

Investigation of Spray Characteristics in TOSQAN-101 Experiment Using OpenFOAM CFD Simulation

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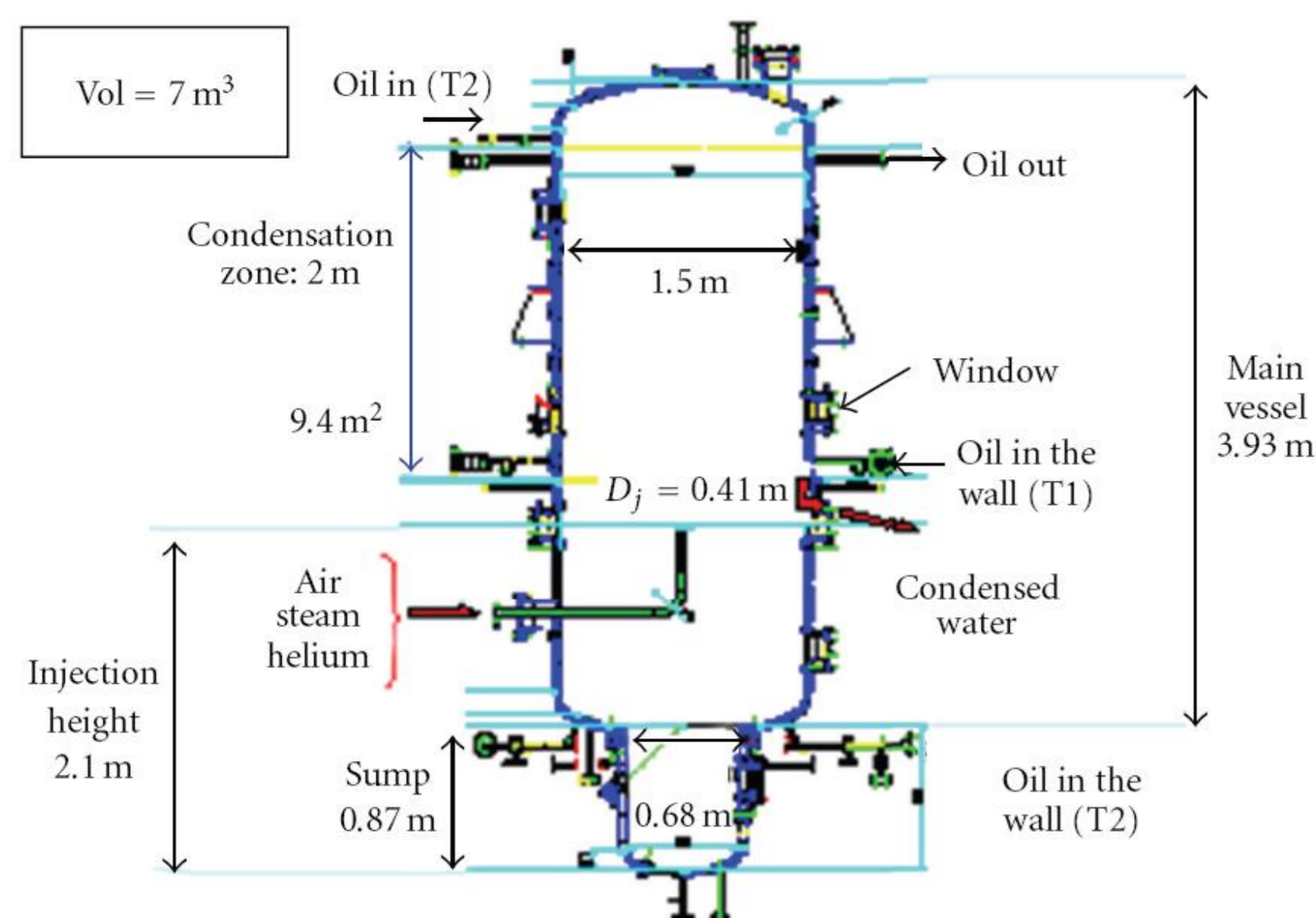
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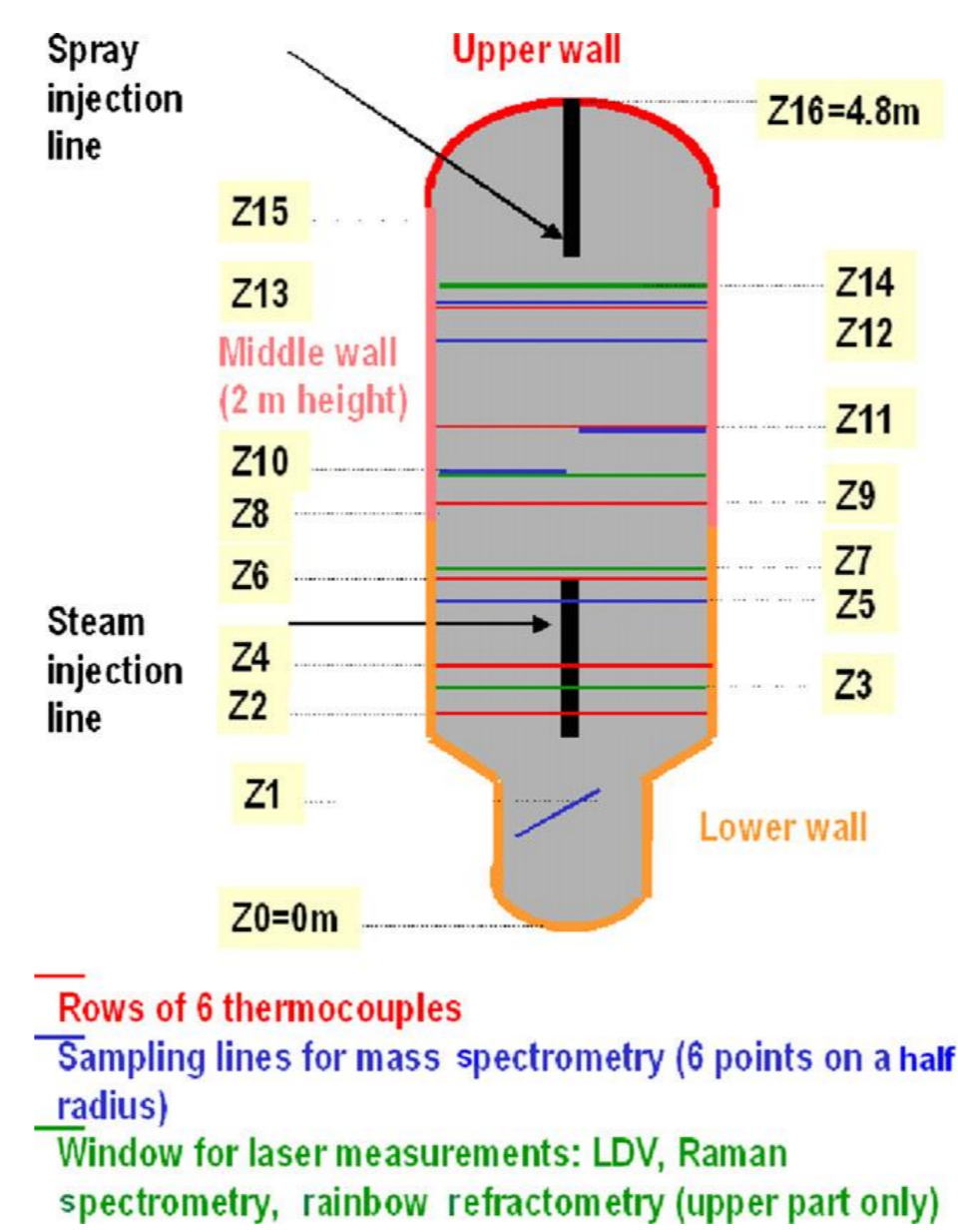
1. Introduction

Backgrounds

- Containment spray
 - When the reactor core is damaged, the containment building becomes heated and pressurized by steam emitted from RCS
 - The spray** is used to cool and depressurize the containment building
 - However, **re-pressurization** due to free volume decrease and **increase of H₂ concentration** due to steam condensation
- TOSQAN-101 experiment
 - TOSQAN-101 experiment : Examined influence of spray in reducing steam partial pressure in air-steam mixture, conducted by IRSN



The geometry of TOSQAN vessel



Measurement points of TOSQAN vessel

Objectives

- To analyze TH behavior and spray characteristics of the TOSQAN-101 experiment using CFD
- In OpenFOAM-v2112 environment, used **Euler-Eulerian** framework

2. Computational Methods

Mesh system

- 223,056 cells, mostly hexahedrons
- Wall boundaries are divided to reflect temperature data that varies with height

Numerical solver

- reactingTwoPhaseEulerFoam
 - Euler-Eulerian two-phase flow solver** that can consider multiple species

Interfacial momentum transfer

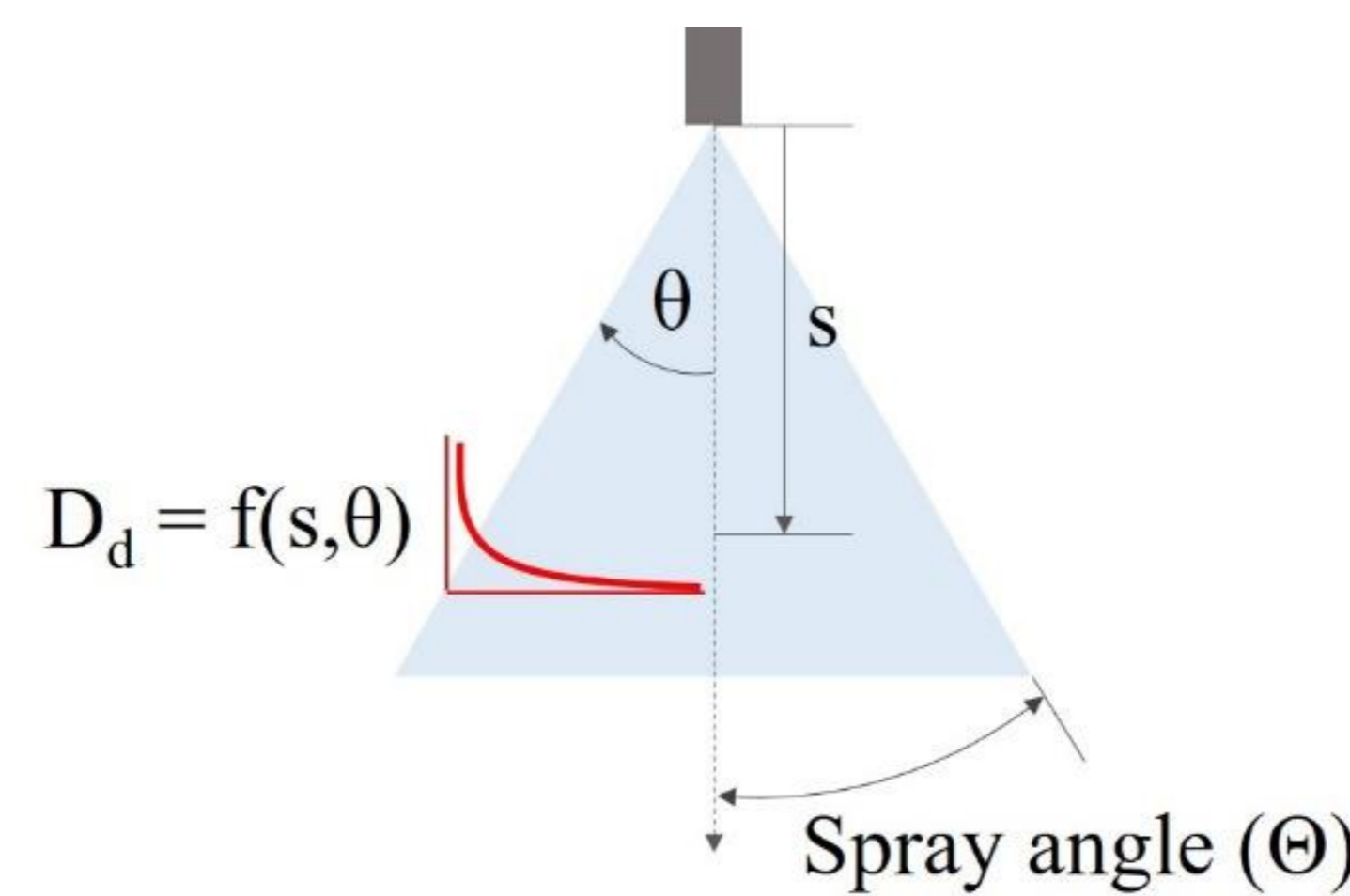
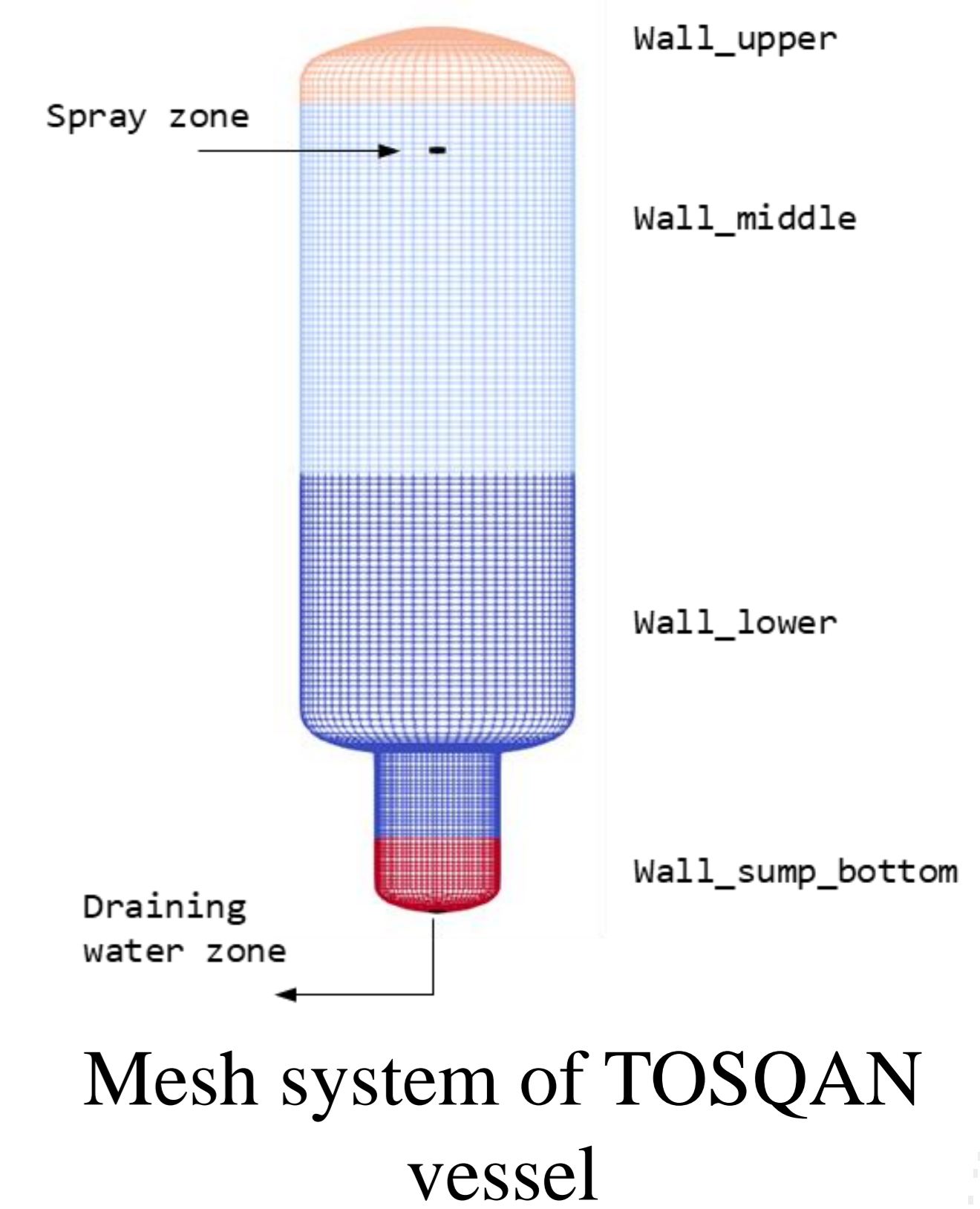
- Drag force : Schiller-Naumann
- Turbulent dispersion force : Custom model
 - To simulate spreading of spray
 - Turbulent dispersion coefficient is modeled as a **function of distance from the origin of spray injection and the spraying angle**

Wall temperature boundary condition

Time [s]	Upper [°C]	Middle [°C]	Lower [°C]
0	121.8	122.3	121.7
50	121.4	121.6	121.3
200	120.8	120.4	120.3
700	120.3	120.0	119.4
1000 ~	119.3	120.1	115.4

Boundary conditions for spray

Spray flow rate [g/s]	29.96
Spray angle [°]	55
Spray injection height [m]	4.13
Droplet size [μm]	200
Vertical droplet velocity [m/s]	10
Droplet injection temperature [°C]	At t = 0 s : 119.1 At t = 120 s : 22.1 From t = 1000 s : 27.7
C _{td} value by distance from origin of injection	0 m : 1×10 ⁵ 0.5 m : 5×10 ⁵ 1.5 m : 10 ⁶ 3 m : 0



Expression of turbulent dispersion coefficient model

$$M_d^{td} = -D_d \times \nabla \alpha_d \quad (1)$$

$$D_d = C_{td} \times \left(\frac{\theta}{\Theta}\right)^n \quad (2)$$

3. Results and Conclusions

- At the beginning of the experiment, the steam volume fraction (SVF) was decreased rapidly near the injector → **Condensation has occurred**
- In CFD, the SVF increased slightly and then decreased gradually → **Condensation is not predicted properly**
- The slope of pressure decrease in the experiment and CFD is also different, and after 1500 s in CFD results, pressure increase again
- It is judged that there was a problem in calculating the composition at the interface between phases in **predicting the condensation of steam**
- The spray model and saturation pressure models that influence the composition at the interface between phases will be reviewed.

