

## Effect of recycled $U_3O_8$ powders on doped $UO_2$ pellets property

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### 1. Introduction

To reduce the fuel cycle costs and the total mass of spent light water reactor (LWR) fuels, it is necessary to extend the fuel discharged burn-up [1]. Extending the fuel discharged burn-up, while enhancing the safety features is one of the major challenges to nuclear energy industries because it can reduce the maintenance and fuel cycle cost [2]

Research on fuel pellets focuses on increasing the pellet density and grain size to increase the uranium contents and the high burn-up safety margins for LWRs. KAERI has developed a doping technology to increase the density and grain size of  $UO_2$  pellets. In this technology, the 1000ppm of additives were used and the grain size of  $UO_2$  pellets was increased up to  $50\mu m$ . This grain size is about 5 times larger than that of commercial  $UO_2$  pellet.

In a commercial  $UO_2$  fuel pellet manufacturing process, defective  $UO_2$  pellets or scraps are produced and those should be reused. A common recycling method for defective  $UO_2$  pellets or scraps is that they are oxidized in air at about  $450^\circ C$  to make  $U_3O_8$  powder and then added to  $UO_2$  powder. In the oxidation of a  $UO_2$  pellet, the oxygen propagates along the grain boundary. The  $U_3O_8$  formation on the grain boundary causes a spallation of the grains. So, size and shape of  $U_3O_8$  powder deeply depend on the initial grain size of  $UO_2$  pellets. Since the grain size of doped  $UO_2$  pellet is quite larger than that of commercial pellet, it is expected that the shape and size of  $U_3O_8$  from large grain sized pellets are somewhat different to those from conventional pellets.

In this study, the effect of  $U_3O_8$  powders on the doped  $UO_2$  pellet property was examined. Two kinds of  $U_3O_8$  powders which have different size to each other were prepared. Those  $U_3O_8$  powders were mixed with doped  $UO_2$  powders and sintered into pellets. Density and grain size evolution of pellets with increase of  $U_3O_8$  contents were evaluated and compared.

### 2. Experimental

Mixed powder of  $MnO-Al_2O_3$  additive and  $UO_2$  was prepared. Total amount of Mn-Al in the powder mixture was 1000ppm in weight. Two kinds of  $U_3O_8$  powders were prepared. ADU  $UO_2$  powders larger than  $150\mu m$  and Mn-Al doped  $UO_2$  pellets were oxidized to  $U_3O_8$  powders at  $450^\circ C$  in air, respectively. The initial grain size of the Mn-Al doped  $UO_2$  pellet was about  $40\mu m$ .

0~10wt% of those  $U_3O_8$  powders were added to  $MnO-Al_2O_3-UO_2$  powder mixtures and then mixed for 24h with a tumbling mixer.

Final powder mixtures were pressed into green pellets and then sintered powder sintered at  $1730^\circ C$  for 4 h in flowing  $H_2$  gas.

The sintered density of the pellets was measured by a water immersion method. The pellets were sectioned axially, ground and polished. The polished pellets were thermally etched at  $1290^\circ C$  in carbon dioxide gas in order to examine their grain boundaries. The pore and grain structure were examined by an optical microscope and grain size was determined by a linear intercept method.

### 3. Results

Fig. 1 shows the typical grain structure of sintered pellets. This figure clearly showed that the grain structure was greatly altered by the origin of  $U_3O_8$  powder in the powder mixture. The grain size and density were decreased considerably in the  $UO_2$  pellet which was fabricated by using the powder mixture of  $UO_2$  with the  $U_3O_8$  obtained by oxidation of large grained  $UO_2$  pellet.

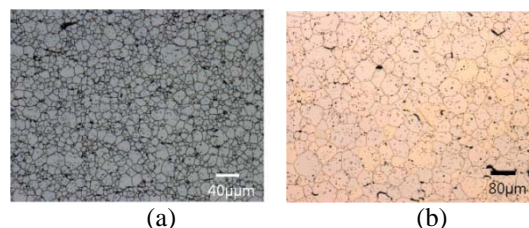


Fig. 1. Effect of  $U_3O_8$  powders on the grain structures of sintered pellets: The  $U_3O_8$  powders originated from (a)  $UO_2$  sintered pellet, (b) powder.

Fig. 2 shows the density and grain size change according to initial  $U_3O_8$  contents in  $UO_2$  pellets. The density and grain size of the  $UO_2$  pellet which was fabricated by using the pellet-oxidized  $U_3O_8$  powder was shown in Fig. 2 (a). The density and grain size decreased due to the addition of  $U_3O_8$  powder. It could be thought that a sinterability of the powder mixture was degraded by the pellet-oxidized  $U_3O_8$  powder.

On the other hand, the density and grain size of  $UO_2$  pellet which was produced by using the powder-oxidized  $U_3O_8$  powder hardly changed (Fig. 2 (b)).

Two kinds of  $U_3O_8$  powders have a different size to each other. The particle size of powder-oxidized  $U_3O_8$  powder is lower than that of pellet-oxidized powder.

Therefore, it can be thought that there is a difference of specific surface area between pellet-oxidized and powder-oxidized  $U_3O_8$  powder. The sinterability of powder mixture would be affected by these differences.

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[2] OECD, NEA report No. 6224, Very High burn-ups in Light Water Reactors (2006).

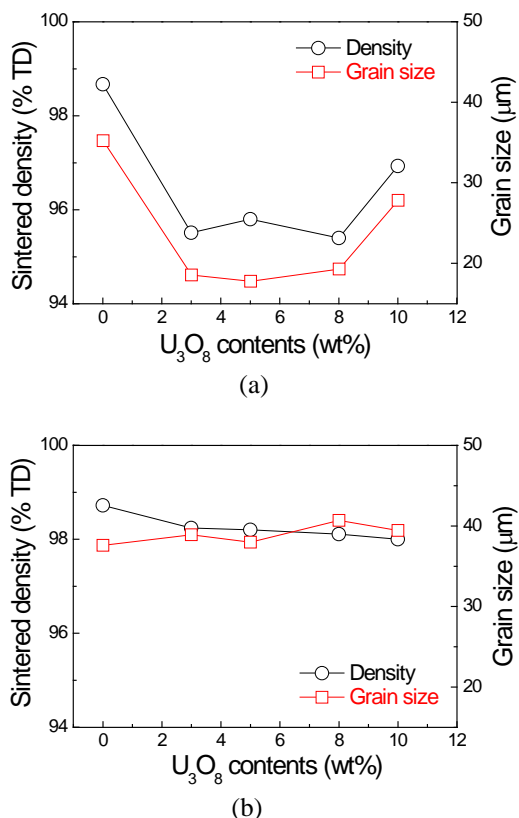


Fig. 2. The density and grain size of Mn-Al and  $U_3O_8$  doped  $UO_2$  pellet: (a) pellet-oxidized  $U_3O_8$  doped, (b) powder-oxidized  $U_3O_8$  doped.

#### 4. Conclusions

The effect of  $U_3O_8$  powders on the doped  $UO_2$  pellet property was examined. The  $UO_2$  pellet was fabricated by using two kinds of  $U_3O_8$  powders which have different size to each other. And then, the density and grain size change of fabricated pellets were investigated.

In the results, the powder-oxidized  $U_3O_8$  powder hardly affects the sinterability, but the pellet-oxidized  $U_3O_8$  powder degraded the sinterability. Therefore, in the recycling of  $U_3O_8$  powder, it can be concluded that the powder-oxidized  $U_3O_8$  powder is more profitable.

#### ACKNOWLEDGEMENT

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#### REFERENCES

[1] Ph. Dehaut et al., Proceeding of the IAEA Technical Committed Meeting, “Advanced in fuel