



Preliminary Study on the Effect of Control Rod Depletion for the Operation of SMR using STREAM/RAST-K

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- **Introduction**
- **Effects of control rod inserted operation**
- **Control rod depletion module in RAST-K**
- **Depletion analysis of i-SMR fuel assembly**
- **Conclusion**

Introduction



Control rod depletion for i-SMR analysis

- **innovative-Small Modular Reactor (i-SMR)**
 - **Soluble Boron Free (SBF) operation**
 - **Innovative Burnable Absorber (BA) design**
 - Control the excessive reactivity
 - CIMBA, CSBA, WABA, etc.
 - **Rod inserted operation**
 - To achieve criticality
 - **Control rod inserted operation analysis**
 - Should consider effects on fuel and control rod

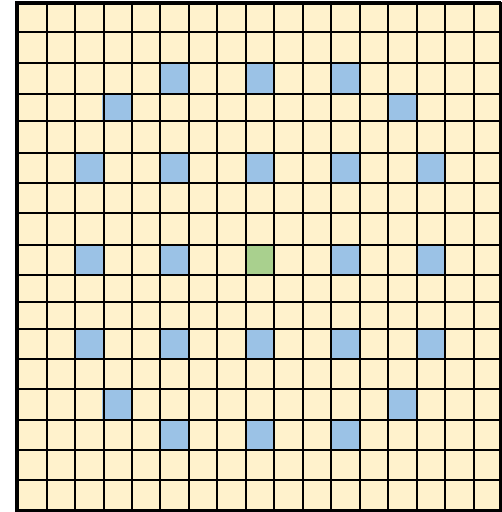
Effects of control rod inserted operation



Test case

▪ Test FA model

- 17x17 WH Fuel Assembly
- No burnable poison
- Boron concentration: 0 PPM
- Moderator Temperature: 600 K
- Fuel Temperature: 900 K

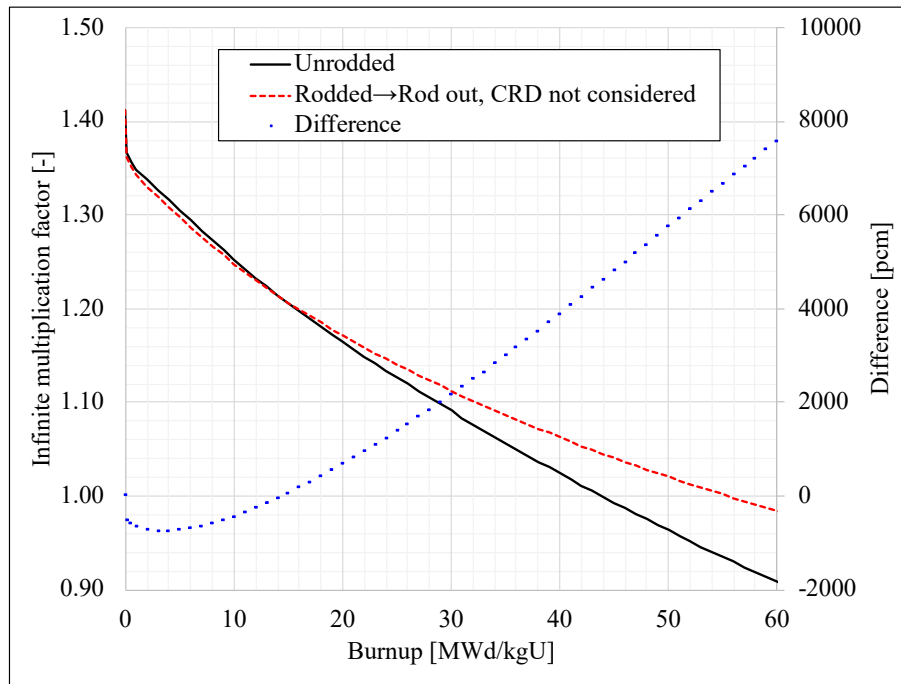


▪ Test description

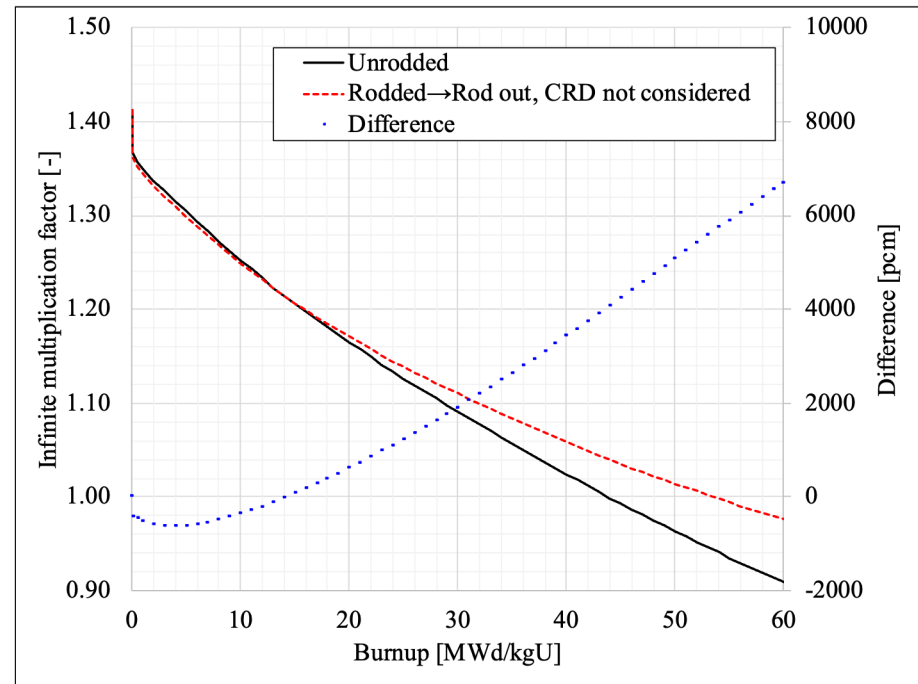
Index	Description
Test 1	Depletion of fuel under rodDED/unrodDED condition
Test 2	Depletion of fuel under rodDED condition (considering control rod depletion or not)

Test 1: Depletion of fuel under rodDED/unroDDed condition

- Case1: Depletion under unroDDed condition
- Case2: Depletion under roDDed condition → Rod withdrawn
 - Restart calculation (Snapshot at rod withdrawn state)
- Not considering depletion of control rod material
- Effect of depletion history



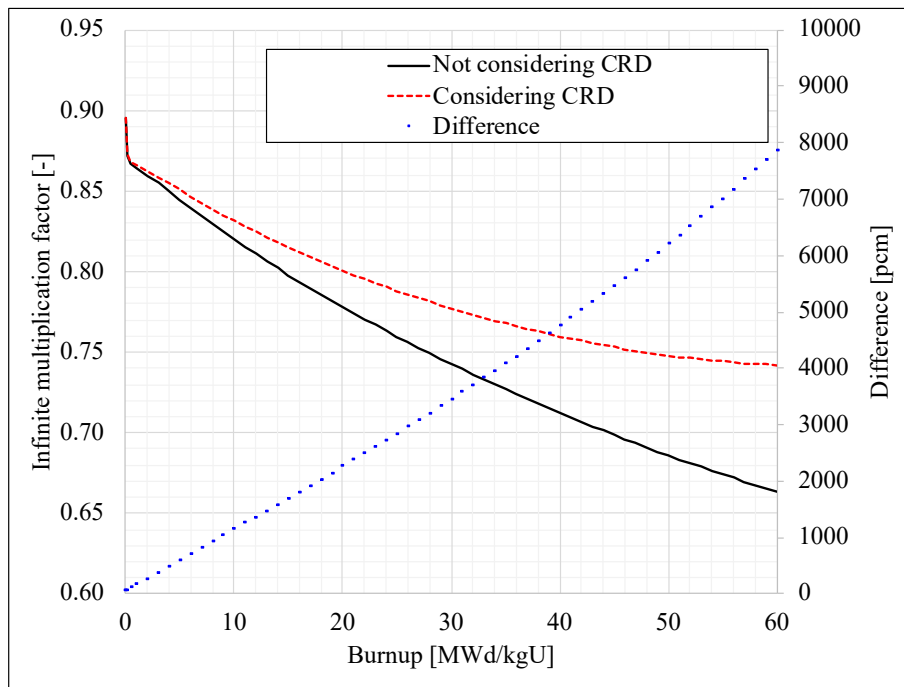
B4C Control rod



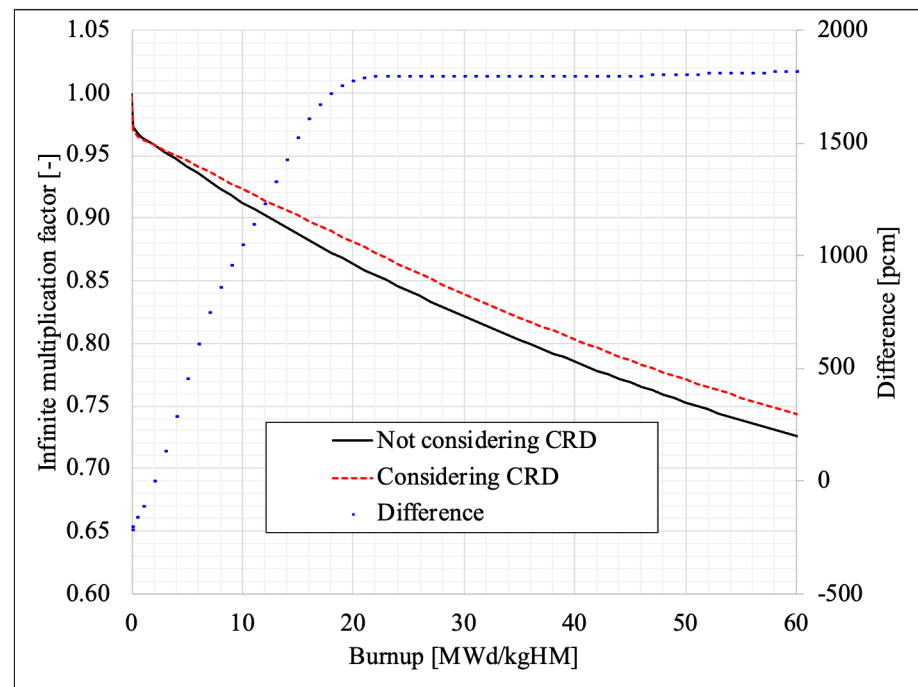
AIC control rod

Test 2: Depletion of fuel under rodded condition

- **Case1: Depletion under rodDED condition (not considering CRD)**
- **Case2: Depletion under rodDED condition (considering CRD)**
- **Effects of control rod depletion**
 - Number density decrease of control rod materials
 - RodDED history effect for both cases



B4C Control rod

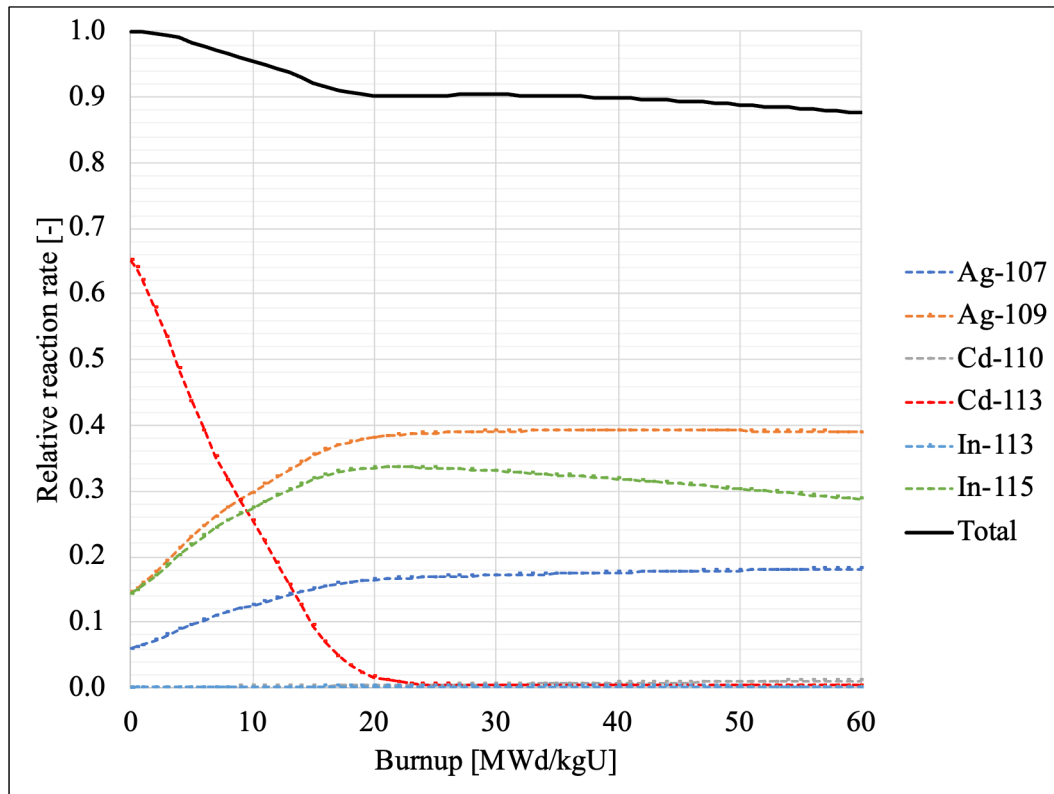


AIC control rod

Depletion of AIC

▪ Absorption reaction rate of AIC materials

- Rapid decrease of Cd-113's absorption reaction rate (~20 MWd/kgU)
 - Very high absorption cross section of Cd-113
- Gentle slope of degradation after the depletion of Cd-113



Isotope-wise relative absorption reaction rate

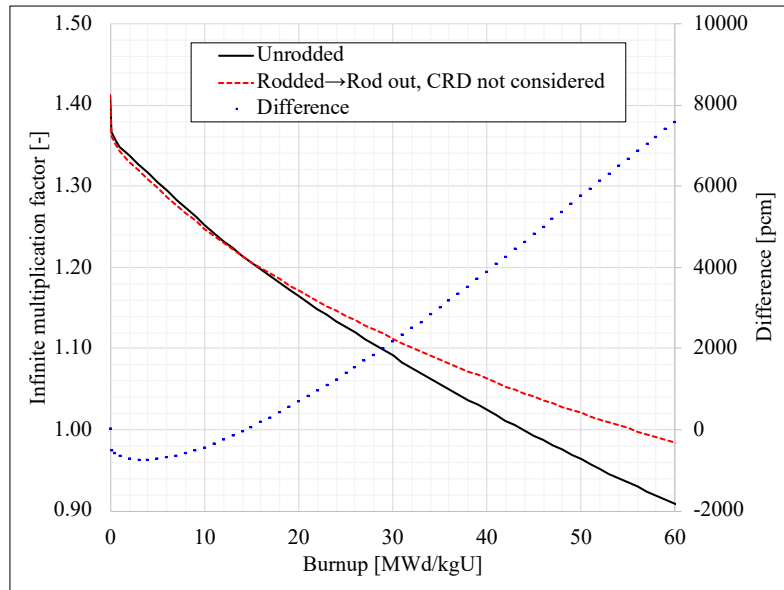
Summary: Effects of control rod inserted operation

▪ Effects on fuel (Test 1)

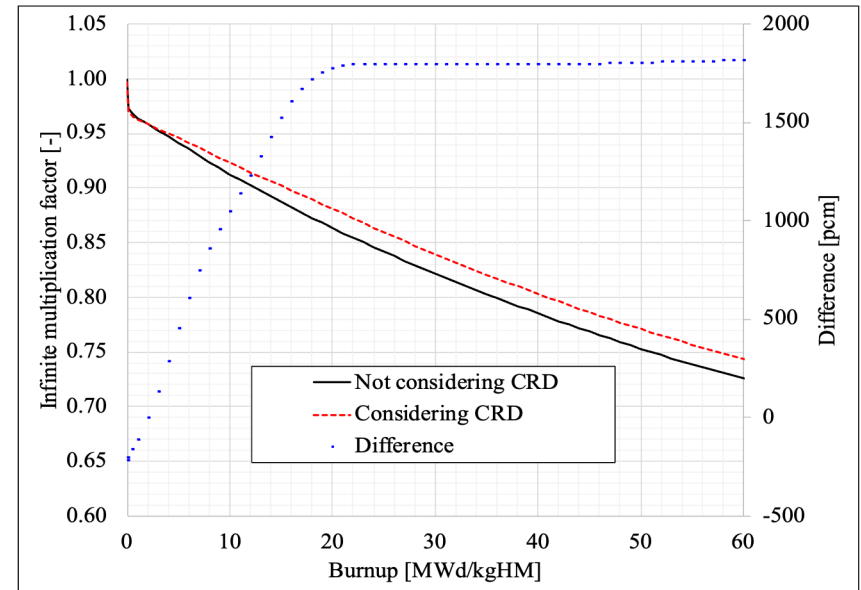
- Depletion behavior depends on the rodded history
 - Neutron spectrum hardening

▪ Effects on control rod (Test 2)

- Absorption reaction rate degradation
 - Control rod depletion



Test 1

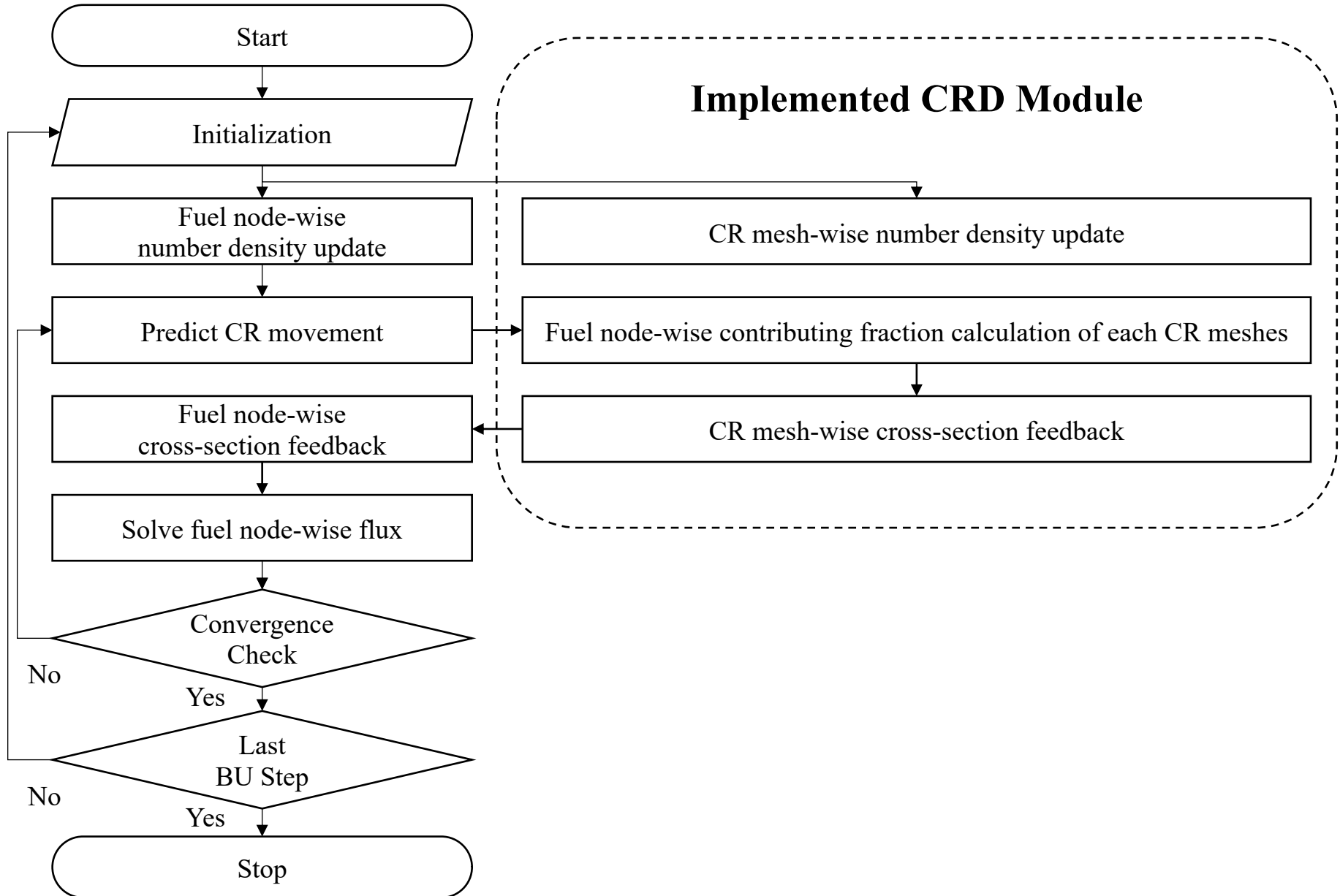


Test 2

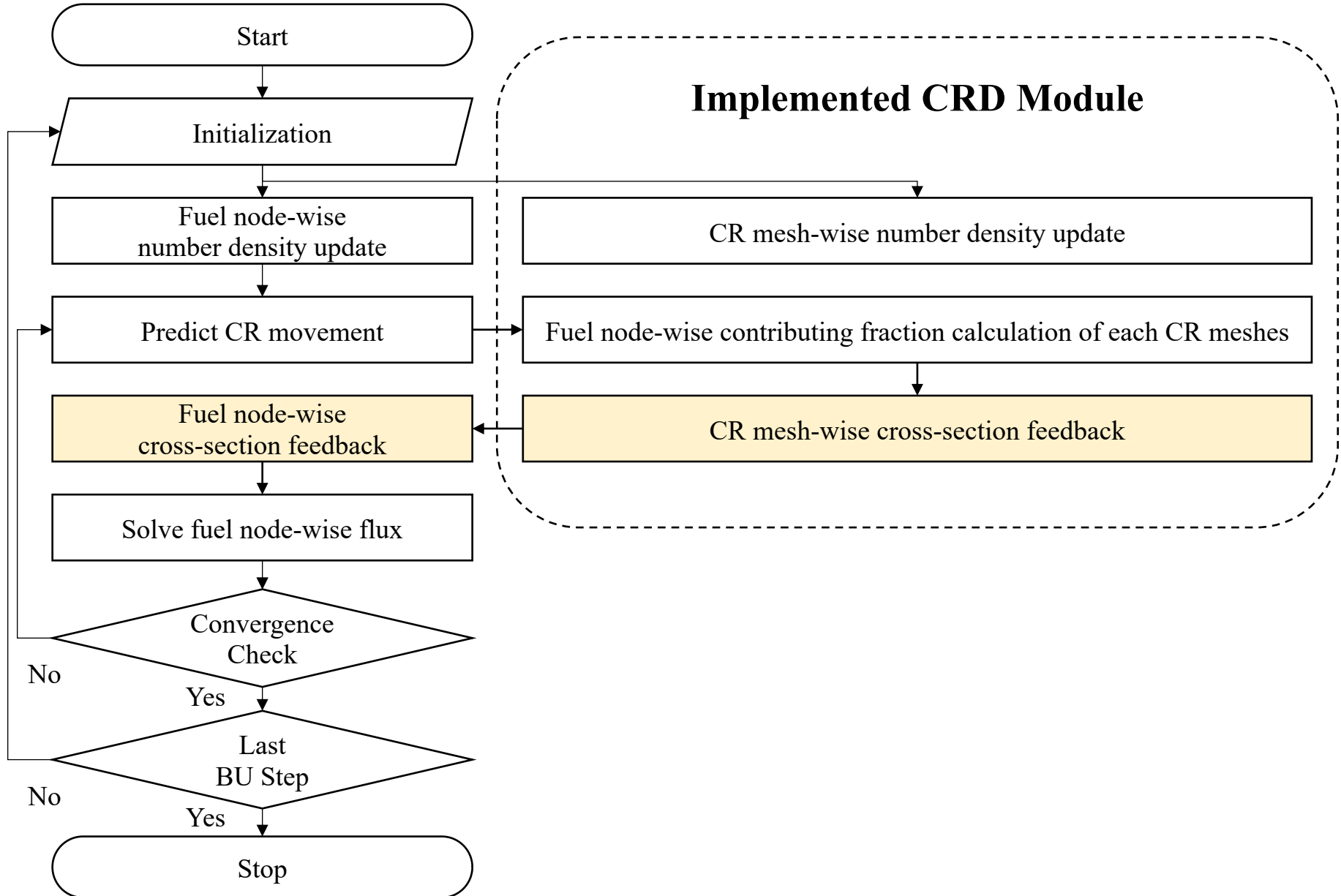
Control Rod Depletion Module



Flowchart of RAST-K



Flowchart of RAST-K



Cross section feedback

▪ Functionalized cross section model

$$\sigma = f\left(BU, \mathbf{PPM}, \sqrt{T_{fuel}}, T_{mod}, CR\right) \longrightarrow \sigma = f\left(BU, \sqrt{T_{fuel}}, T_{mod}, CR, \mathbf{CRDEP}\right)$$

- *BU* : Burnup
- *PPM* : Boron concentration
- T_{fuel} : Fuel temperature
- T_{mod} : Moderator temperature
- *CR* : Control rod
- *CRDEP* : Depleted fraction of control rod material
 - › Fresh, 1% burnt, 5% burnt, ...

▪ History dependent cross section feedback

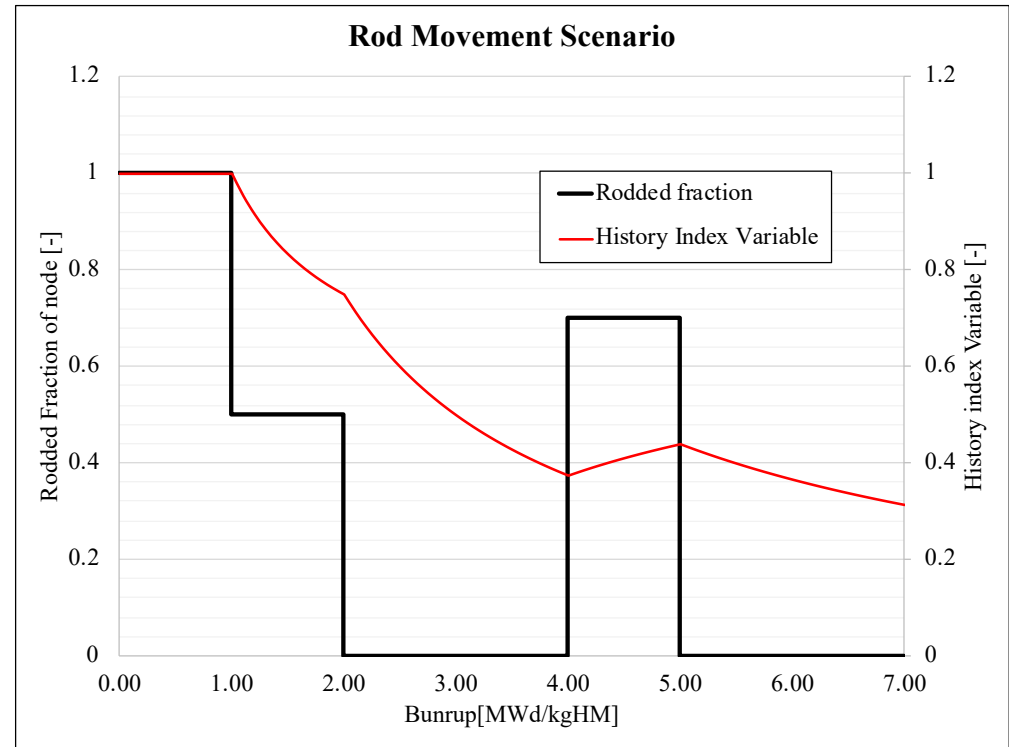
• Feedback cross sections having rodded/unrodded histories

- Σ_{Rodded} : Cross section following rodded history
- $\Sigma_{Unrodded}$: Cross section following unrodded history

History index variable

- Burnup weighted Rodded/Unrodded depletion fraction
 - Saves node-wise history

$$h = \frac{\sum_i^k (f_{Rodded}^i \cdot \Delta BU_i)}{\sum_i^k (\Delta BU_i)}$$



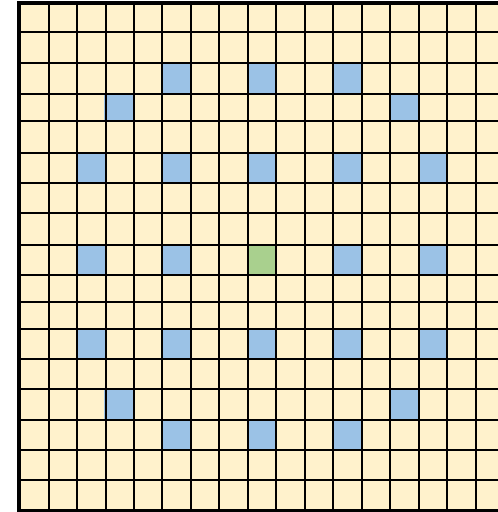
- Cross section feedback using the history index variable

$$\Sigma_{Node}^k = h \cdot \Sigma_{Rodded}^k + (1 - h) \cdot \Sigma_{Unrodded}^k$$

Test Case

▪ Test FA model

- 17x17 WH Fuel Assembly
- No burnable poison
- Boron concentration: 0 PPM
- Moderator Temperature: 600 K
- Fuel Temperature: 900 K
- Control rod material: AIC



▪ Test description

Index	Description
Test 3	Depletion under rodged condition
Test 4	Depletion under unrodged condition → rod insertion
Test 5	Depletion under rodged condition → rod withdrawal

Test 3: Prediction of depletion under rodded condition

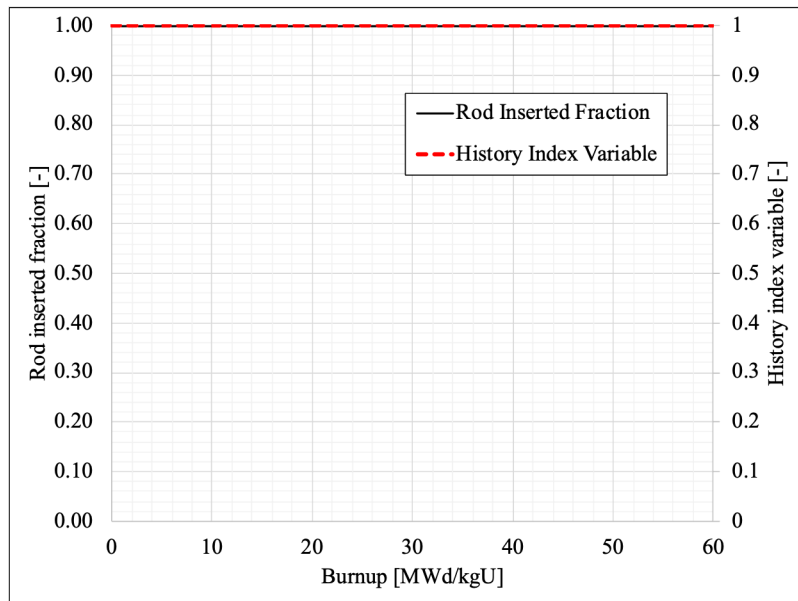
▪ Rodded condition (~ 60 MWd/kgU)

• Current method

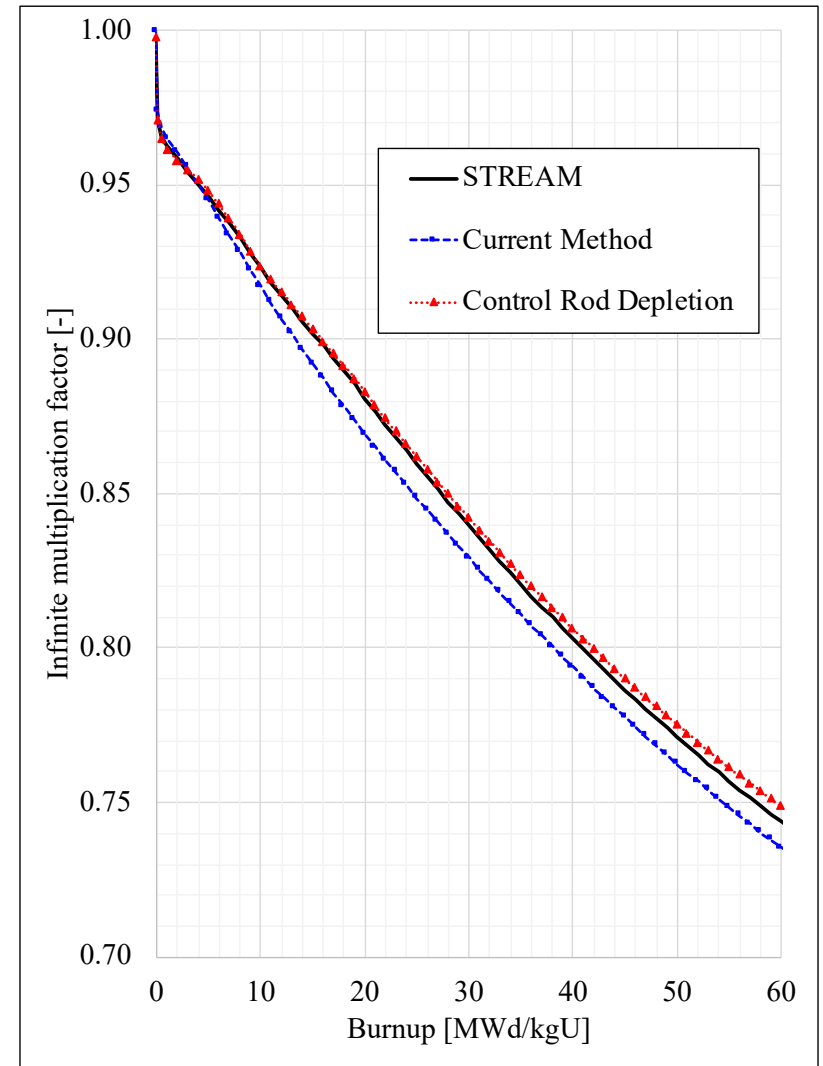
- Not considering control rod depletion
- Unrodded history based

• Control rod depletion

- Considering control rod depletion
- History follow calculation



Rod insertion history

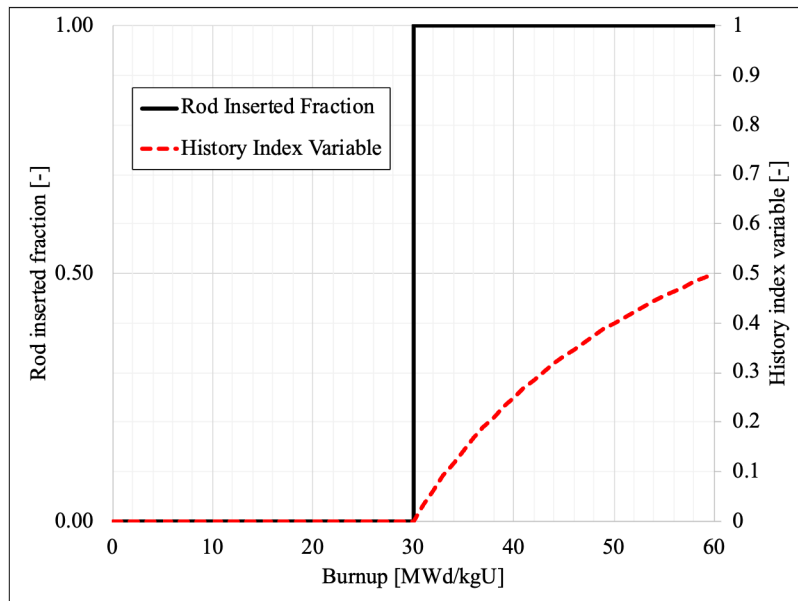


Infinite multiplication factor

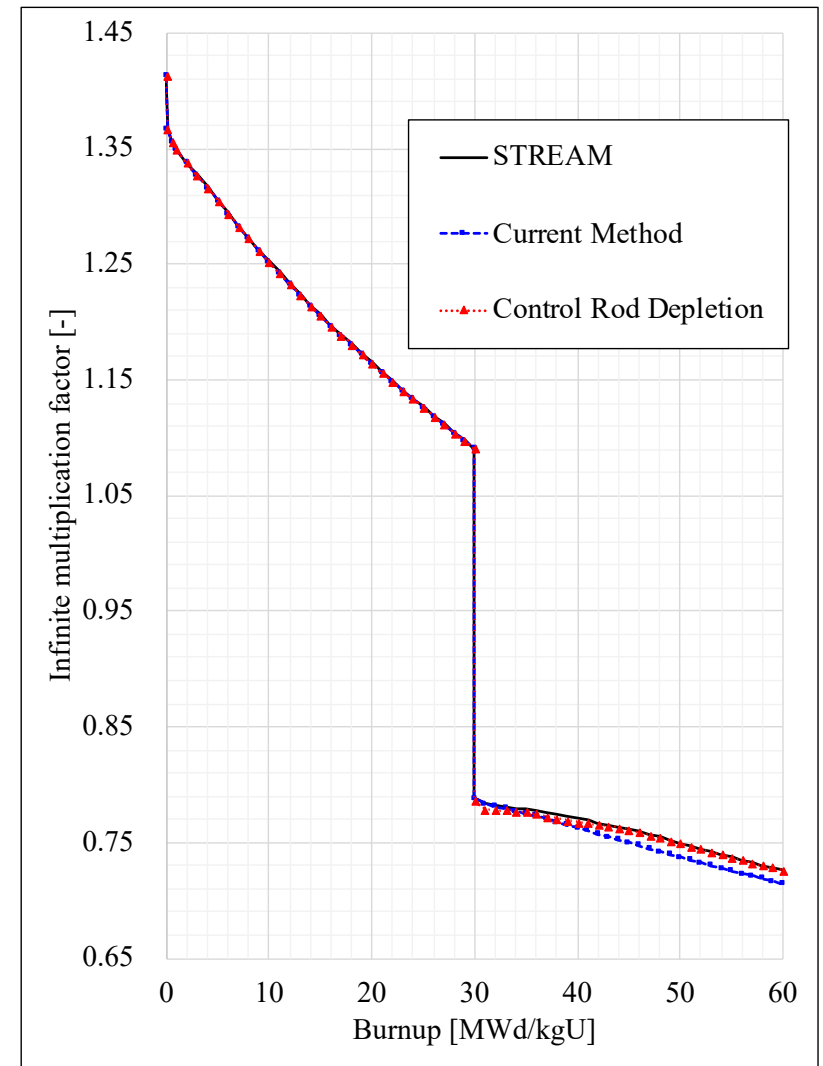
Test 4: Depletion under unrodded condition → rod insertion

Withdrawn → Rod insertion at 30 MWd/kgU

- Depletion until 30 MWd/kgU
 - No difference between two cases
- Rod insertion at 30 MWd/kgU
 - Gradually increasing history index variable
 - Current method: accumulation of error



Rod insertion history

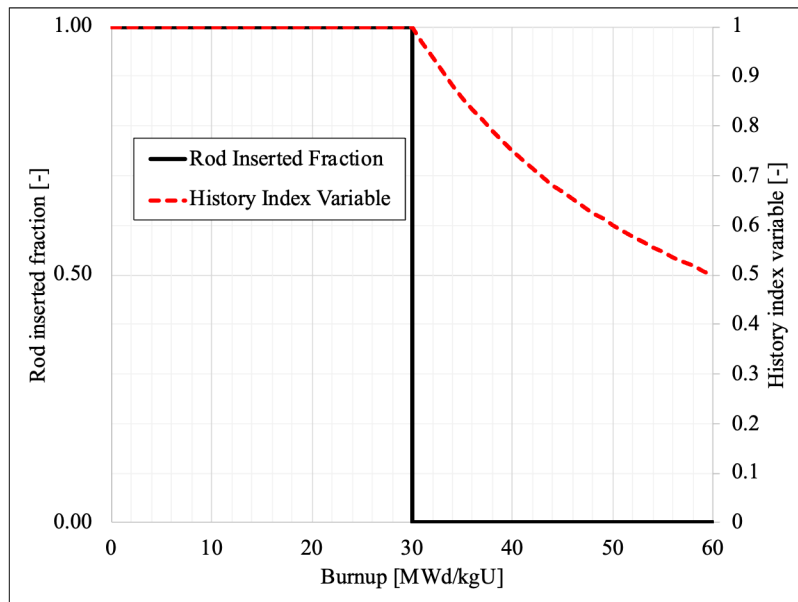


Infinite multiplication factor

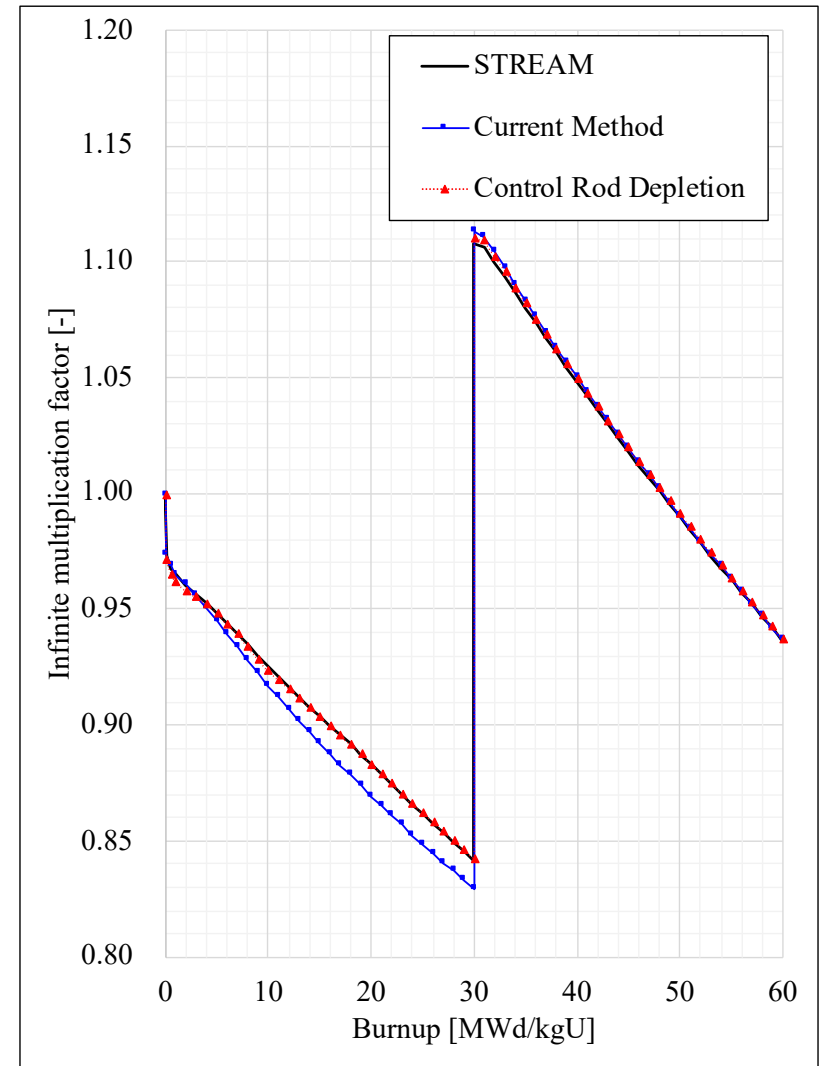
Test 5: Depletion under rodDED condition → rod withdrawal

■ Inserted → Rod withdrawal at 30 MWd/kgU

- Depletion until 30 MWd/kgU
 - Depletion under rodDED condition
 - Current method: error accumulation
- Rod insertion at 30 MWd/kgU
 - Gradually decreasing history index variable



Rod insertion history



Infinite multiplication factor

Depletion Analysis

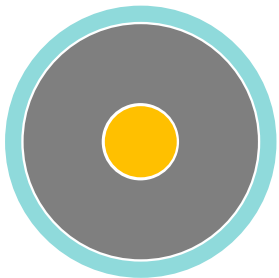
CIMBA-based i-SMR Fuel Assembly



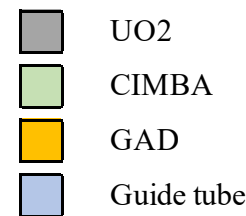
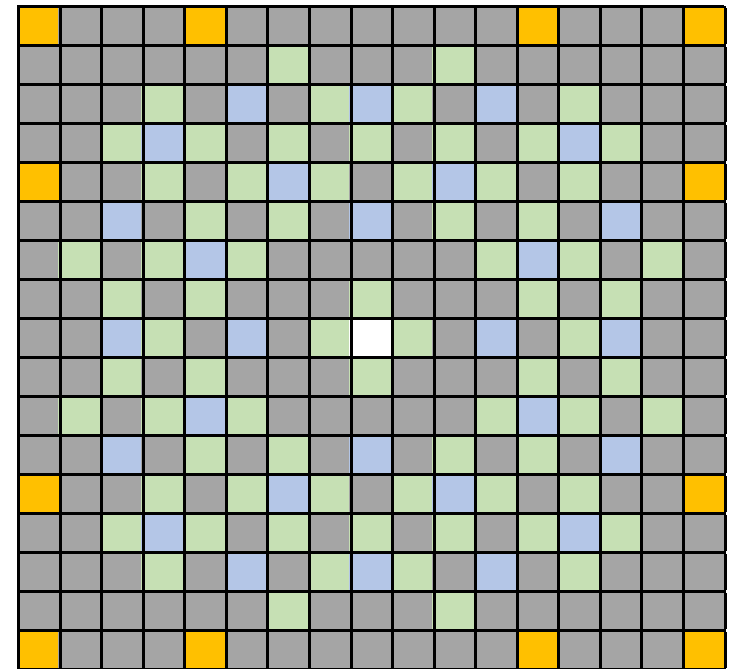
Test Case

▪ Test FA model

- **17x17 CIMBA Fuel Assembly**
- **Total number of fuel pin: 260**
 - UO₂ (Annular): 176
 - CIMBA pin: 72
 - GAD pin: 12
- **Number of guide tubes: 28**
- **Boron concentration: 0 PPM**
- **Fuel Temperature: 850 K**
- **Moderator Temperature: 584 K**

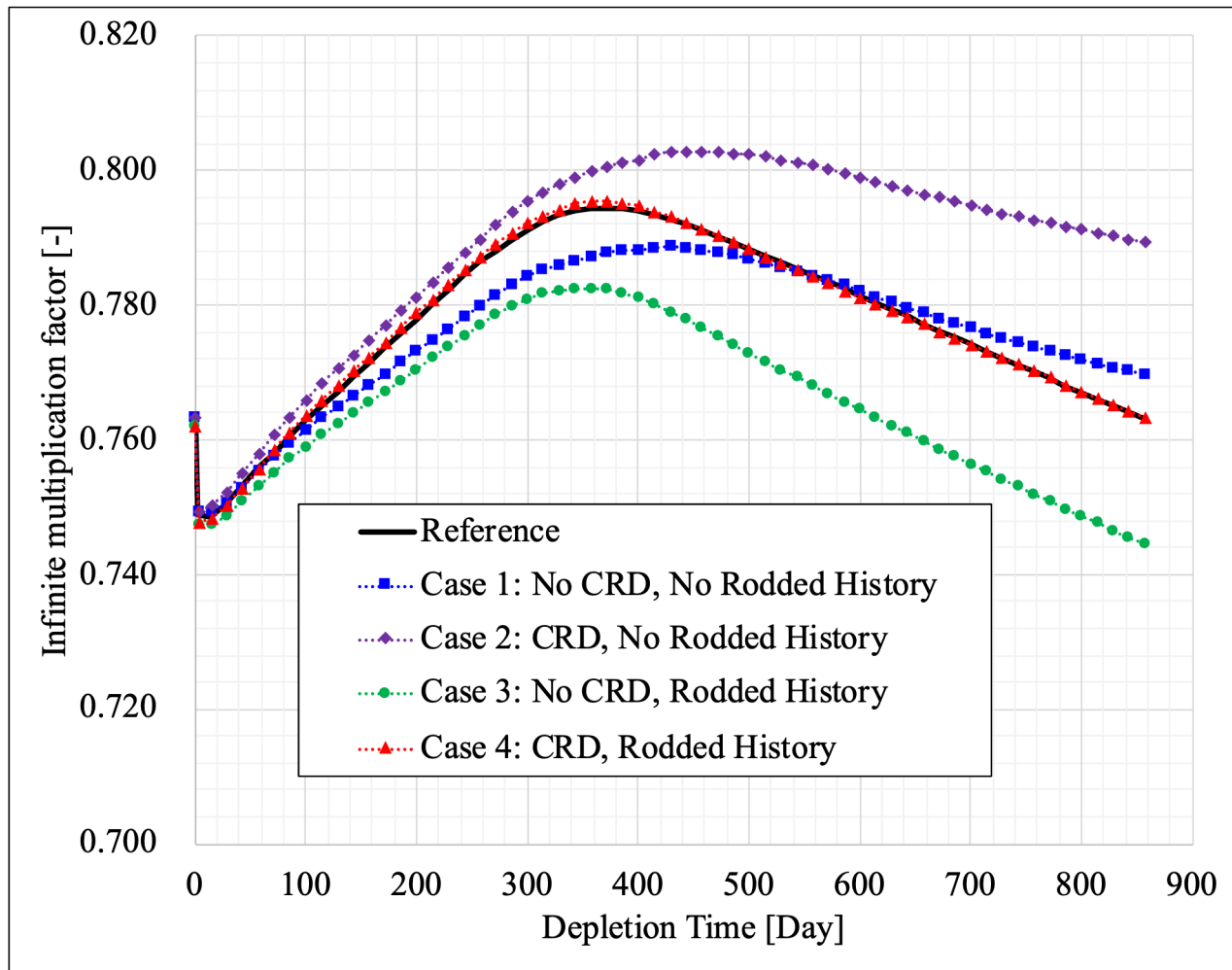


CIMBA pin: Annular UO₂ pin + Cylindrical BA



Depletion calculation of the i-SMR Fuel assembly

- Calculated k_{∞} of the rodded FA against burnup
 - Maximum error of Case 4: 109 pcm



Conclusion



Conclusion

- **Effects of control rod insertion**
 - **Depletion behavior under rodded condition**
 - Due to spectrum hardening
 - **Degradation of absorption strength**
 - Control rod depletion
- **Control rod depletion module in RAST-K**
 - **Cross section feedback**
 - considering control rod depletion
 - **History following**
 - History index variable, h and cross section feedback

$$h = \frac{\sum_i^k (f_{Rodded}^i \cdot \Delta BU_i)}{\sum_i^k (\Delta BU_i)}$$

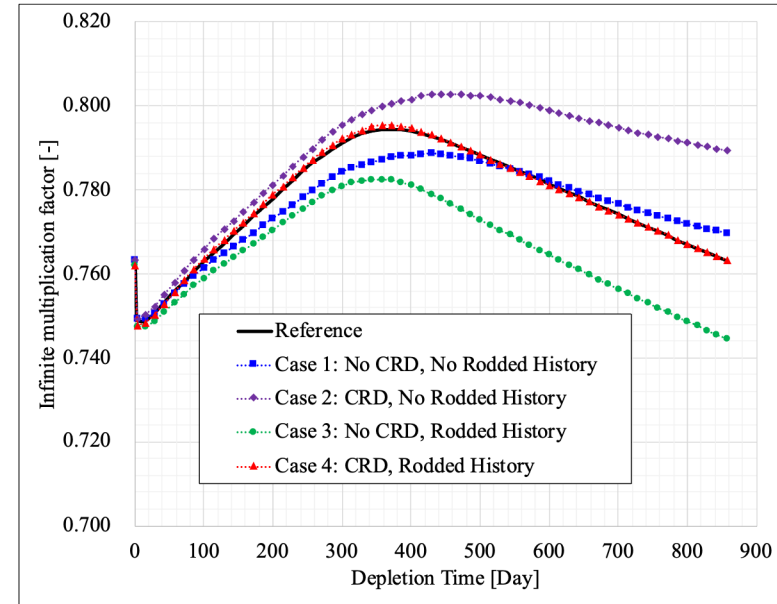
$$\Sigma_{Node}^k = h \cdot \Sigma_{Rodded}^k + (1 - h) \cdot \Sigma_{Unrodded}^k$$

Conclusion

- **i-SMR fuel assembly depletion analysis**
 - **Accurate infinite multiplication factor prediction**
 - Less than 109 pcm error

- **Ongoing works**

- **Detailed depletion history**
 - Depleted CR insertion
- **Axially heterogeneous cases**



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