transient concrete dry-out model** is used, the depth will be decreased.
- **COCCI** predicts **ablation depth** larger than **CORQUENCH** because predicted **bulk melt temperature** is higher.

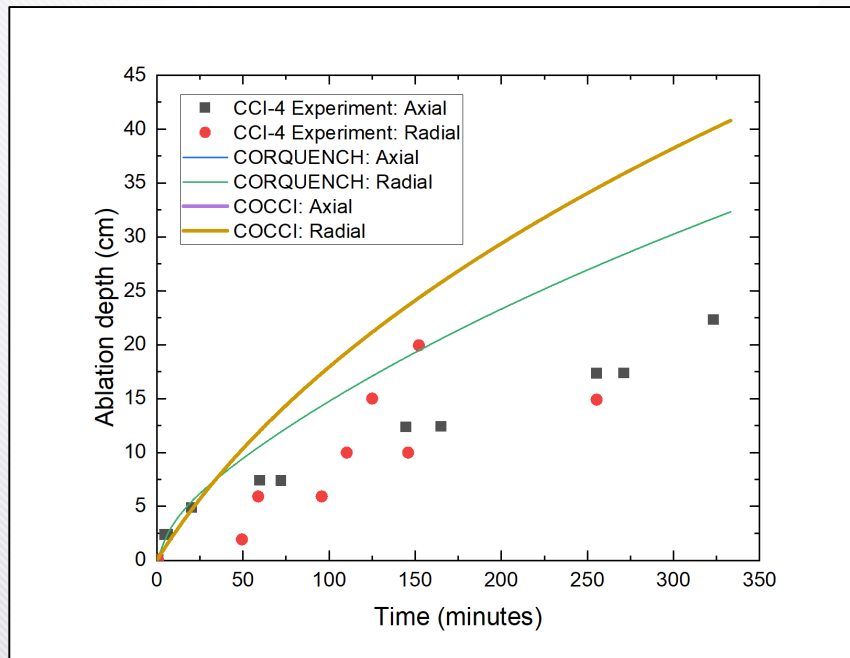


Fig. 2. Comparison of ablation depth

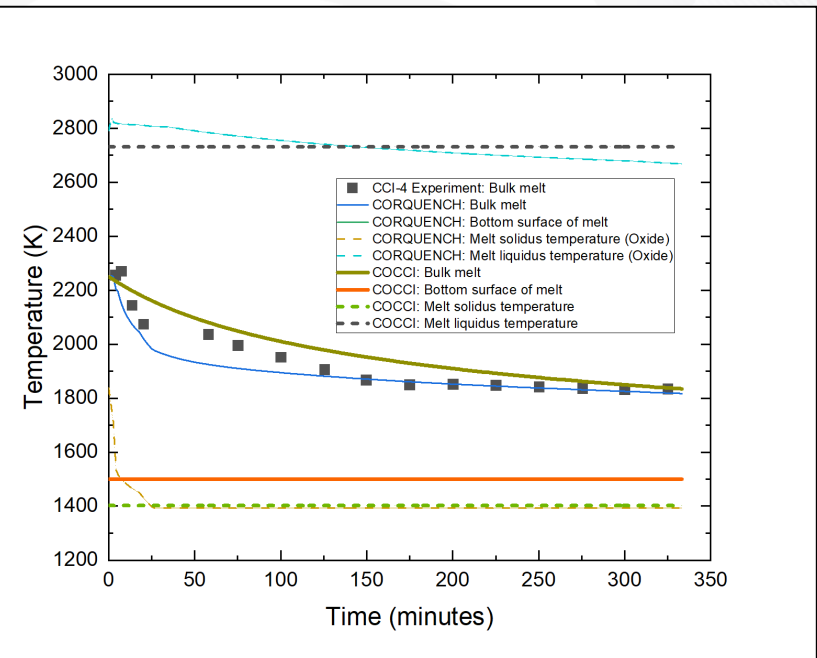


Fig. 3. Comparison of temperature

03 Result

❖ Comparison of heat flux and heat transfer coefficient

- Because **bulk melt temperature** is higher in COCCI, **heat fluxes** are also higher.
- **Heat transfer coefficient** is almost similar because same model was used.
- The difference of **heat transfer coefficient** in early phase comes from the difference of **corium material properties** such as heat capacity.

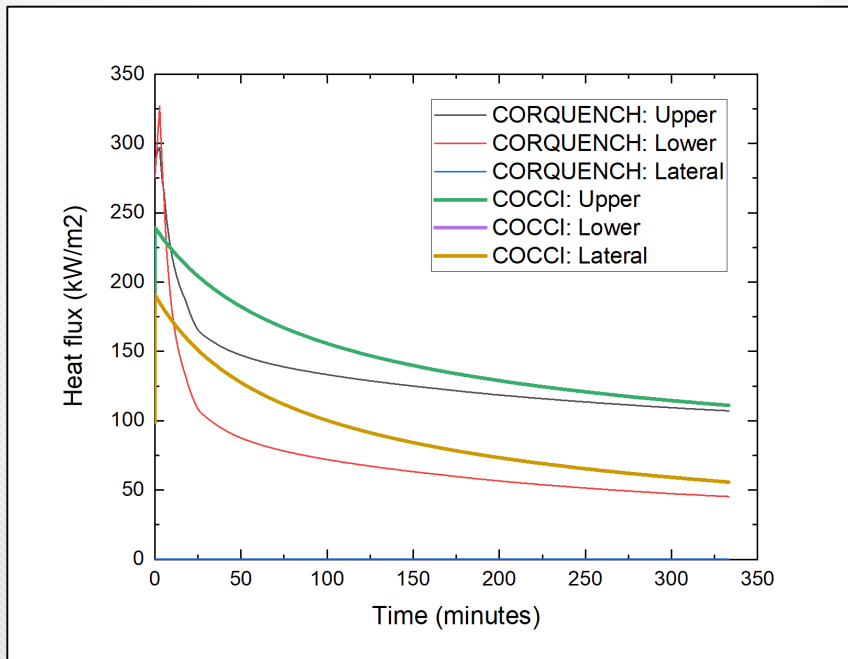


Fig. 4. Comparison of heat flux

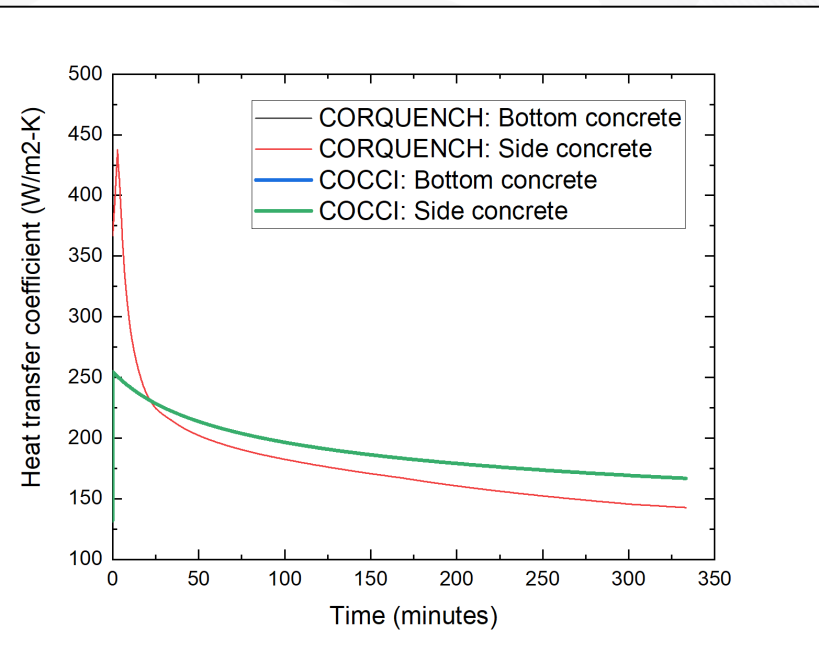


Fig. 5. Comparison of heat transfer coefficient

03 Result

❖ Comparison of elevation and mass

- In COCCI, increase rate of **corium mass and volume** are higher comparative to **ablation rate**.
- It was assumed that the whole **decomposition gas** remains in corium so that the estimated **bulk melt temperature** is also higher in COCCI.

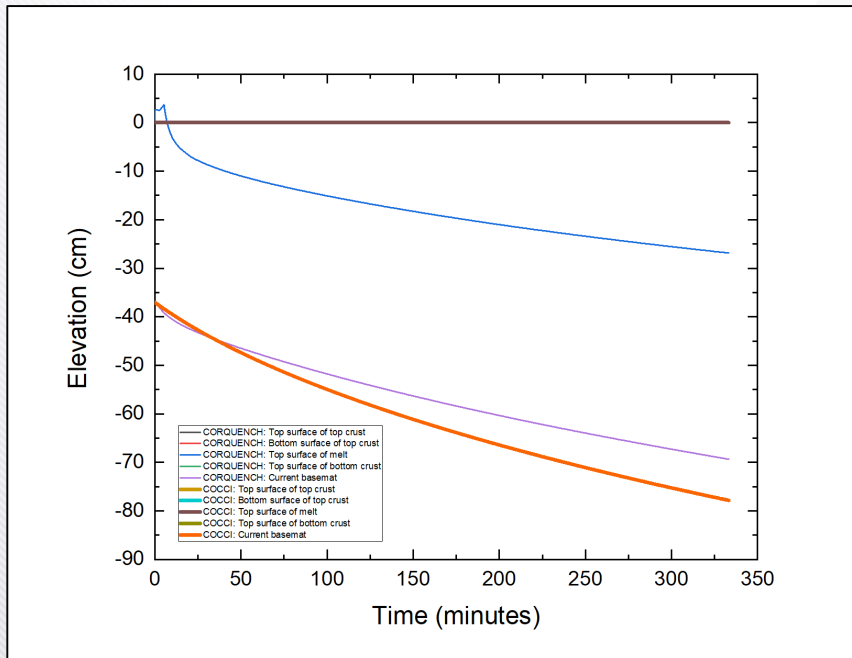


Fig. 6. Comparison of elevation

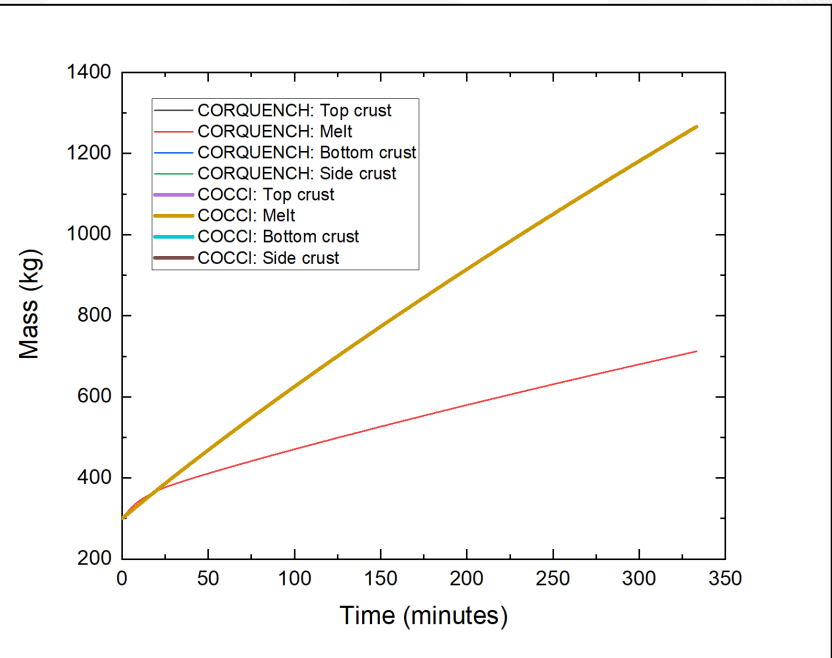


Fig. 7. Comparison of mass

04 Conclusion

❖ Summary and further study

- Both **CORQUENCH** and **COCCI** predicts **ablation depth** larger than experiment, because **quasi-steady concrete decomposition model** was used.
 - **Transient concrete dry-out model** will be updated for **COCCI**.
- The estimated **heat transfer coefficient** from **CORQUENCH** and **COCCI** was different in early phase because several **corium material properties** were different.
 - Change of all **corium material properties** by **concrete decomposition** will be updated for **COCCI**.
- The estimated increase rate of **corium mass and volume** is higher in **COCCI** comparative to **ablation rate** because it was assumed that the whole **decomposition gas** remains in corium so that the estimated **bulk melt temperature** is also higher.
 - **Decomposition gas behavior model** will be updated for **COCCI**.

THANK YOU

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