# A study for quantitative analysis of I-129 in radioactive waste using a high-temperature combustion furnace

Chae-yeon Lee <sup>a,b</sup>, Ji-Young Park<sup>a</sup>, Hyuncheol Kim<sup>a</sup>, Jong-Myoung Lim<sup>a</sup>,

<sup>a</sup>Korea Atomic Energy Research Institute, 111, Daedeok-daero 989, Yuseong, Daejeon, Republic of Korea <sup>b</sup>Chungnam National University, 99, Daehak-ro, Yuseong-gu, Daejeon, Republic of Korea <sup>\*</sup>Corresponding author: jmlim@kaeri.re.kr

### 1. Introduction

Radioactive wastes such as concrete and soil are generated during decommissioning, and it is very important to accurately identify the concentration of nuclides such as <sup>129</sup>I to dispose of them and evaluate the cost of treatment [1]. <sup>129</sup>I is a nuclide of major interest from a disposal point of view because it has a very long half-life of  $1.57 \times 10^7$  years.

To determine the radioactivity of <sup>129</sup>I in solid samples, the alkaline extraction and solvent concentration method have been widely used. However, the method should use many chemical reagents to change the oxidation states of iodine, and therefore, the analytical process becomes complicated [2]. Conversely, the pretreatment technique using the volatilization characteristics of iodine is a method of separate and concentrate <sup>129</sup>I by absorbing gaseous <sup>129</sup>I volatilized at a high temperature into a trap solution [3]. It can effectively remove organic matter in the sample and has the advantage of simplifying the matrix by extracting only the pure nuclides to be analyzed. Therefore, it can be measured directly without a separate purification process.

In this study, an experimental recovery evaluation of the method of extracting <sup>129</sup>I from a sample using a high-temperature combustion furnace was conducted. And the applicability of simultaneous analysis of gaseous nuclides such as <sup>3</sup>H and <sup>14</sup>C by optimizing the combustion conditions was checked. Also, the effectiveness of <sup>129</sup>I concentration measurement using ICP-QMS (quadrupole ICP-MS) was evaluated.

#### 2. Methods and Results

# 2.1 Combustion conditions optimization

An experiment was conducted to confirm the optimal combustion conditions for extracting <sup>129</sup>I using Pyrolyser-6 Trio<sup>TM</sup> Furnace under 6 different combustion conditions. The method validation samples were prepared by putting about 3 g of sea sand on the sample boat, and then spiked with 0.2 g of <sup>129</sup>I (17.19 Bq g<sup>-1</sup>). The temperature of the second zone in the furnace tube was raised to 800 °C before start sample burning, and then the sample was put in. As a trap solution, 1.0 M NaOH 20 mL was put in a bubbler and used. After combustion, 8 mL of the trap solution and 12 mL of Gold Star were added to a 20 mL plastic vial to prepare a sample for LSC measurement and then

measured for 30 minutes. To evaluate the recovery, 0.2 g of <sup>129</sup>I (17.19 Bq g<sup>-1</sup>) was spiked into a vial same way to prepare a standard sample and measured together.

To effectively extract <sup>129</sup>I in the sample using the combustion furnace, it is important to inject an appropriate flow and transport it to the trap solution. When comparing the condition 1 (only air) and 2 (air and  $O_2$  at >450 °C), it was confirmed that  $I_2$  was more effectively oxidized to IO3<sup>-</sup> and well trapped in the form of I<sup>-</sup> in Condition 2. The recoveries of the condition 3 and 4, using 7 g of Pt catalyst, were significantly lower than those of the conditions 1 and 2 which the catalyst was not used. Through the memory effect test, loss of <sup>129</sup>I was ascertained that <sup>129</sup>I remained in the catalyst. The recovery according to the amount of catalyst was compared. When the catalyst was reduced to 5 g, the recovery significantly increased about 2 times. Finally, the combustion conditions for the extract <sup>129</sup>I in the solid samples were optimized with condition 5 as showed in the Table I.

Table I: <sup>129</sup>I recovery according to combustion conditions

Condition	Catalyst	Flow	Time	Recovery (%)	
				Mean	SD
1	-	Only Air	3hr	77	10
2	-	$\operatorname{Air} \to \operatorname{O}_2$	3hr	99	10
3	7 g	Only Air	3hr	34	12
4	7 g	Air $\rightarrow O_2$	бhr	24	9
5	5 g	Air $\rightarrow$ O <sub>2</sub>	бhr	77	9
6	10 g	Air $\rightarrow O_2$	6hr	50	11

Using the Pyrolyser-6 Trio<sup>TM</sup> Furnace, <sup>3</sup>H and <sup>14</sup>C can be analyzed with a recovery of more than 95 % [4]. <sup>3</sup>H and <sup>14</sup>C were extracted by applying the combustion conditions optimized in this experiment. <sup>3</sup>H and <sup>14</sup>C were separately trapped with 0.01M HNO<sub>3</sub> and Carbosorb<sup>®</sup> E+, respectively. The average recovery of <sup>3</sup>H and <sup>14</sup>C were about 90 % and 101 %, respectively. Since both nuclides were effectively trapped, it was possible to determine the applicability of simultaneous extraction of <sup>3</sup>H and <sup>14</sup>C under the combustion conditions of <sup>129</sup>I.

# 2.2 Confirmation of catalyst necessity

When a sample containing a lot of organic matter is analyzed with a combustion furnace, a lot of carbonaceous gas may be generated. In this case, the catalyst may serve as oxidizer to minimize contamination of the trap solution due to incomplete combustion flue gas. The different amount of catalyst was filled for each tube and dried chicken were burned. As the amount of catalyst decreased, the color of the trap solution changed to yellow. When the colored samples were measured by LSC and the SQPE values were compared. As compared with the standard solution, the SQPE values of the samples using 0 g and 3 g of the catalyst dropped significantly, and it was confirmed that there was no difference from 5 g as shown in the Figure 1. When the SQPE value decreases as resulted color quenched in sample, the counting efficiency dramatically decreases. Therefore, it was possible to confirm the necessity of a catalyst when using a combustion furnace.



Fig. 1. Quenching effect according to the amount of catalyst

### 2.3 Availability of nitric acid trap solution

An experiment was conducted to confirm the applicability of 0.01M HNO<sub>3</sub> as a trap solution of <sup>129</sup>I using the combustion conditions optimized in Table 1. When the 0.01M HNO<sub>3</sub> 20 mL for the <sup>129</sup>I trap solution was used, it was found that <sup>129</sup>I was hardly trapped. Addition of 0.1 g of NaHSO<sub>3</sub> as a reducing agent to the same solution led recovery rate up to 85 %. This is because NaHSO<sub>3</sub> oxidizes volatilized I<sub>2</sub> to stable I<sup>-</sup> and serves to be well trapped in the solution [3]. However, since there is a possibility that the reducing agent used in the trap solution may reduce the intensity during ICP-QMS measurement, the amount was reduced to 0.05 g. As a result, it showed a recovery of 87%. It was confirmed that 0.05 g of a reducing agent can be added to 0.01M HNO<sub>3</sub> as a trap solution of <sup>129</sup>I.

Table II: Comparison of recovery according to trap solution

Trap solution	Recovery of <sup>129</sup> I (%)		
	Mean	SD	
0.01M HNO3	4	1	
0.01M HNO <sub>3</sub> + NaHSO <sub>3</sub> 0.1g	85	13	
0.01M HNO <sub>3</sub> + NaHSO <sub>3</sub> 0.05g	87	14	

2.4 Analyzing the <sup>129</sup>I using ICP-QMS

Finally, the ICP-QMS and LSC measurement for the extracting <sup>129</sup>I using a tube furnace was compared. 8 mL was measured by LSC, and 1 mL was diluted 10-fold with ultrapure water and measured by ICP-QMS. The analytical results for the same samples were compared in the Table III. When analyzing <sup>129</sup>I by ICP-QMS, <sup>129</sup>Xe contained as an impurity in argon gas used for plasma formation affects the background concentration. However, when the blank sample was measured in this experiment, it was at a level of 30 pg g<sup>-1</sup>, which was determined to be negligible. As presented in Table III, analytical results were in a similar average recovery of about 60 %. Thus, it was confirmed that effective quantitative analysis of <sup>129</sup>I was possible with ICP-QMS.

Table III: Comparison of LSC and quadrupole ICP-MS in Mini-tube furnace analysis

	Recovery of <sup>129</sup> I (%)					
Sample ID	LSC		ICP-QMS			
	Mean	SD	Mean	SD		
Tube 1	79	17	72	10		
Tube 2	35	13	35	10		
Tube 3	80	13	80	10		
Tube 4	45	13	51	17		
Tube 5	81	11	84	7		
Tube 6	40	19	45	11		

#### 3. Conclusions

The analytical method validated in this study to the analysis of <sup>129</sup>I in decommissioned waste could be used to quickly classify and treat large capacity radioactive waste with a simple process. In addition, it is possible to extract volatile radionuclides at the same time through a single combustion process. For <sup>3</sup>H and <sup>129</sup>I collected in the same solution, the concentration measurement is different using LSC and ICP-QMS, respectively. Since they do not affect mutually measured values, accurate quantitative analysis of <sup>129</sup>I is possible. In actual sample analysis, 0.01M HNO<sub>3</sub> and Carbosorb<sup>®</sup> E+ can be used as trap solutions. <sup>3</sup>H and <sup>129</sup>I can be collected in 0.01M HNO<sub>3</sub> and <sup>14</sup>C in Carbosorb<sup>®</sup> E+.

Therefore, analysis of <sup>129</sup>I using a combustion furnace is expected to not only have excellent applicability as an efficient analysis process at the decommissioning site, but also be utilized in daily environmental radioactivity evaluation.

### REFERENCES

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