

Feasibility Study on the Application of ^4He Gas Scintillator Detector in Differential Die-Away(DDA) System by using MCNP Simulation

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1. Introduction

Dry storage casks were considered to temporarily store spent nuclear fuel in a Pressurized Light Water Reactor (PLWR or PWR). According to relevant domestic laws and regulations, the account of spent nuclear fuel information should be provided. The information on spent nuclear fuel includes the history of irradiation, burn-up rate, uranium mass (special nuclear material), shape, and mass.

The Differential Die-Away(DDA) analysis method measures induced fission neutrons generated by irradiating fissile material with neutrons. The amount and type of nuclear material can be estimated by measurement of induced fission neutrons. The DDA analysis techniques based on ^3He detectors are studied for analyzing the quantitative production of special nuclear materials in spent nuclear fuel in various countries [1-3].

In this study, MCNP simulation studies are conducted to analyze the feasibility of applying the ^4He gas scintillation detector (S670e, Arktis) to the DDA system to verify the burn-up rate and history of irradiation.

2. Method of Analysis

2.1 Neutron Detection Principle of S670e Detector [4]

This section describes the principle of fast neutron and thermal neutron measurement through the S670e detector to be used in the study. The S670e detector can acquire fast neutron and thermal neutron measurement signals simultaneously, and it uses two types of mechanisms - scintillation pulse and conversion light pulse.

The S670e detector chamber is filled with ^4He gas at 180 bar. The scintillation pulse is emitted by excited ^4He by scattering ^4He gas and fast neutrons. Inner wall side of the chamber, ^6Li is applied to detect thermal neutrons by using $^6\text{Li}(n, \alpha)^3\text{H}$. The generated alpha rays scattered with ^4He atoms and emitted the conversion light pulse.

The SiPM has measured the signal of the scintillation pulse and conversion light pulse. Each pulse characteristic has a difference. Thus, the S670e can separate the detection signal.

2.2 MCNP simulation method and DDA time-signal analysis method

MCNP simulation with ^4He gas scintillator detector was performed for neutron detection in the DDA system, and the geometry of the simulation is shown in Fig. 1.

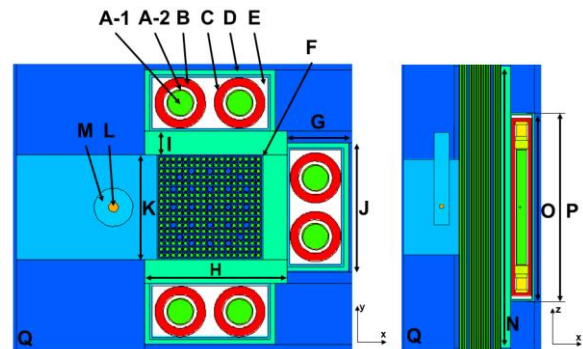


Fig. 1. Geometry of MCNP simulation.

Table I: Dimension of Component in MCNP Simulation [9]

Component	Dimension (cm)
A-1	^4He detector Dia.: 5.214 Height: 60.826
A-2	^6Li film Thickness: 0.001
B	HDPE Thickness: 0.0, 1.75
C	Cd layer Thickness: 0.0, 0.05
D	Detector Box Width: 11.74 Length: 24.96 Thickness: 0.5
E	Detector Box
F	Fuel assembly Guide Thickness: 0.23
G	Lead shield 12.74
H	Lead shield 29.41
I	Lead shield 5.0
J	Lead shield 26.96
K	Tungsten shield 21.86
L	Target of neutron generator Dia.: 2, Height: 2
M	Neutron generator Dia.: 8, Height: 50
N	lead shield 150
O	Detector Box Height: 99
P	Lead shield 100
Q	Water

The spent nuclear fuel assumed Westinghouse type 17x17, and its characteristics were derived using Scale code 6.2. The S670e detector was placed around the spent nuclear fuel, and the detailed specifications of the analysis modeling are shown in the following table 1. The HDPE and Cd layer are used for considering the effects of the neutron detection signal. HDPE is applied for analyzing the moderation effect. The Cd layer is considered to analyze the measurement effect of low-energy neutrons below 0.5 eV. The D-T (Deuterium-Tritium) generator is used as a neutron source. The neutron energy is 14.1 MeV. In this case, the neutron is generated through the neutron generator from 0 to 90 μ s by using 'tme' option. The spontaneous fission neutrons emitted from spent nuclear fuel were not considered. For the DDA time and signal analysis, the numerical equation was derived from each neutron detection data during 101~200 μ s.

3. Results and Discussion

3.1 Fast and Thermal Neutron Detection

Neutron measurement signals were analyzed for cases where the initial concentration was 2.0%, the cooling period was 5 years, the burnup was 10 and 60 GWd/tU, and the effects of HDPE and Cd layers were compared. The fast and thermal neutron detection results are shown in figures 2 and 3, respectively.

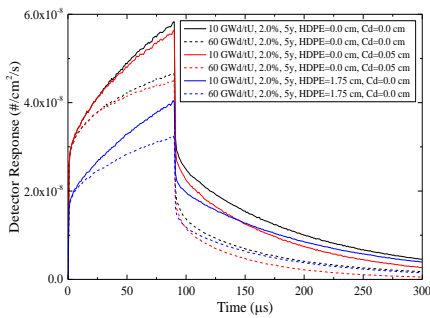


Fig. 2. Effects of HDPE and Cd layer in fast neutron detection.

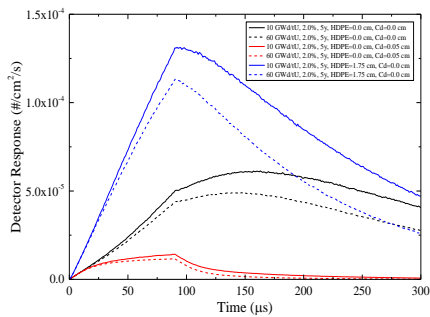


Fig. 3. Effects of HDPE and Cd layer in thermal neutron detection.

The effect of HDPE and Cd layers was observed. In detecting fast neutrons, a rapid decrease in the measurement signal was observed immediately after 90 μ s when the neutron generator was turned off. The fast neutron signal is slightly decreased in Cd layer results. However, the HDPE results show that the fast neutron signal decreased 6×10^{-8} to 4×10^{-8} #/cm²/s. The thermal neutrons results show the different effect of HDPE and Cd layer. The thermal neutron detection signal (w/o HDPE and Cd layer) is increased after 90 μ s. The thermal neutron signal in 90 μ s is about 5×10^{-5} #/cm²/s. When the HDPE is applied, the thermal neutron signal in 90 μ s is increasing 5×10^{-5} to 1.2×10^{-4} #/cm²/s. It is seen that the decrease in the fast neutron signal causes an increase in the thermal neutron signal. However, when the Cd layer is applied, the thermal neutron signal decreases 5×10^{-5} to 2×10^{-5} #/cm²/s. It can be shown that the Cd layer interrupts the incident of scattered neutrons in the water below 0.5 eV to the detector.

3.2 DDA time-DDA signal analysis

This section discusses the DDA time and DDA signal analysis results with HDPE and Cd layer effects. In this case, various spent nuclear fuel properties are used as follows:

- Initial enrichment: 2.0, 3.0, 4.0, 5.0%
- Burn-up rate: 15, 30, 35, 40, 45, 50, 55, 60 GWd/tU

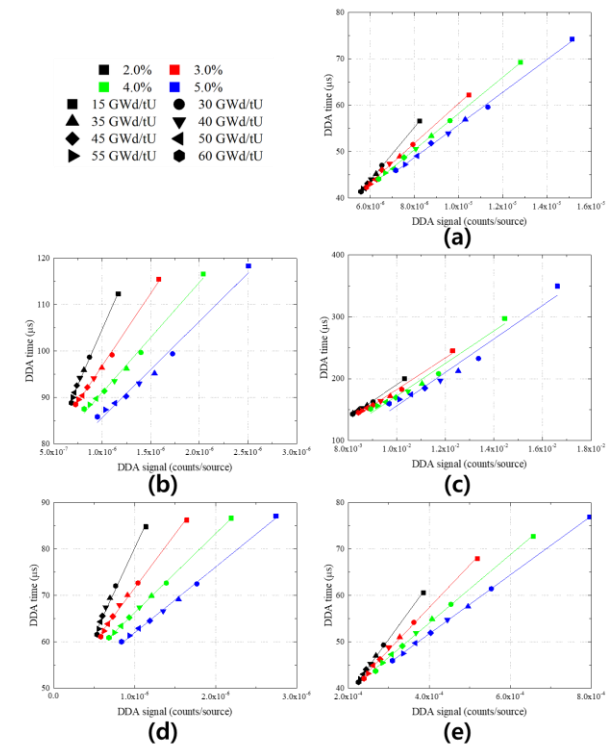


Fig. 4. DDA signal-DDA time analysis results.

Figure 4(a) shows the results of previous studies (6 bar of ^3He detector used) [3]. The results show the DDA signal range is $5.5 \times 10^{-6} \sim 1.5 \times 10^{-5}$ counts/source, and the DDA time range is 41~75 μs . In these results, the high initial enrichment with a low burn-up rate case has the largest DDA signal and time. It has the most significant amount of nuclear material in simulated cases. However, the lower initial enrichment with a high burn-up rate case has the smallest DDA signal and time. In other words, if the amount of nuclear material is small, the DDA signal and DDA time are also small.

Figures 4(b) and 4(c) are the DDA signal and DDA time analysis results for fast neutrons and thermal neutrons of the S670e detector with HDPE, respectively. In the fast neutron results, the DDA signal is lower than in previous results (Fig. 4(a)). However, the DDA time increased to 85~120 μs . In the thermal neutron results, the DDA time was significantly increased to 150~350 μs compared to the previous results of 40~75 μs , and the DDA signal was about 103 times larger.

Figures 4(d) and 4(e) are the DDA signal and DDA time analysis results for fast neutrons and thermal neutrons with the Cd layer. In the fast neutron results, the DDA time is 60~87 μs , and the DDA signal is $5 \times 10^{-6} \sim 2.7 \times 10^{-6}$ counts/source. Compared to fig. 4(a) and fig. 4(d), the DDA signal slightly decreased in this case, but DDA time increased. However, the thermal neutron results showed no significant difference in DDA time, but the measured signal increased about 30~50 times.

As a result of DDA time and DDA signal analysis, the case of using the S670e detector shows a more apparent difference in the DDA signal and DDA time than the case of using the existing ^3He detector. Therefore, it can be confirmed that there is an advantage in applying the S6703 used in this study to the DDA system.

4. Conclusion

The DDA analysis method confirms the special nuclear material in spent nuclear fuel. The induced fission neutron and spontaneous fission neutron energy are above 1 MeV. Thus, the fast neutron detection without moderation method can be considered for the DDA analysis method. The ^4He detector has some advantages of being applied to DDA analysis technology. It can measure fast and thermal neutrons at the same time. In this study, S670e, fast and thermal neutron detector, is used for the analysis of applying the DDA system by using MCNP simulation. The results show that the S670e fast and thermal neutron detector applies to the DDA system. In the future, quantitative studies will determine the amount of specific nuclear materials in spent fuel using the ^4He gas scintillation detector (S670e)-based DDA system.

REFERENCES

- [1] T. Martinik, et. al., Design of a Prototype Differential Die-Away Instrument Proposed for Swedish Spent Nuclear Fuel Characterization, Nuclear Instruments and Methods in Physics Research Section A, Vol. 821, 55-65, 2016.
- [2] T. H. Lee, et. al., Monte Carlo simulations of differential die-away instrument for determination of fissile content in spent fuel assemblies, Nuclear Instruments and Methods in Physics Research Section A, Vol. 652, No. 1, 103-107, 2011.
- [3] C.W.Lim et al., Development of Computational Modeling and Simulation Methodology to Estimate Special Nuclear Materials by DDA and DDSI Technique(NSTAR-21P352-42), KoFONS, 2021
- [4] A.R.D. Ltd., Arktis S670(e) Detector series Operating Manual, Arktis Radiation Detector Ltd, 2018.

Acknowledgements

This work was supported by the Nuclear Safety Research Program through the Korea Foundation of Nuclear Safety (KoFONS) using the financial resource granted by the Nuclear Safety and Security Commission (NSSC) of the Republic of Korea (No. 2106016).