

# **Assessment of Fission Product Migration in Molten Salt and Metal Reactor (MSMR)**



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## **Summary & Conclusions**

# Introduction (1/2)

## Needs for mobile power source

- Deployment of large nuclear reactors becomes inadequate for:
  - Military base
  - Mining industry
  - Small village in remote area
  - In space (Moon & Mars) and spacecraft...
- Often, fossil fuel (mostly diesel) based generators are utilized
  - Adverse effect(s) stemming from CO<sub>2</sub> emission
- As one of the remedies, miniaturized reactor concept is pursued



## Ultra-micro reactor

- A miniaturized reactor small enough to be loaded in a container and could be easily transported by a vehicle
  - Container size: 234.8 cm width, 239.0 cm or 269.5 cm height
- Realization via Molten Salt Reactor (MSR) concept?



# Introduction (2/2)

## Molten salt reactor (MSR)

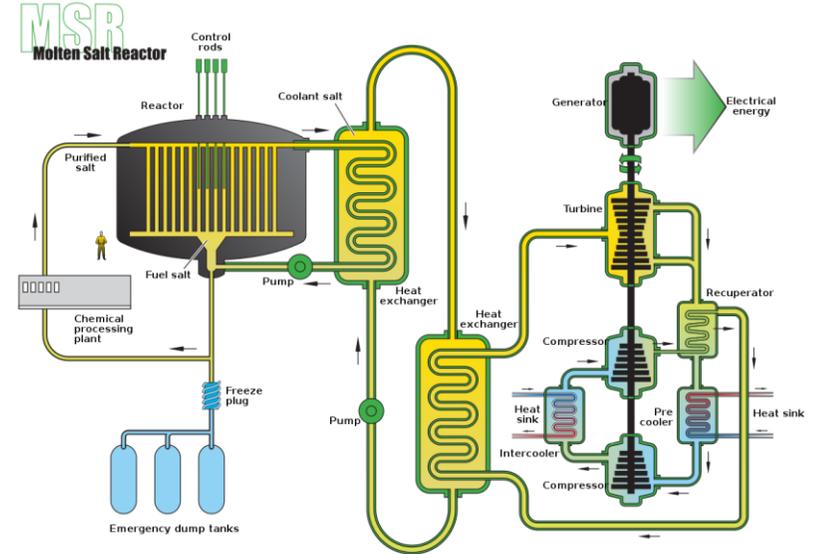
- Reactor which consists of molten salt (dissolved fuel), where the salt acts as both fuel and coolant
  - circulates between the active core and heat exchanger
- Superior inherent safety attributes:
  - No meltdown, no hydrogen explosion
  - Strong negative feedback originating from thermal expansion of fuel salt

## Limitation of Thermal spectrum MSR

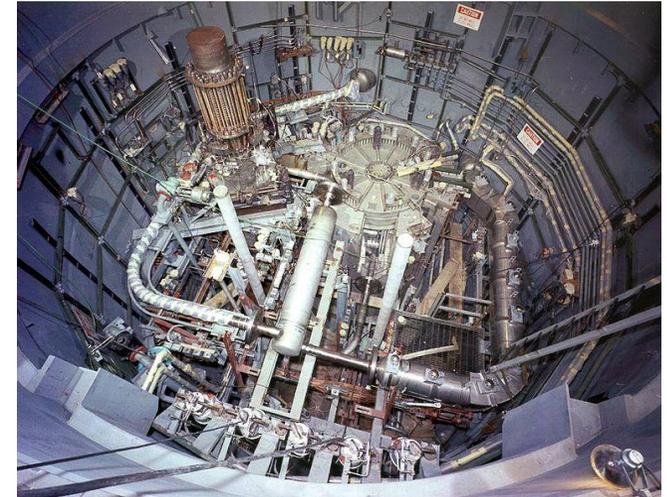
- Proliferation concern by online fuel reprocessing
- Production of radioactive waste from the usage of graphite moderator & Generation of tritium

## Limitation of HALEU-loaded MSFR for ultramicro reactor

- HALEU: High Assay Low Enriched Uranium (<19.75 w/o)
- Calculated cylindrical MSFR size for criticality (NaCl-UCl<sub>3</sub> fuel / eutectic composition)
  - Reactor diameter should be at least 215 cm & Fuel inventory about 20-30 tons.
  - Too large to be loaded in a container ---
  - To overcome, MSMR concept is proposed.



Schematic diagram for MSR



ORNL MSRE

# Concept and Modelling of MSMR (1/4)

## Liquid metal as fuel

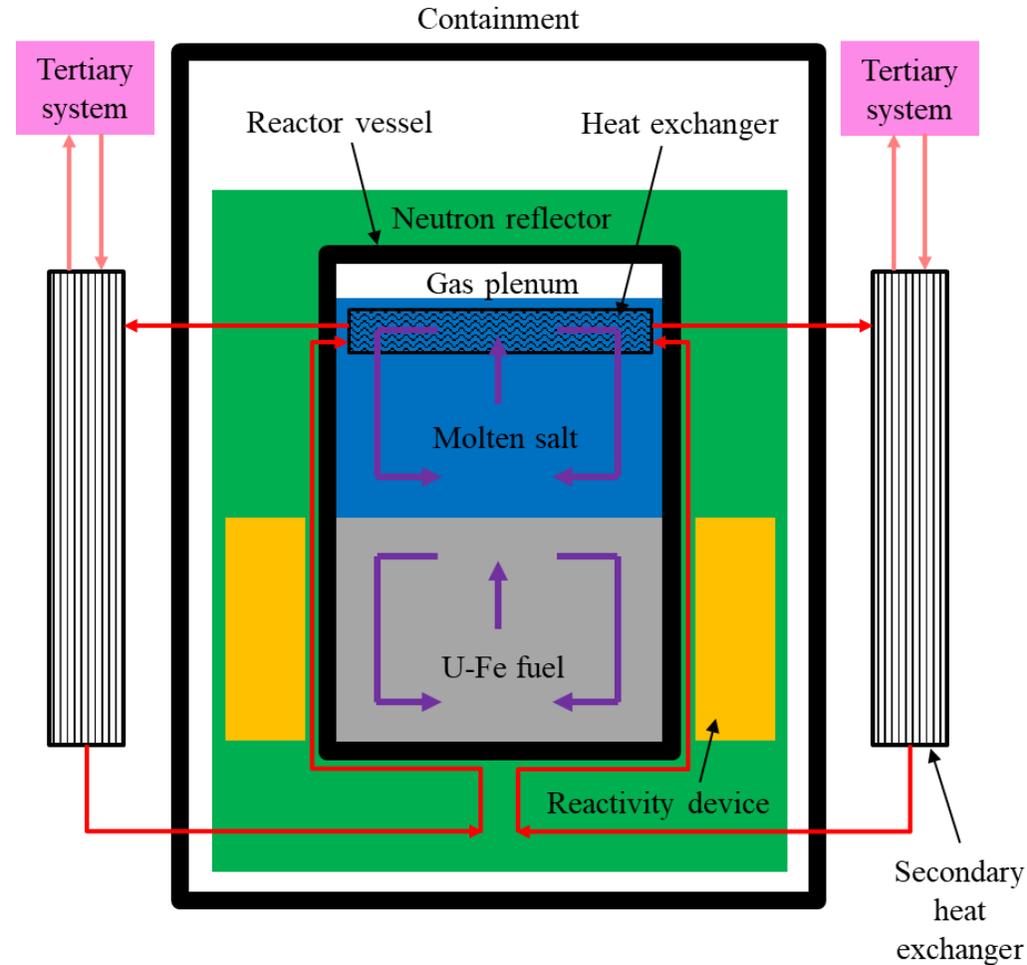
- Generates the heat
- Compact fuel
  - High conversion ratio
  - Small core size
  - Low fuel mass

## Molten salt as coolant

- Natural circulation or pump operation
- Trap of non-gaseous fission products
  - Noble metal in the liquid fuel
  - Non-noble metal (Cs, I, Sr etc) in the salt

## Secondary system

- Removing heat from primary system
  - Flowing through the heat exchanger
  - Cooling outer surface of reactor vessel



# Concept and Modelling of MSMR (2/4)

## Liquid metallic fuel (U-Fe alloy)

- Eutectic composition:
  - 66-34 (number), 89-11 (mass)
  - Melting temperature: 723°C
- Density for U and Fe

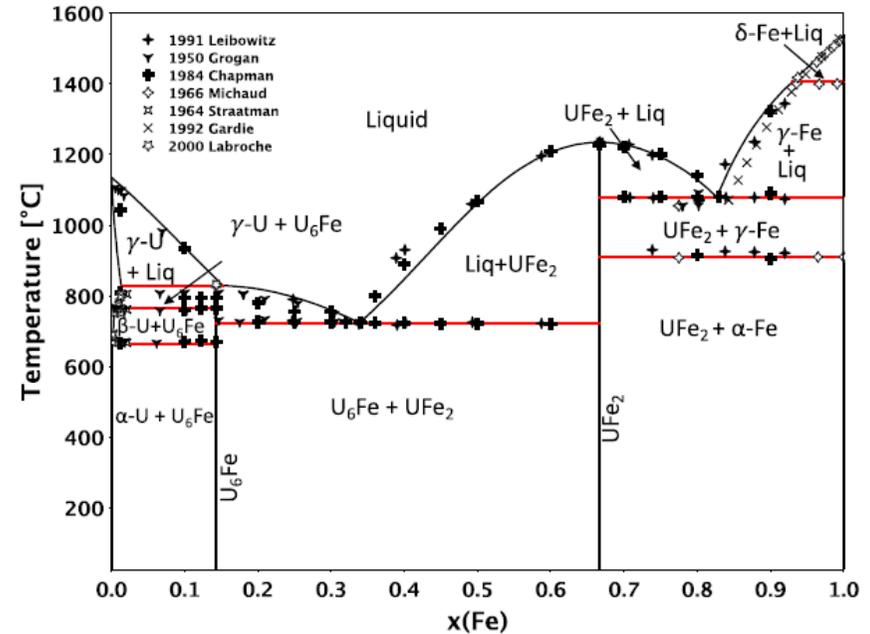
$$\rho(T) = A - BT$$

Metal	A	B
Fe	8.618	8.83e-4
U	19.520	1.601e-3

- Density for mixture: Ideal Liquid Model

$$\frac{1}{\rho} = \sum_i \left( \frac{w_i}{\rho_i} \right)$$

U-Fe phase diagram



- Moore, E. E., Turchi, P. E., Landa, A., Söderlind, P., Oudot, B., Belof, J. L., ... & Perron, A. (2019). Development of a CALPHAD thermodynamic database for Pu-U-Fe-Ga alloys. *Applied Sciences*, 9(23), 5040.

- Grosse, A. V., & Kirshenbaum, A. D. (1963). The densities of liquid iron and nickel and an estimate of their critical temperature. *Journal of Inorganic and Nuclear Chemistry*, 25(4), 331-334.

- Rohr, W. G., & Wittenberg, L. J. (1970). Density of liquid uranium. *The Journal of Physical Chemistry*, 74(5), 1151-1152.

# Concept and Modelling of MSMR (3/4)

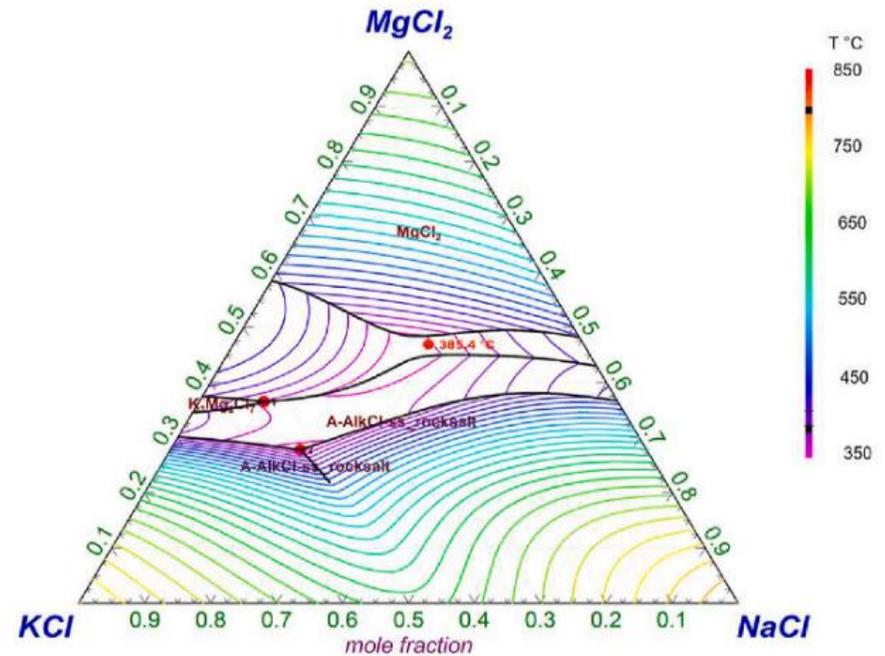
## Molten salt coolant (NaCl-KCl-MgCl<sub>2</sub>)

- Eutectic composition: 30.2-22.7-47.1 (mol)
  - Melting temperature: 385°C
- Density
  - Linear approximation of each component
  - Ideal Liquid Model

$$\rho(t) = \rho_m - k(t-t_m)$$

Formula	$t_m/^\circ\text{C}$	$\rho_m/\text{g cm}^{-3}$	$k/\text{g cm}^{-3} \text{ }^\circ\text{C}^{-1}$
NaCl	800.7	1.556	0.000543
KCl	771	1.527	0.000583
MgCl <sub>2</sub>	714	1.68	0.000271

Haynes, W. M., Lide, D. R., & Bruno, T. J. (2016). CRC handbook of chemistry and physics. CRC press.



Villada, C., Ding, W., Bonk, A., & Bauer, T. (2021). Engineering molten MgCl<sub>2</sub>-KCl-NaCl salt for high-temperature thermal energy storage: Review on salt properties and corrosion control strategies. *Solar Energy Materials and Solar Cells*, 232, 111344.

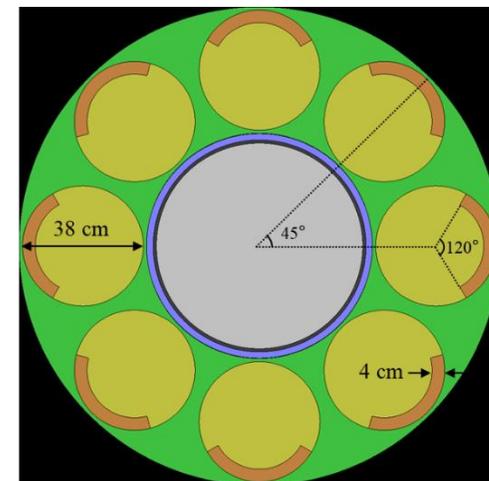
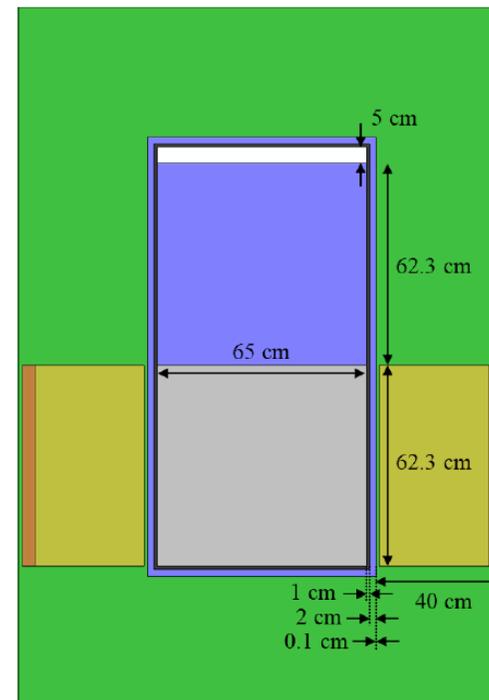
# Concept and Modelling of MSMR (4/4)

## Reactor Layout

- Fuel zone
  - Diameter = 65 cm, Height = 62.3 cm
  - Uranium enrichment = 12 wt.%
  - Fuel inventory: 2,818 kg
- Upper molten salt zone: Same as Fuel zone
  - Chloride enrichment = 99 at.% Cl-37
- Gas plenum: 5 cm
- Reactor vessel: 1 cm
- Secondary system: 2 cm thickness gap molten salt-filled
- Reflector: 40 cm SS304

## Drum-shaped reactivity control device

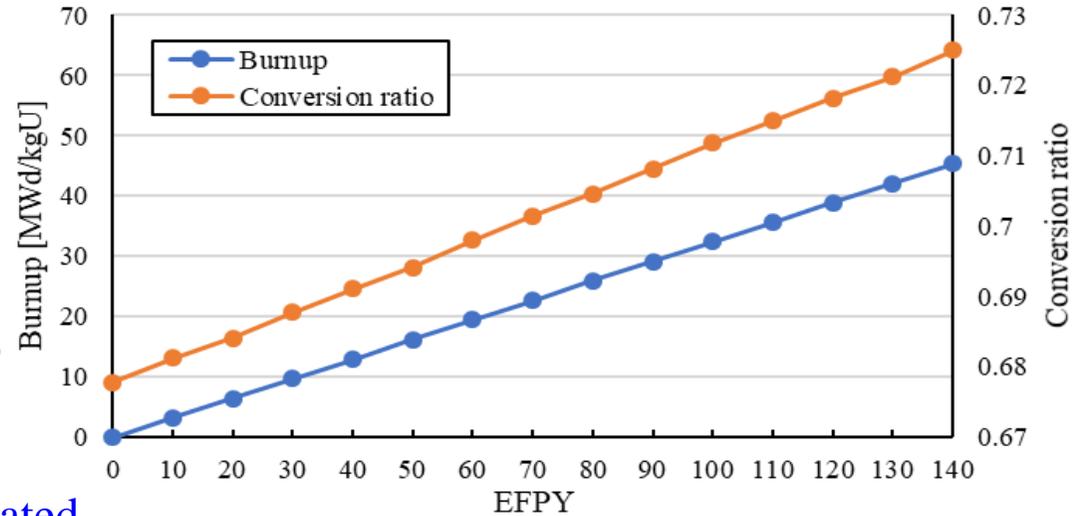
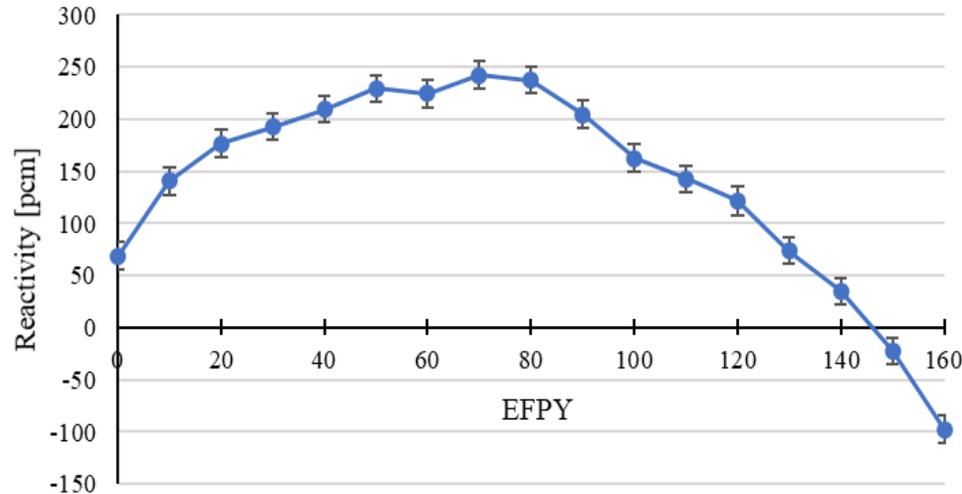
- Located in the reflector region and surrounding the active core
- Drum body: SS304 (same as a reflector)
  - The number of drums: 8
  - Height: 62.3 cm
  - Diameter: 38 cm
- Pad: B<sub>4</sub>C (98% of theoretical density, 90wt.% of B-10)
  - Pad thickness: 4 cm
  - Arc angle: 120°



# Numerical Results (1/6)

## Reactivities and conversion ratios .vs. Full-power operation time (2.5 MWth)

- Program: Serpent 2.2.0
- Samples: (History: 100,000, inactive cycle: 100, active cycle: 300)



250 pcm of maximum reactivity can be estimated.

140 years of lifetime and 45 MWd/kg of discharge burnup can be estimated.

The worth of the reactivity control drum has been estimated to  $2,629 \pm 20$  pcm

## Fuel Temperature Coefficient

Temperature range [C]	800 - 900	900 - 1000	1000 - 1100	1100 - 1200
Temperature coefficient [pcm/K]	$-2.48 \pm 0.06$	$-2.48 \pm 0.06$	$-2.51 \pm 0.06$	$-2.67 \pm 0.06$

# Numerical Results (2/6)

## Fission Product Information

- Three types of fission products
  - Noble gas, noble metal, others
- Fission products at 45 MWd/kg burnup
  - Total mass: 131.2 kg

Noble gas	gaseous fission products that do not dissolve in liquid fuel and molten salt
Noble metal	non-gaseous fission products that do not dissolve in molten salt
Salt seeker (Others)	fission products can be dissolved in molten salt

Element	Type	Mass fraction [%]	Element	Type	Mass fraction [%]	Element	Type	Mass fraction [%]
<b>Xe</b>	Noble gas	12.58606	<b>Hf</b>	Noble metal	4.52E-17	<b>Pm</b>	Others	0.038028
<b>Kr</b>	Noble gas	1.163383	<b>Hg</b>	Noble metal	1.41E-24	<b>Sm</b>	Others	2.675983
<b>Rn</b>	Noble gas	8.42E-14	<b>Tl</b>	Noble metal	4.64E-14	<b>Gd</b>	Others	0.123585
<b>Zr</b>	Noble metal	12.44069	<b>Pb</b>	Noble metal	7.71E-07	<b>Dy</b>	Others	0.002517
<b>Nb</b>	Noble metal	0.002414	<b>Bi</b>	Noble metal	8.63E-11	<b>Ho</b>	Others	8.84E-05
<b>Mo</b>	Noble metal	9.971559	<b>Te</b>	Noble metal	1.446093	<b>Er</b>	Others	0.000111
<b>Tc</b>	Noble metal	2.471687	<b>Se</b>	Noble metal	0.192263	<b>Tm</b>	Others	7.55E-06
<b>Ru</b>	Noble metal	5.93603	<b>Po</b>	Noble metal	1.80E-12	<b>Yb</b>	Others	4.25E-06
<b>Rh</b>	Noble metal	1.767941	<b>I</b>	Noble metal	0.693799	<b>Y</b>	Others	1.481246
<b>Pd</b>	Noble metal	2.280483	<b>At</b>	Noble metal	3.78E-21	<b>Rb</b>	Others	1.226256
<b>Ag</b>	Noble metal	0.124034	<b>La</b>	Others	3.629297	<b>Cs</b>	Others	8.660187
<b>Cd</b>	Noble metal	0.214767	<b>Ce</b>	Others	6.794389	<b>Sr</b>	Others	1.629292
<b>In</b>	Noble metal	0.034521	<b>Pr</b>	Others	3.39548	<b>Ba</b>	Others	6.435432
<b>Sn</b>	Noble metal	0.325362	<b>Nd</b>	Others	12.10858	<b>Br</b>	Others	0.066805
<b>Sb</b>	Noble metal	0.081617						

# Numerical Results (3/6)

## Fission Product Information

- Three types of fission products
  - Noble gas: gaseous fission products that do not dissolve in liquid fuel and molten salt
  - Noble metal: non-gaseous fission products that do not dissolve in molten salt
  - Salt seeker (Others): fission products that can be dissolved in molten salt
- Assumptions and scenarios of fission product behavior
  - All noble gases are completely removed from the fuel
  - All noble metals remain in the fuel
  - Some of the salt-seekers in the fuel migrate to the molten salt

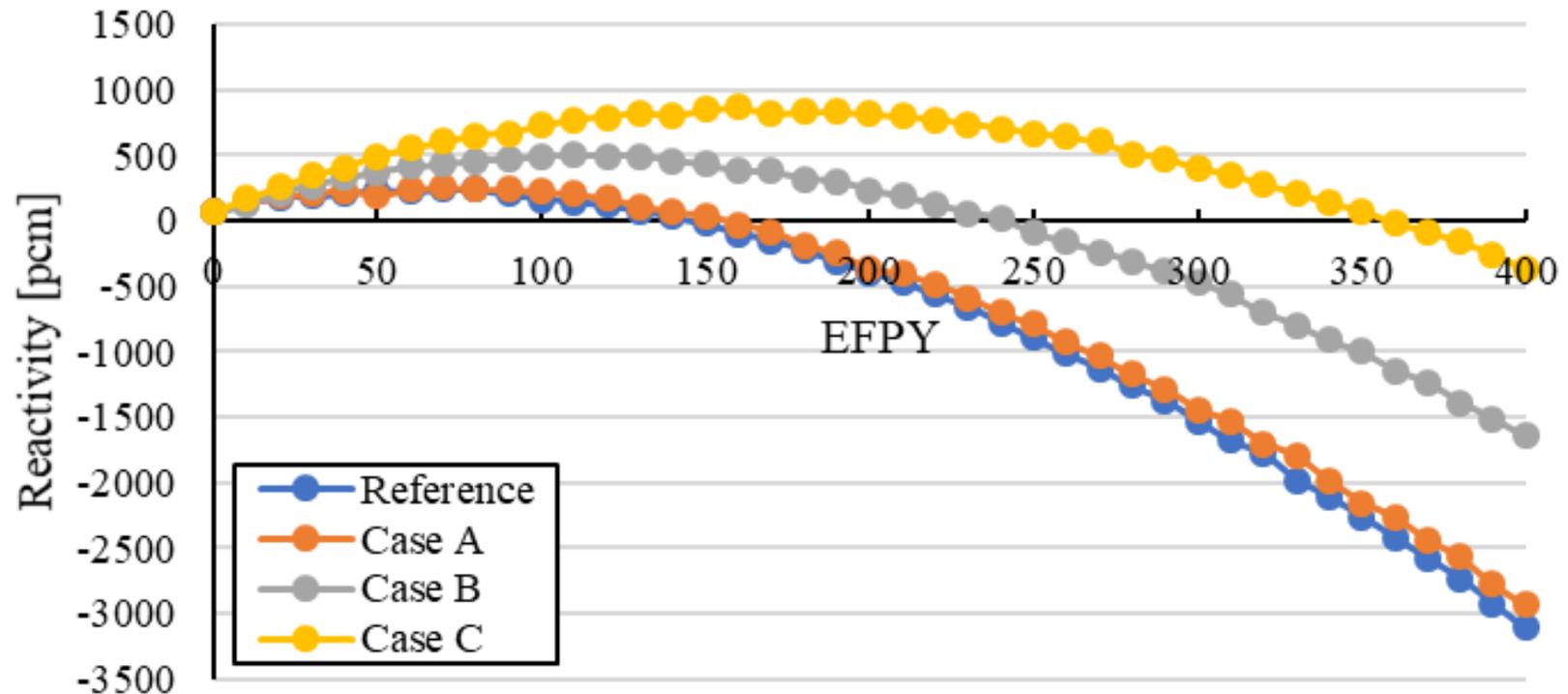
	Noble gas	Noble metal	Salt-seeker elements
Reference	Not removed	Remains in fuel	Not removed
Case A	Completely removed	Remains in fuel	Not removed
Case B	Completely removed	Remains in fuel	50% removed*
Case C	Completely removed	Remains in fuel	100% removed

\* Removal ratios of all elements are identical

# Numerical Results (4/6)

## Reactivities .vs. Full-power operation time (dependent on three scenarios)

- Program: Serpent 2.2.0, library: ENDF/B-VII.1
- History: 100,000, inactive cycle: 100, active cycle: 300

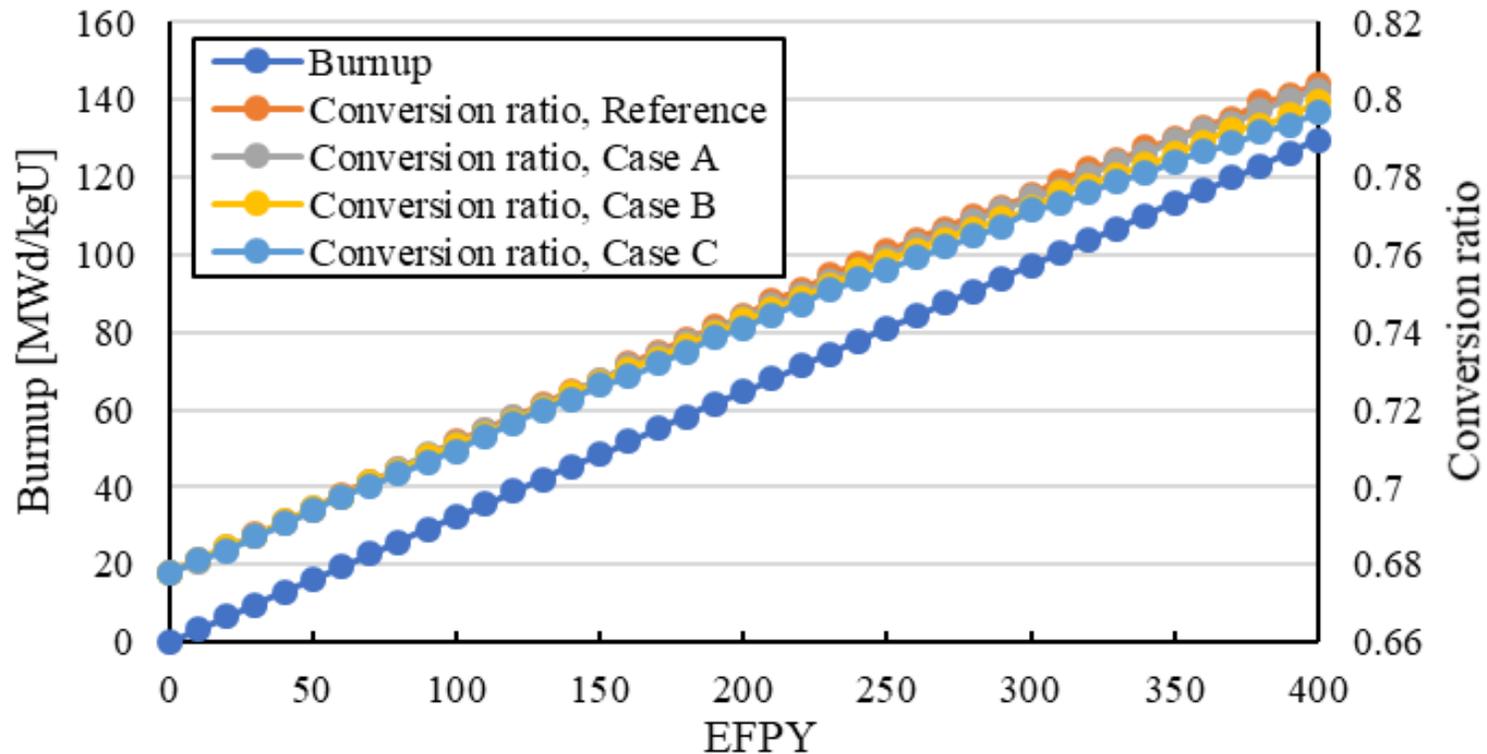


Reactivity and reactor lifetime can reach up to 870 pcm and 350 years respectively.

# Numerical Results (5/6)

## Burnup and Conversion ratios .vs. Full-power operation time

- Program: Serpent 2.2.0, library: ENDF/B-VII.1
- History: 100,000, inactive cycle: 100, active cycle: 300

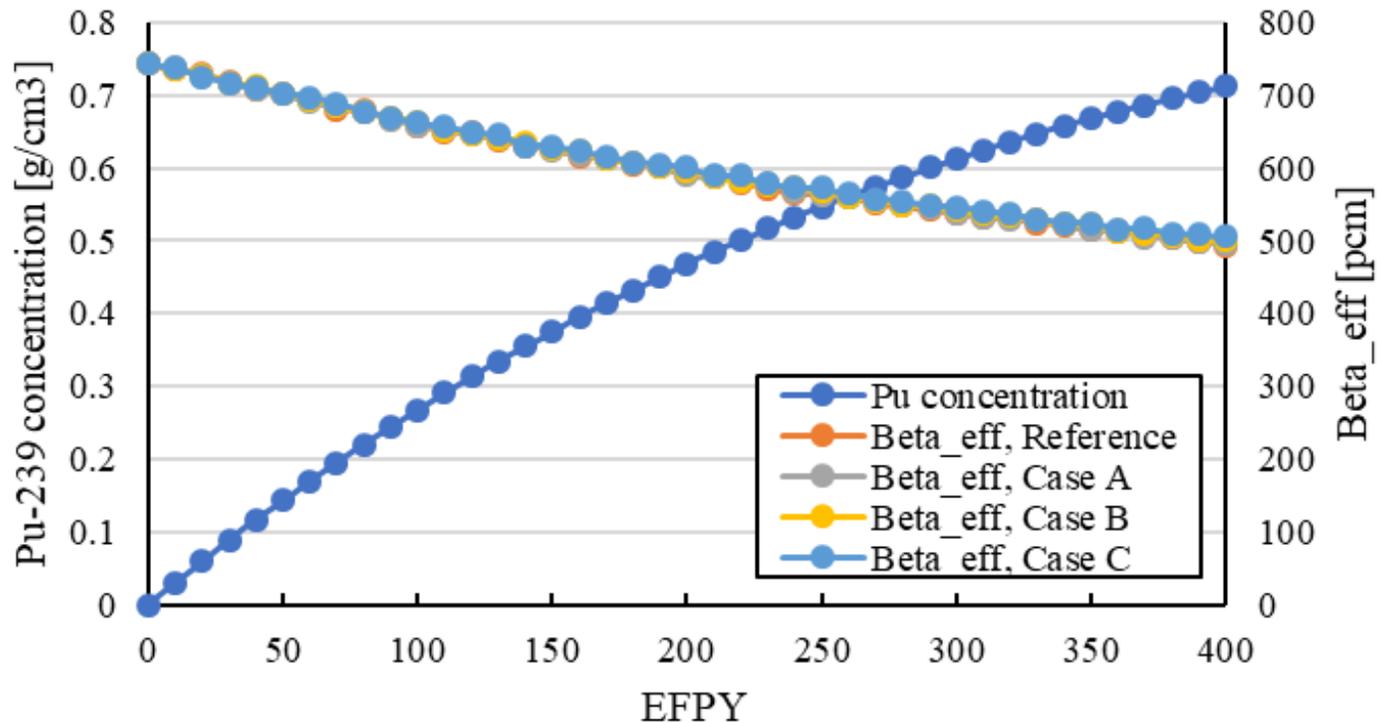


Conversion ratios rise with increasing burnup due to accumulation of Pu  
Migration of fission products hardly affects the conversion ratio

# Numerical Results (6/6)

## Pu concentration and delayed neutron fraction .vs. Full-power operation time

- Program: Serpent 2.2.0, library: ENDF/B-VII.1
- History: 100,000, inactive cycle: 100, active cycle: 300



Plutonium is accumulated and  $\beta_{\text{eff}}$  decreases with increment of burnup  
Plutonium accumulation rate dwindles due to utilization of plutonium  
Migration of fission products hardly effects  $\beta_{\text{eff}}$

# Summary & Conclusions

**The effect of fission product removal on the neutronics behavior of MSMR has been investigated**

- Expected reactor lifetime can be expanded up to 2.5 times
- Maximum reactivity can rise up to 3 times
- The evolution trends for discharge burnup, conversion ratio, and delayed neutron fraction are similar to each other

	Reference	Case A	Case B	Case C
Expected reactor lifetime	140 years	150 years	240 years	350 years
Maximum reactivity	240 pcm	260 pcm	510 pcm	820 pcm
Discharge burnup	45 MWd/kg	49 MWd/kg	78 MWd/kg	113 MWd/kg
Conversion ratio	0.67-0.73	0.67-0.73	0.67-0.76	0.67-0.78
Delayed neutron fraction	630-743 pcm	624-743 pcm	573-743 pcm	524-743 pcm

- Case A) Noble gas removed, Noble metal remains, Salt-seeker elements not removed
- Case B) Noble gas removed, Noble metal remains, Salt-seeker elements 50% removed
- Case C) Noble gas removed, Noble metal remains, Salt-seeker elements 100% removed

# Summary & Conclusions

## **The MSMR can be utilized as an ultramicro-miniaturized reactor**

- The diameter of MSMR is estimated at about 65 cm
- Fuel mass of the reactor is about 2.8 tons
- Its life is estimated to be about 140 years with 2.5 MWth
- Normal operation is guaranteed in aspect of temperature coefficient and reactivity worth

## **Behavior of fission products can alter several properties of MSMR**

- Lifetime and maximum reactivity can rise up to about 2.5 times and 3 times
- Removal of fission products can be advantage in terms of lifetime but challenges in terms of excess reactivity
- For more precise of assessment and optimization, chemical properties of fission products should be more investigated

**Thank you for your attentions**  
**Any Questions?**

