

## Synthesis of Alternative Y<sub>2</sub>O<sub>3</sub>-based High-temperature Material for Melting Crucible of Metal Fuel

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### 1. Introduction

The transuranic(TRU) element is used to fabricate metal fuels for Sodium-cooled Fast Reactors(SFRs) [1-3]. U-TRU-Zr-RE metal fuel slugs have been fabricated with an injection casting process operating under atmospheric pressure [4-5]. RE is composed of rare-earth elements consisting of 53wt.% Nd, 25wt.% Ce, 16wt.% Pr, and 6wt.% La. Since highly reactive RE is included during the pyro-processing process, even the plasma-spray coated Y<sub>2</sub>O<sub>3</sub> layer on the melting crucible is reacted with RE in the metal fuel and forms the reaction products of RE-Y-O system, which produces a considerable amount of fuel loss and a large amount of radioactive crucible waste. It is necessary to develop an alternative reaction-resistant crucible material that prevents high reactivity with fuel melt to control the fuel loss and reduce the radioactive waste. Alternative Y<sub>2</sub>O<sub>3</sub>-based crucible material, is of interest as a potential candidate for thermal barrier coating in highly refractory materials due to its chemical and thermal stability [6].

In this study, Y<sub>2</sub>O<sub>3</sub>-based high-temperature ceramic material was introduced as an alternative reaction-preventing crucible material candidate, referring to a fabrication feasibility and a phase stability. 5 kinds of Y<sub>2</sub>O<sub>3</sub>-based ceramic pellet were prepared and characterized as a sintering method according to the pseudo binary phase and pseudo ternary phase diagrams.

### 2. Methods and Results

High temperature ceramic powders of Al<sub>2</sub>O<sub>3</sub>, Y<sub>2</sub>O<sub>3</sub>, La<sub>2</sub>O<sub>3</sub>, Nd<sub>2</sub>O<sub>3</sub>, ZrO<sub>2</sub> and CeO<sub>2</sub> were used with a purity higher than 99.9% and a particle size smaller than 2.5 μm as raw materials in this experiment. Mixed powder slurry of the ceramic material with was obtained through wet ball milling for 24 hrs. The powder slurry was then annealed by heating at 1000 °C for 10 hrs to remove foreign adhering substances including moisture.

Wet ball milling was again performed for 24 hrs to obtain a powder slurry with a uniform composition of the calcined powder. At this time, when the powder slurry was put into the spray-drying apparatus, the rotation speed of the disk was in the range of 6000 rpm to 7000 rpm. Spherical mixed powder ranging from 10 μm to 60

μm in particle size was prepared from the slurry of mixed powders through a spray drying and a sieving process. Green compact was made using the mixed powders by cold isostatic pressing(CIP). Finally, Y<sub>2</sub>O<sub>3</sub>-based high-temperature ceramic pellets of Y<sub>2</sub>O<sub>3</sub>-50mol.% Al<sub>2</sub>O<sub>3</sub>(YAG), Y<sub>2</sub>O<sub>3</sub>-25mol.%Nd<sub>2</sub>O<sub>3</sub>-15mol.% La<sub>2</sub>O<sub>3</sub>, Y<sub>2</sub>O<sub>3</sub>-30mol.% Nd<sub>2</sub>O<sub>3</sub>-5mol.%La<sub>2</sub>O<sub>3</sub>, Y<sub>2</sub>O<sub>3</sub>-50mol.% Nd<sub>2</sub>O<sub>3</sub>-40mol.% ZrO<sub>2</sub>, and Y<sub>2</sub>O<sub>3</sub>-25mol.%Nd<sub>2</sub>O<sub>3</sub>-15mol.%CeO<sub>2</sub> were synthesized by holding the temperature ranging from 1550°C to 1620°C upto 10 hrs. The density of the sintered pellets was determined using an Archimedean immersion method. The microstructure of the sintered synthetics was investigated by scanning electron microscopy combined with energy dispersive spectroscopy(SEM/EDS). The phase structure of the sintered synthetics was examined by X-ray diffraction (XRD).

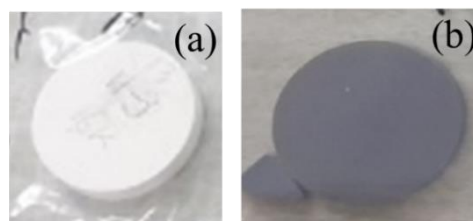


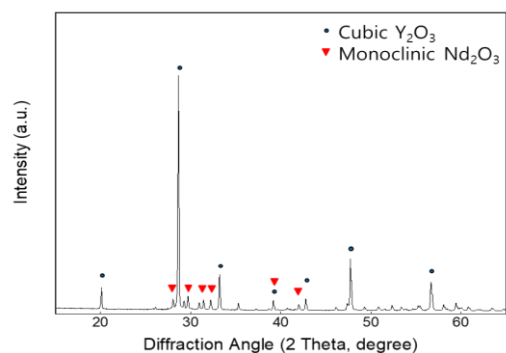
Fig. 1. Typical Y<sub>2</sub>O<sub>3</sub>-based ceramic pellets synthesized at high temperature; (a) Y<sub>2</sub>O<sub>3</sub>-50mol.% Al<sub>2</sub>O<sub>3</sub>(YAG) and (b) Y<sub>2</sub>O<sub>3</sub>-Nd<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>

Y<sub>2</sub>O<sub>3</sub>-based ceramic pellets were generally soundly fabricated as showed in Fig. 1. Density of the alternative crucible material according to molar composition was showed in Table 1. As the sintering temperature and the sintering time increased, the density of Y<sub>2</sub>O<sub>3</sub>-based ceramic pellets prominently increased. The density generally shows an indirect indication of the internal defects such as pores in the sintered pellet. The Y<sub>2</sub>O<sub>3</sub>-based ceramic pellets sintered below 1550°C generally showed insufficient densification with a low relative density of 78.8% in average density due to the lack of consolidation. When the sintering temperature was raised to 1620°C, the relative density increased greatly up to 91.1% of theoretical density with sufficient consolidation. Especially, bulk density and relative density of Y<sub>2</sub>O<sub>3</sub>-25mol.%Nd<sub>2</sub>O<sub>3</sub>-15mol.%La<sub>2</sub>O<sub>3</sub> and

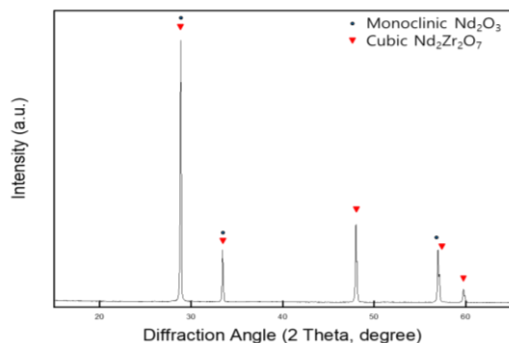
$Y_2O_3$ -30mol%  $Nd_2O_3$ -5mol% $La_2O_3$  pellet showed an excellent densification, with a high relative density of above 99% and low porosity of below 1%.

Table 1. Measured bulk density and relative density of sintered pellets according to molar composition of the  $Y_2O_3$ -based ceramic pellets.

$Y_2O_3$ -based crucible material	Measured density ( $g/cm^3$ )	Relative density (%)	Porosity (%)
$Y_2O_3$ -50 $Al_2O_3$ (YAG)	3.58	79.4	16.5
$Y_2O_3$ -25 $Nd_2O_3$ -15 $La_2O_3$	5.81	99.9	0.1
$Y_2O_3$ -30 $Nd_2O_3$ -5 $La_2O_3$	5.76	99.8	0.8
$Y_2O_3$ -50 $Nd_2O_3$ -40 $ZrO_2$	5.62	89.4	3.6
$Y_2O_3$ -25 $Nd_2O_3$ -15 $CeO_2$	5.07	87.2	7.4



(a)



(b)

Fig. 2. Typical X-ray diffraction patterns according to molar composition of the  $Y_2O_3$ -based ceramic synthetics.

Typical X-ray diffraction patterns of the sintered synthetic according to alternative material composition are shown in Fig. 2. The major phases of  $Y_2O_3$ -30mol.% $Nd_2O_3$ -5mol.% $La_2O_3$  and  $Y_2O_3$ -25mol.%  $Nd_2O_3$ -15mol.% $La_2O_3$  sintered body revealed as a cubic  $Y_2O_3$  and a monoclinic  $Nd_2O_3$  phase as shown in Fig. 2-(a). The major phases of  $Y_2O_3$ -50mol.% $Nd_2O_3$ -40mol.%

$ZrO_2$  sintered body revealed as a cubic  $Nd_2Zr_2O_7$  and a monoclinic  $Nd_2O_3$  phase as shown in Fig. 2-(b). The XRD analysis result was found to be in good agreement with the previously reported results of the  $Y_2O_3$ - $Nd_2O_3$  and the  $Y_2O_3$ - $Nd_2O_3$  pseudo phase diagram [7].

### 3. Conclusions

$Y_2O_3$ -based ceramic material as an alternative reaction-preventing crucible material was synthesized by a sintering method at elevated temperature. The bulk density and the relative density of  $Y_2O_3$ -25mol.% $Nd_2O_3$ -15mol.% $La_2O_3$  and  $Y_2O_3$ -30mol.%  $Nd_2O_3$ -5mol.% $La_2O_3$  synthetics showed an excellent densification, with a high relative density of above 99% and low porosity of below 1%. The major phases of  $Y_2O_3$ -30mol.% $Nd_2O_3$ -5mol.% $La_2O_3$  and  $Y_2O_3$ -25mol.%  $Nd_2O_3$ -15mol.% $La_2O_3$  sintered body revealed as a cubic  $Y_2O_3$  and a monoclinic  $Nd_2O_3$  phase with phase stability by sintering ranging from 1550°C to 1620°C, irrespectively of the molar ratio of  $La_2O_3$ . It is thought that the  $Y_2O_3$ - $Nd_2O_3$ - $La_2O_3$  synthetic is the most promising candidates of the reaction-preventing crucible materials for the injection casting of U-TRU-Zr-RE metal fuels.

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