

## Dimensional Change of Annular Pellet Fabricated using $U_3O_8$ - $UO_2$ Powder Mixture

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### 1. Introduction

To increase the economic efficiency of a nuclear power generation, the development of an innovative nuclear fuel for a high burnup and extended cycle is necessary. It must be considered both uprating a power of nuclear reactor and increasing the safety margin of nuclear fuel, simultaneously. One of the best ways to do this is a new fuel geometry design that is of an annular shape pellet in its inner and outer cladding, and has the geometry design of both an internal and external cooling system (dual cooled nuclear fuel) [1].

The dual cooled fuel is being developed by Korea Atomic Energy Research Institute (KAERI). Also, as a part of the project, the development of a fabrication technology of an annular pellet is now in progress [2].

In the development of a fabrication technology of an annular pellet for dual cooled fuel, it is important that a dimensional tolerance of an annular pellet satisfied with a fuel design criteria.

During a typical pellet fabrication process, fairly amount of defective  $UO_2$  pellets are produced and it is necessary to recycle the scraps. Generally, the defective scraps are powdered through the air oxidation and then mixed with co-milled powder, and further processed to fabricate  $UO_2$  pellets [3-5].

In this study, the dimension and dimensional tolerance change of  $U_3O_8$  added  $UO_2$  sintered annular pellet was observed. And then, a resintering test [6] of the fabricated annular pellet was performed.

### 2. Experimental

ADU- $UO_2$  (Ammonium Diuranate) powder was granulated with a pressure of 70 MPa and a 20 mesh (aperture: 850  $\mu m$ ) sieve.  $U_3O_8$  powder was prepared by heating  $UO_2$  pellets in flowing air at 400°C for 3 h. The granulated  $UO_2$  powder was mixed with the prepared  $U_3O_8$  powder (0~10 wt%) by using a Turbula mixer for 0.5 h. And it was mixed with a lubricant powder (0.3 wt% zinc stearate).

The  $U_3O_8$ - $UO_2$  powder mixture was compacted by using a double acting press, and sintered at 1730 °C for 4h in a flowing  $H_2$  atmosphere. And then, the sintered annular pellets were resintered at 1700 °C for 24h in a flowing  $H_2$  atmosphere.

The sintered and resintered density of the annular pellet was determined by using an immersion method, and the dimensions of the annular pellet were measured by using a 3-dimensional precise measuring system (VERTEX 230, MicroVu).

### 3. Results

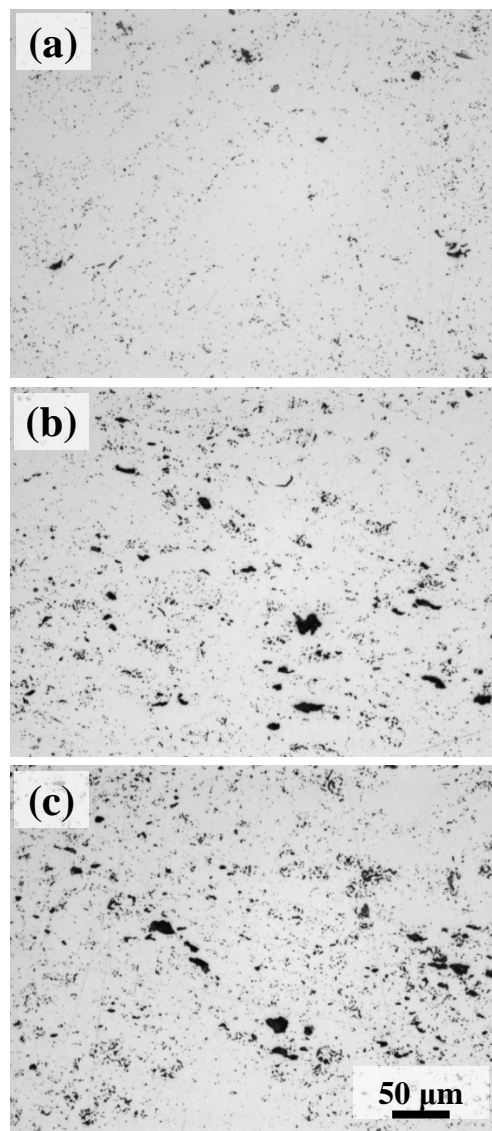


Figure 1. The optical microscopic image ( $\times 200$ ) of sintered  $UO_2$  annular pellets: (a) 0 wt%, (b) 6 wt%, (c) 10 wt%  $U_3O_8$  powder added.

Figure 1 shows a microstructure of the sintered annular pellet fabricated using the  $U_3O_8$ - $UO_2$  powder mixture. The number of large and small pore increased with increasing  $U_3O_8$  contents. In the  $U_3O_8$ -added annular pellet, group of small pore (trace of  $U_3O_8$  powder) could be observed.

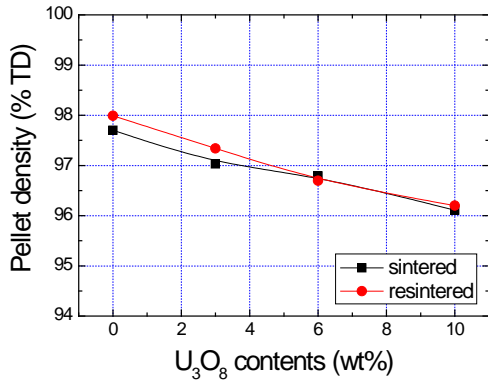


Figure 2. The sintered and resintered density of the annular pellet as a function of U<sub>3</sub>O<sub>8</sub> contents.

Figure 2 shows the sintered and resintered density of the annular pellet as a function of U<sub>3</sub>O<sub>8</sub> contents. The density of annular pellet decreased with increasing U<sub>3</sub>O<sub>8</sub> contents, because of the formed pore in the pellet due to U<sub>3</sub>O<sub>8</sub> powder. On the other hand, density change of the annular pellet during a resintering test was little.

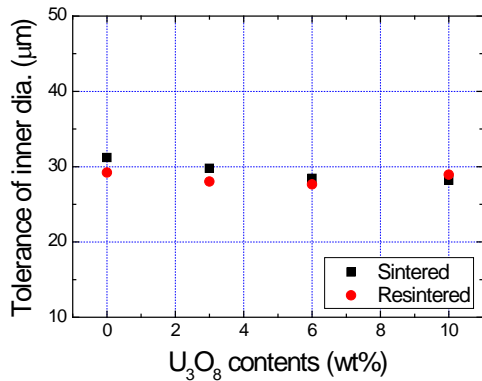


Figure 3. The tolerance of inner diameter of sintered and resintered annular pellet as a function of U<sub>3</sub>O<sub>8</sub> contents.

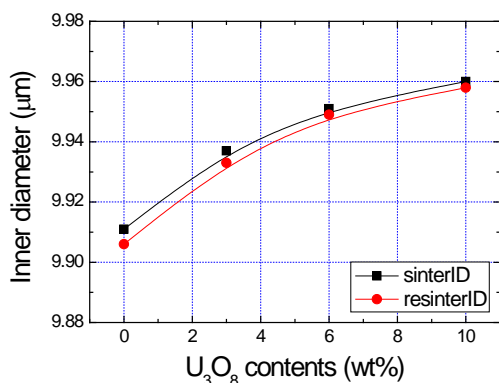


Figure 4. The inner diameter of sintered and resintered annular pellet as a function of U<sub>3</sub>O<sub>8</sub> contents.

The inner diametric tolerance of sintered and resintered annular pellet as a function of U<sub>3</sub>O<sub>8</sub> contents

is shown in Figure 3. There was little influence of the U<sub>3</sub>O<sub>8</sub> addition on the tolerance of annular pellet.

Figure 4 shows the inner diameter of the sintered and resintered annular pellet as a function of U<sub>3</sub>O<sub>8</sub> contents. The inner diameter of the annular pellet increased with increasing U<sub>3</sub>O<sub>8</sub> contents.

#### 4. Summary

The effect of U<sub>3</sub>O<sub>8</sub> addition on the density, dimension and dimensional tolerance of annular pellet was experimentally observed. In the results, it could be observed that the tolerance of inner diameter of annular pellet hardly changed due to U<sub>3</sub>O<sub>8</sub> addition. However, inner diameter of annular pellet increased with increasing U<sub>3</sub>O<sub>8</sub> contents. Therefore, to recycle the scrap U<sub>3</sub>O<sub>8</sub> powder, an effort to maintain a constant inner diameter is needed. Also, the minimization of inner diametric tolerance is simultaneously needed.

#### ACKNOWLEDGEMENT

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