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Preliminary Estimates of Nuclear Weapon Potential in North Korea's New ELWR

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- 2016년 – 2017년 (핵보유 시도)

- 4차 핵실험 (16.1월)
- 5차 핵실험 (16.9월)
- 6차 핵실험 및 ICBM 발사 (17.9월)

- 2018년 (북핵 일부 합의)

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- 평양공동선언 (9.19)

- 2019년

- 하노이, 제2차 북미정상회담 (2.27-28) -> **결렬**

- 2021년 이후, 영변 핵시설 재가동

북미협상: 북미 비핵화 실무협상에 엇갈린 양국 입장

2019년 10월 6일



REUTERS

북한대표단을 태운 차량이 미국과 회담장소인 스톡홀름 인근 리딩고 섬으로 향하고 있다

베트남 하노이 2차 정상회담 이후 약 7개월여 만에 열린 스웨덴 북-미 비핵화 실무협상이 사실상 결렬됐다.

앞서 북한 김명길 외무성 순회대사와 미국 스티븐 비건 국무부 대북특별대표가 각각 이끄는 북-미 협상단은 5일(현지 시간) 스웨덴 스톡홀름 북동쪽 리딩고 섬에서 비핵화 협상을 벌였다.

Figure 1. 북미협상 결렬^[1]

- The Nyongbyon nuclear scientific research center has the IRT-2000 research reactor, a 5 MWe reactor, and a 100 MWth reactor.



Figure 2. 북, 영변 주요 핵시설[2]

[2] 김지은 (Sep. 19, 2019). ““영구 폐기 뜻” 영변 핵시설, 북 핵개발의 심장”. 한겨레. <https://www.hani.co.kr/arti/politics/defense/862869.html>

- The Experimental Light Water Reactor (ELWR) was recently constructed at the Nyongbyon site in the 2010s.



Figure 3. Development of pipelines at the ELWR from 2010 to 2013^[3]

[3] Sulgiye Park and Allison Puccioni (Jan. 24, 2024). "North Korea's Pursuit of an ELWR: Potential Power in Nuclear Ambitions?". 38NORTH. <https://www.38north.org/2024/01/north-koreas-pursuit-of-an-elwr-potential-power-in-nuclear-ambitions/>

- This new ELWR reportedly began operations in October 2023.

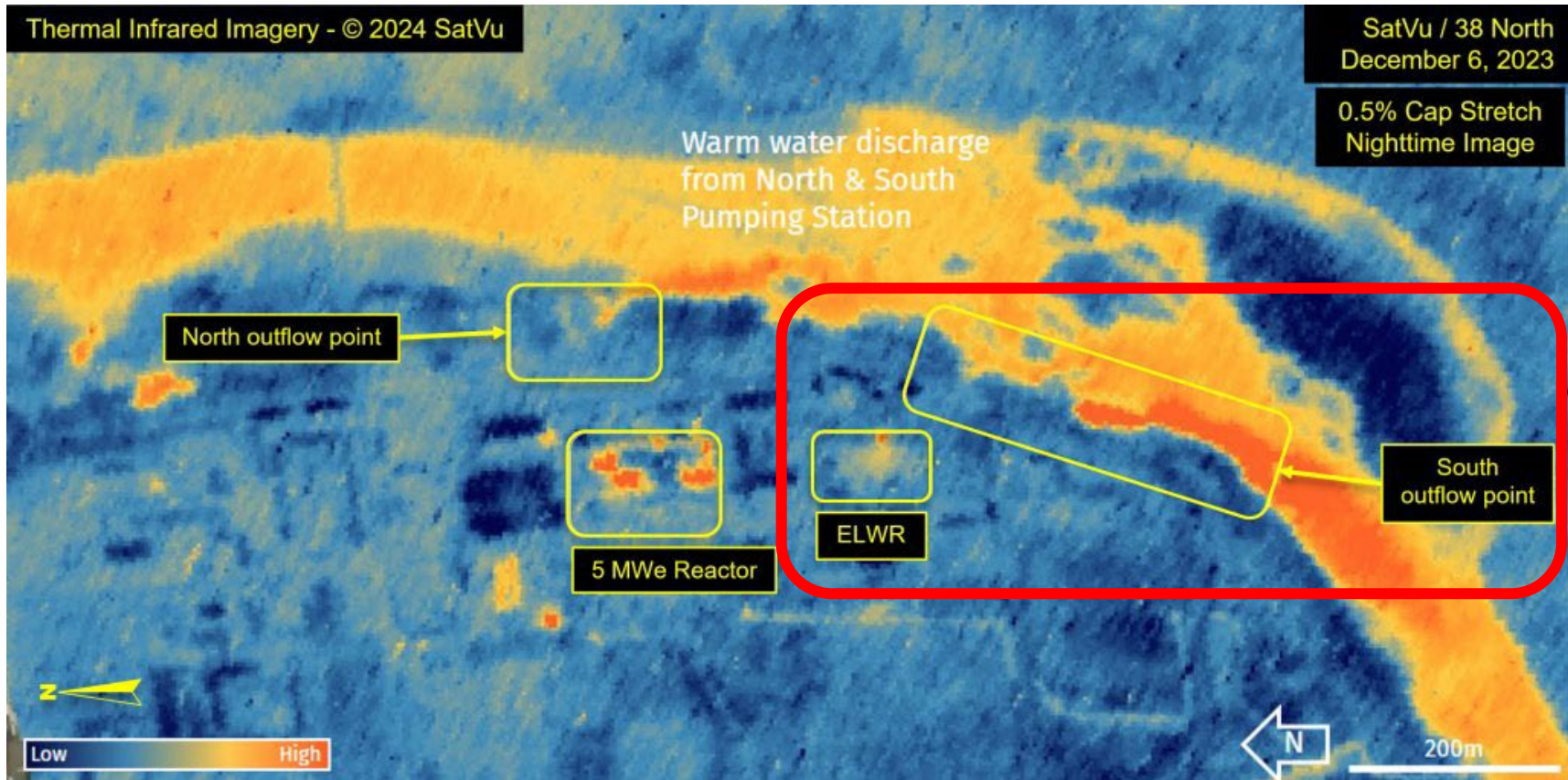


Figure 3. Thermal image over Yongbyon Nuclear Scientific Research Center from
October, 2023.
Blue (lower heat) -> Red (higher heat)^[3]

• The 5 Megawatt-electric Reactor

- Power: 25 MWth
- **Type: Magnox (Graphite-moderated gas-cooled reactor)**
- Fuel: 50 tons, metallic natural-uranium (^{235}U 0.72 wt%)
- From 1986, producing Weapon-Grade Plutonium

Table I: Operation history of 5 MWe Reactor and WG-Pu production estimations^[4]

Operation and shutdown	Residence; avg. burnup	Amount.Spent fuel Removed	Reprocess Duration	Separated WG-Pu
Op. 1986–1989 Shutdown 1989 (70–100 days)	3 years (Unknown)	Unknown	Unknown	Less than or equal to 2 kg
Op. 1989–1994 Shutdown 1994	Unknown (~650 MWd/t)	Full core: 50 tons U	2003.01–06	20–30 kg
Op. 2003–2005 Shutdown 2005 (~70 days)	2 years (330 MWd/t)	Full core	2005.06–12	10–14 kg
Op. 2005–2007 Shutdown July 2007	1+ year (Less than 200 MWd/t)	Full core	2009	~8 kg
Op. 2013–2015 Shutdown 2015	2 years (intermittent: Uncertain burnup)	Likely full core	2016	5.5–8 kg

Op. 2016

In Reactor

total 45 ~ 62 kg

- **The new Experimental Light-Water Reactor**

- Power: 100 MWth
- **Type: VVER-440 (Russia's PWR using hexagonal fuel bundles)**
- Fuel: 4 tons, 3.5 wt% enriched UO_2 ^[5]
- Constructed since 2010 & Tested the cooling water system (July 2022)
- Begun operating since **October 2023**



Figure 4. A significant amount of water discharge from the ELWR
(Left: **October 4, 2023** / Right: **December 10, 2023**)^[6]

[5] Hecker S.S. (Dec. 20, 2010). "Redefining denuclearization in North Korea". Bulletin of the Atomic Scientists. <https://thebulletin.org/2010/12/redefining-denuclearization-in-north-korea-2/>

[6] David Albright (Jan, 2024). North Korea's ELWR: Finally Operational After a Long Delay. ISIS report

- **Oak Ridge Isotope GENERation (ORIGEN) module in SCALE code**
 - **Point-depletion (0-D) code** that calculate time-dependent concentrations, activities, and radiation source terms for a large number of isotopes simultaneously generated or depleted by neutron transmutation, fission, and radioactive decay
 - Neutron spectrum-dependent libraries are created from interpolation of existing reactor libraries in SCALE code, using Automated Rapid Processing (**ARP**) module.
 - Depletion calculations are used the Chebyshev Rational Approximation Method (CRAM) in solving the Bateman equation.
 - For post-processing, **OPUS** module shows calculated isotopics and spectra to be sorted, ranked, and converted to other units.

- Weapon-Grade Plutonium (**WG-Pu**) estimation
- WG-Pu is defined as plutonium with a high content of the fissile isotope (^{239}Pu)
- **Pu quality** =
$$\frac{\text{fissile Pu isotopes mass } (^{239}\text{Pu})}{\text{total Pu isotopes mass (total Pu)}} \geq 93 \text{ wt}\%$$
- The Pu quality monotonically decreases due to the preferential fission reactions of ^{239}Pu .

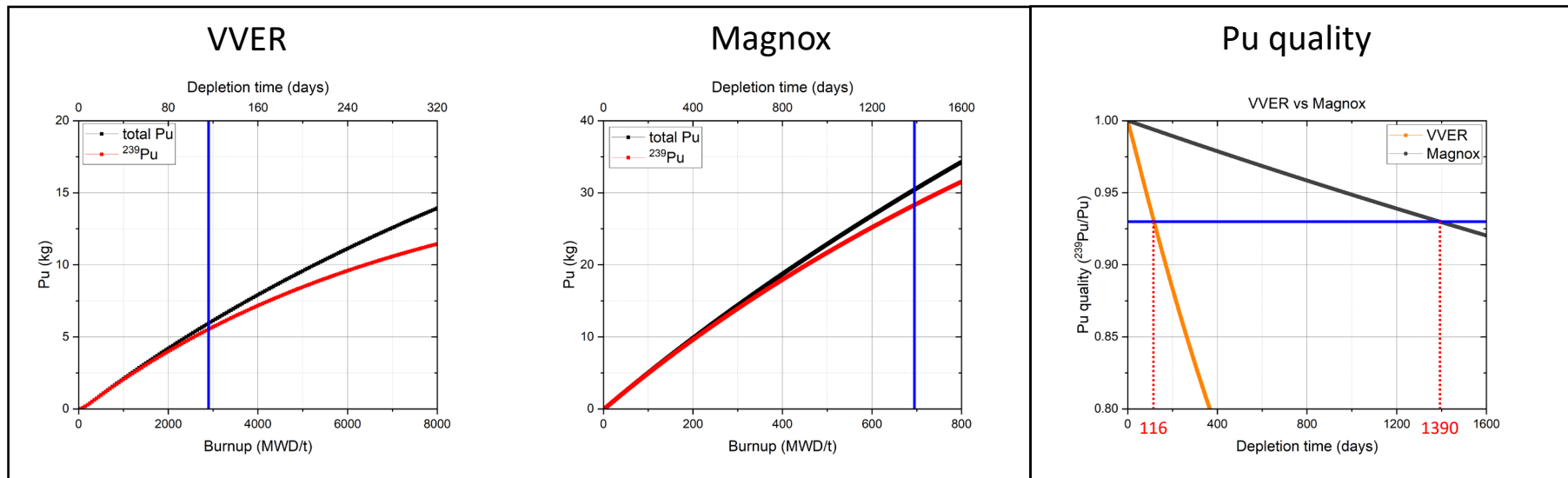


Figure 5. Comparison of plutonium production and quality over depletion by reactor types (Left: VVER / Middle: Magnox / Right: Pu quality)

- **Depletion time**

- VVER: 116 days
- Magnox: 1390 days

- **Burnup**

- VVER: 2900 MWd/tU
- Magnox: 695 MWd/tU

- **Pu production**

- VVER: 5.94 kg
- Magnox: 30.4 kg

- **Grams of WG-Pu per MWd**

- VVER: 0.512 g/MWd
- Magnox: 0.876 g/MWd

Table II: Plutonium Production and Weapon Potential

	VVER	Magnox
Thermal power (MWt)	100	25
Initial mass of uranium (tons)	4	50
Depletion time at which Pu quality becomes 93 wt% (days)	116	1390
Burnup (MWd/tU)	2900	695
WG-Pu production (kg)	5.94	30.4
Grams of WG-Pu per MWd (gPu/MWd)	0.512	0.876
Separated WG-Pu (kg)	3.74 ~ 4.28	19.2 ~ 21.9
Annual WG-Pu production (kg/year)	11.8 ~ 13.5	5.04 ~ 5.75
Number of nuclear weapon potentials (number/year)	2.95 ~ 4.49	1.26 ~ 1.92

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If North Korea decided to use the LWR as a source of weapon-grade plutonium for weapons, it could grow its nuclear weapons arsenal significantly by using a driver fuel/target system. Slated to be 100 MWth, or four to five times larger than the existing Yongbyon reactor, the LWR could produce roughly 20 kilograms of weapon-grade plutonium per year.¹⁷ At 3-4 kilograms of plutonium per weapon, twenty kilograms is enough for 5-6 nuclear weapons per year. The actual annual amount of weapon-grade plutonium could vary significantly, depending on the reactor's actual performance.

¹⁷ ISIS did not perform detailed calculations but a rough estimate was conducted with the support of a reactor expert who was familiar with the use of driver fuel/target systems in reactors. The estimate assumes a 70-80 percent capacity factor, a conversion of 0.85 grams of weapon-grade plutonium per megawatt-thermal-days and an estimated 10 percent reduction in plutonium output to account for the plutonium produced in the driver fuel, which is not usable. The resulting estimate is 19.5-22.3 kg weapon-grade plutonium per year. To assess enrichment requirements, the nuclear reactor expert said that a rule of thumb is that a core composed of 10-20 percent LEU driver fuel would have the same amount of uranium 235 as a core of 3.5 percent LEU fuel.

Figure 6. Institute for Science and International Security report^[7]

- ***Separated Pu**
 - VVER: 3.74 ~ 4.28 kg
 - Magnox: 19.2 ~ 21.9 kg
- ****Annular Pu production**
 - VVER: 11.8 ~ 13.5 kg/year
 - Magnox: 5.04 ~ 5.75 kg/year
- *****Number of nuclear weapon potentials**
 - VVER: 2.95 ~ 4.49 #/year
 - Magnox: 1.26 ~ 1.92 #/year

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* Pu production \times Capacity factor (70 ~ 80 %) \times Reduction in output (10 %)

** Separated Pu \times 365 days \div Depletion time

*** Annular Pu \div (3~4 kg Pu per weapon)

• Plutonium production vs depletion time

- At **one operation**, the Magnox has a more Pu production than the VVER.
- During **the same operation time**, the VVER has a higher Pu production rate than the Magnox. (~130 % higher)

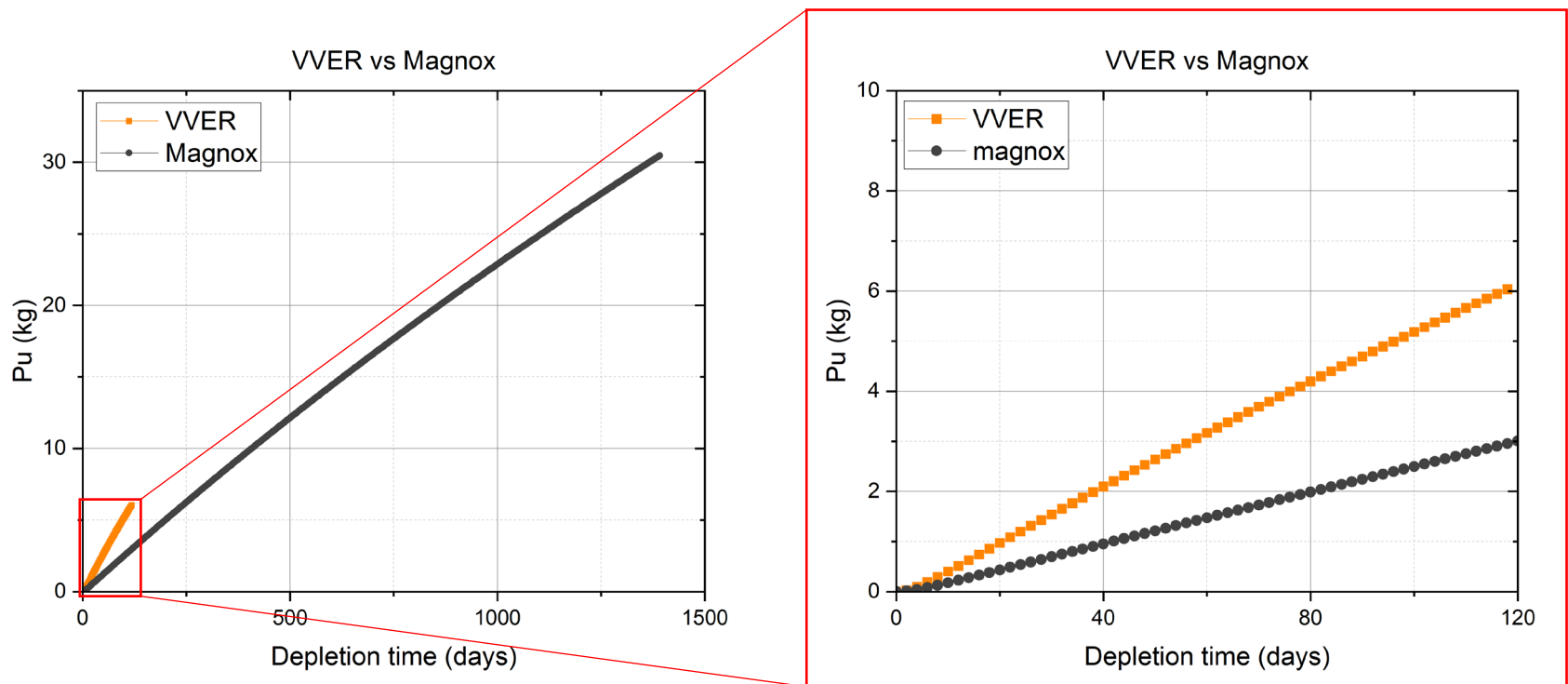
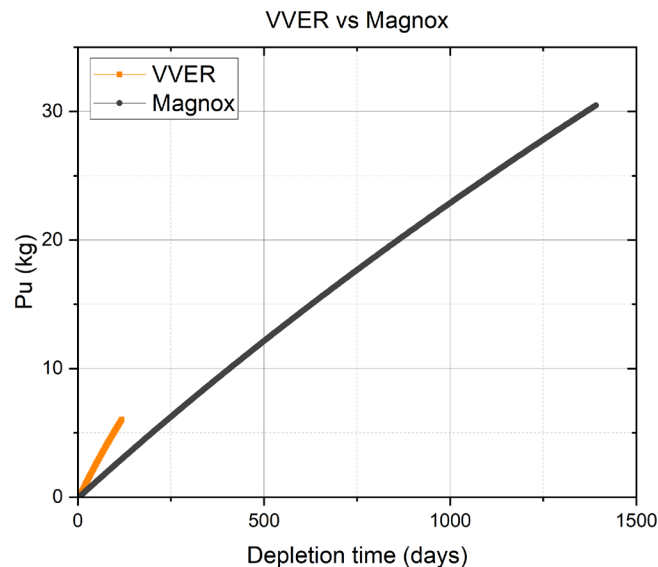


Figure 7. Comparison of plutonium production over depletion time by reactor types

- The construction of a new Experimental Light Water Reactor (ELWR) by North Korea continues to pose a significant nuclear proliferation threat.
- In this work, the plutonium production capacity for this ELWR was estimated, assuming it is based on the Russian VVER reactor design.
- It was estimated that North Korea's existing **Magnox-type reactor can produce 1.26 to 1.92 nuclear weapons per year**, while **the ELWR can produce 2.95 to 4.49 nuclear weapons per year**.
- This result undervalues from the estimation provided in the ISIS report.



	ELWR	5 MWe reactor
Reactor power (MWth)	100	25
Initial uranium mass (tons)	4	50
Grams of WG-Pu per MWd (gPu/MWd)	0.512	0.876
Number of nuclear weapon potentials (number/year)	2.95 ~ 4.49	1.26 ~ 1.92
ISIS's estimation (number/year)	5 ~ 6	

• Limitations

- Light Water Reactors (LWRs) are generally not well-suited for plutonium production.

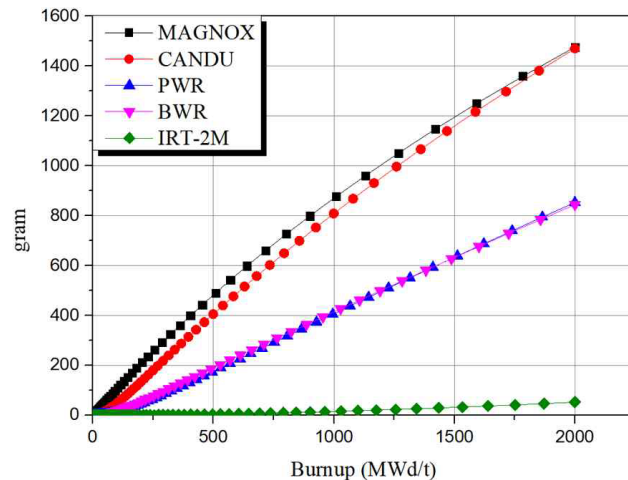


Figure 8. Pu production over burnup per initial uranium ton by reactor types^[8]

Pyongyang's desire for nuclear electricity with LWRs is likely genuine since it has pursued acquisition of LWRs since 1985, first from the Soviet Union, then from the United States, and now on its own. Though it is technically possible that the LWR will be used to produce bomb-grade plutonium, I consider it unlikely because North Korea's existing gas-graphite reactor is more suitable for the production of bomb materials than Pyongyang's LWR.

<Siegfried S. Hecker. (December 20, 2010). "Redefining denuclearization in North Korea", Bulletin of the Atomic Scientists>

• Future works

- This work focused on point-depletion calculations and did not consider neutron leakage and operational periods.
- Incorporating 3D modeling will be needed to attain more accurate results, which may lower the estimated WG-plutonium production capacity.
- Accounting for reactor cooling periods will also be necessary.

Future work (Doing)

• 3D Modeling

- We are using Monte-Carlo code **Serpent2** for full-core 3D analysis.

2-D Fuel bundle

3-D Whole core

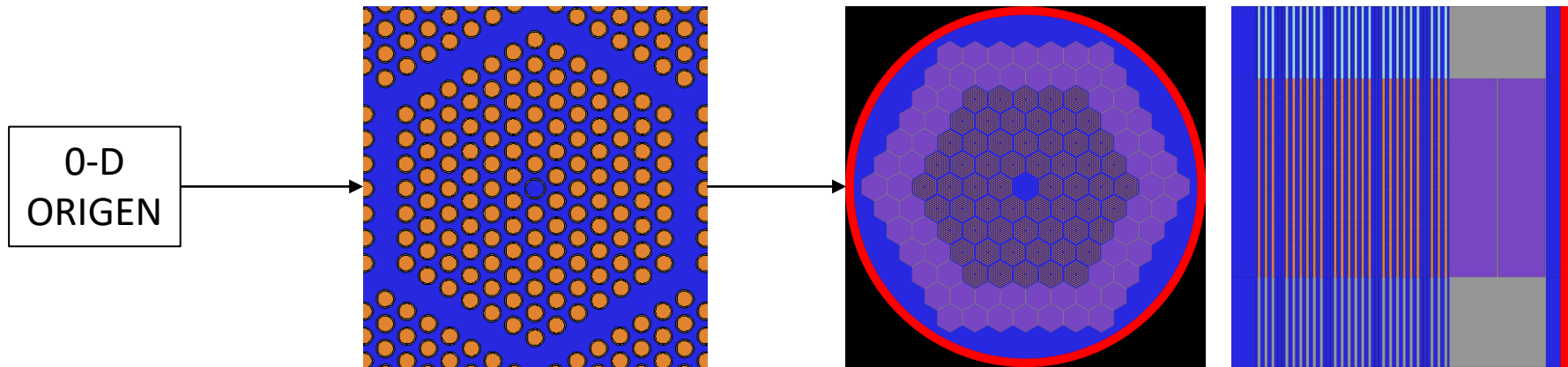


TABLE 2.1.1.1. VVER-440 DESIGN PARAMETERS

TABLE 2.1.1.1. (cont.)

Core description		Fuel type	w/o (given value)
Rated thermal power	1375 MW	Enrichment	
Rated electrical power	440 MW	Geometry (including all supporting elements and enrichments of particular fuel rods)	Fig. 2.1.1.3
Specific power density	84.4 W/cm ²	Number of fuel rods	126
		Total mass of UO ₂ per FA	136 kg (119.75 kg U metal)
Coolant:		Lattice pitch	1.22 cm
Pressure at core inlet	1225.83 N/cm ²	Spacer grid:	
Net core flow	43000 m ³ /h	Material	12X18H10T stainless-steel
HFP inlet temperature	269°C	Density	7.86 g/cm ³
HFP average core outlet temperature	300°C	Number, location, axial dimensions, mass or volume fractions of materials in one spacer grid	Fig. 2.1.1.4
HFP average fuel cladding temperature	302°C	Mass of one spacer grid	0.118 kg
HFP average fuel temperature	707°C	Instrumentation tubes:	
Core:		Material	Z110 - 1%Nb zirconium alloy
Total fuel loading in the core	47 000 kg UO ₂ , 42 000 kg U in Fig. 2.1.1.1	Density	6.52 g/cm ³
Geometry		Outer radius	0.515 cm
Number of fuel batches for initial core	3	Thickness	0.075 cm
Number and type of fuel assemblies in each batch	114, 133, 102, 1.6%; 2.4%; 3	Location in core	in the center of FA
Enrichment of each type of fuel assembly		Fuel rod	
Loading pattern for initial core showing position of each type fuel assembly	Fig. 2.1.1.2	Cladding:	
Effective core radius	144 cm	Material	Z110 - 1%Nb zirconium alloy
Reload pattern		Density	6.52 g/cm ³
Location of control assemblies	Fig. 2.1.1.2	Outer radius	0.455 cm
Identification of control assemblies or rod groups used for control and shut down.	6	Inner radius	0.386 cm
Reflector		Pellet:	
Geometry		Material	UO ₂
Water temperature	Fig. 2.1.1.1	Percent of theoretical density x density	0.95x10.2 g/cm ³
Water pressure	1225.83 N/cm ²	Outer Radius	0.3800±0.0025 cm
Material of core basket (thermal shield)	08X18H10T	Average mass of pellet	13.17 g UO ₂ (11.59 g metal)
Thickness of core basket		Height	3cm
Specification of other components (core barrel)	08X18H10T	Number in fuel rod	82
Fuel assembly data		Height of UO ₂ (HFP)	246 cm
The following information is valid for each type of fuel assembly (FA):		Initial He pressure, if any	~ 0.15 MPa
General		Mass of UO ₂ per fuel rod in a fuel assembly	1080 g
Fuel assembly pitch	14.7 cm	Mass of UO ₂ per fuel rod in a control assembly	1035 g
Gap between assemblies	0.3 cm		
Shell material	Zirconium allo (Z125- 2.5%N		
Shell thickness	0.2 cm		

TABLE 2.1.1.1. (cont.)

Control Assembly						
Geometry:						
in radial plane (cross section of control absorber)		Fig. 2.1.1.5				
in axial plane		Fig. 2.1.1.6				
Absorber						
Density		boron steel				
		7.51 g/cm ³				
Compositions of steel and boron steel						
Material	Weight per cent				Nominal density	
	Fe	Ni	Cr	Mn	B	g/cm ³
Steel	70.5	10	18	1.5	-	7.86
Boron Steel	69.2	9.8	17.7	1.5	1.9	7.51
Compositions of zirconium alloy						
Material	Weight per cent					
	Zr	Nb	Hf			
Z110	98.97	1.0	0.03			
Z125	99.47	2.5	0.03			

Figure 9. VVER-440 Design parameters^[9]

• 3D Modeling

- We aim for the **similar R/H** of the active core and **linear heat densities**.
- Rod number per bundle, rod diameter, rod pitch, and bundle pitch are same.
- To achieve the similar R/H, the number of fuel bundle is determined while the same number of fuel rods per bundle.
- Considering the similar R/H and linear heat density simultaneously, the active core height are decided.

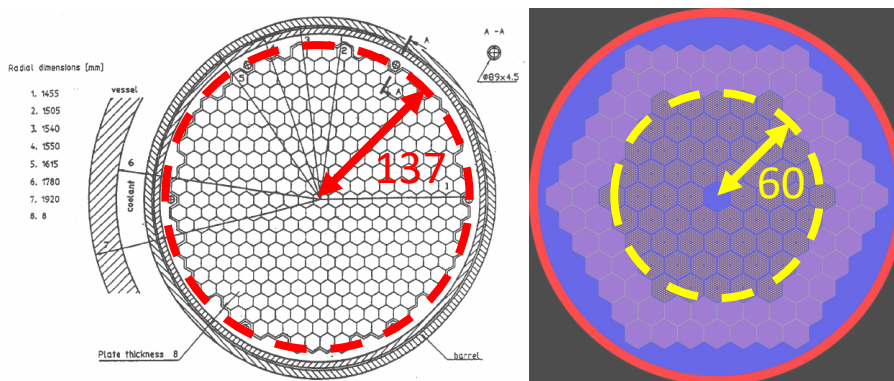


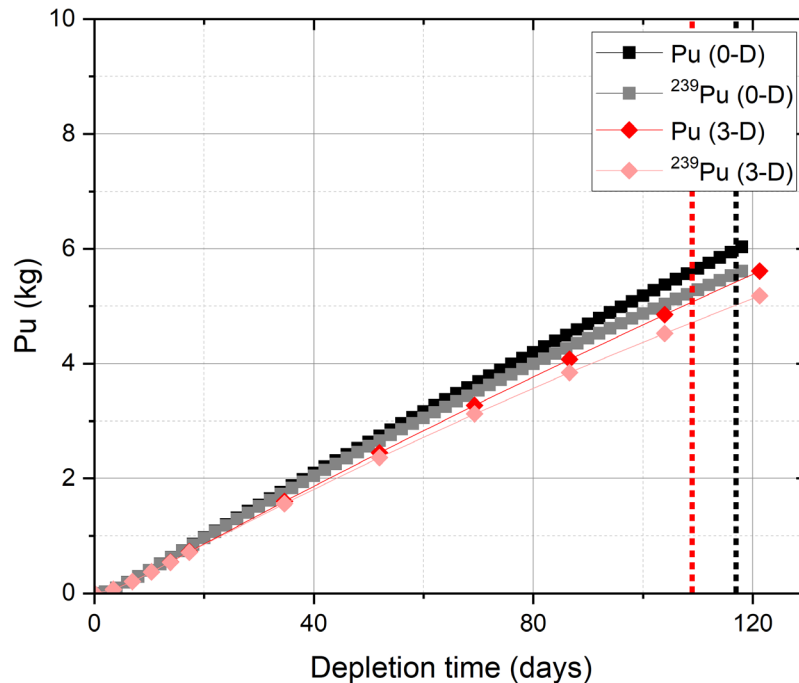
Figure 10. Core configurations of VVER-440^[9] and ELWR
(Left: VVER-440 / Right: ELWR)

Table III: Design parameters of the VVER-440 and ELWR

	VVER-440	ELWR
Thermal power (MWt)	1375	100
Initial uranium mass (tons)	~ 37	3.93
Rod number per bundle	126	126
Number of fuel bundles	312	60
Active core radius (cm)	137	60
Active core height (cm)	246	110
Radius/Height of core	0.555	0.548
Linear heat density (W/cm)	142	120

• 0-D vs 3-D calculations

- Due to the more computational cost of the 3-D calculation compared to 0-D depletion calculation, the 3-D calculation was performed with a longer depletion time step.
- The 3-D calculations result in a smaller amount of plutonium (Pu) production, with approximately a **15.3% difference** compared to the 0-D calculations.



Pu quality = 93 wt%	0-D ORIGEN	3-D Serpent
Depletion time (days)	117	109
Pu production (kg)	6.006	5.086
Number of nuclear weapon potentials (number/year)	2.95 ~ 4.49	2.68 ~ 4.08

Figure 11. Comparison of plutonium production over depletion time by calculation types



Thank you for listening
